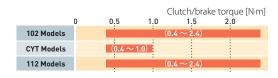
ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES



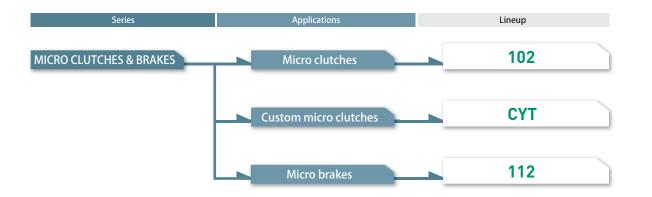
Application Automated teller machines, sorters, office equipment, weighing and packaging machinery, printing machinery, bookbinding machinery, optical equipment

Micro Clutches and Micro Brakes for Precise Control of Compact Precision Equipment

These micro clutches and micro brakes are ideal for compact precision equipment where variations in torque and response must be avoided, such as office equipment, communication equipment, and automobiles. In addition to the 102 (clutch) and 112 (brake) models, which share the same basic clutch/brake design, we also provide CYT models (clutches), which can be customized into a wide variety of types to meet customer needs.



Available Models



For details on selection, see P.308 to 315.

Micro Clutches



■ Mounting

102- 🗆 -1 🔲

Wall-mounted type

Uses a flange-mounted stator. Designed to be short in the axial direction, requiring less installation space.







102- □ -3 □ , CYT

Shaft-mounted type

Uses a bearing-mounted stator. Designed to be relatively easy to mount, reducing the processing and work required for mounting.







Bearing-mounted type

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES**

FLECTROMAGNETIC ACTUATED **CLUTCHES & BRAKES** FLECTROMAGNETIC

CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

■ Shaft coupling system (armatures)



Butt and parallel shaft type (Armature type-3)

These incorporate non-armature parts provided by the customer such as V pulleys, enabling use in designs that use either butt shafts or through-shafts.



Armature type-3



Directly coupled type wound around the parallel axis (armature type-5)

Uses an armature assembly designed for use with through-shafts. Ensures that mounting is relatively easy to complete as well as extremely efficient in its approach.



Directly coupled by being wound around the parallel shaft



Armature type-5



Butt type (Armature type-1)

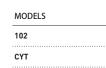
Uses an armature assembly designed for use with butt shafts. May be difficult to mount due to the need for centering and other adjustments, may require the use of a fitting flange, or may require use in combination with flexible couplings.



Coupled directly



Armature type-1



112

Micro Brakes



Shaft-mounted type

These use axial braking in most cases, the effectiveness of which depends on how efficiently parts are mounted.





Mounted to the shaft Armature type-1 Armature type-2

Rotor-mounted type

Uses an armature assembly mounted directly to an inertial body not fastened to the shaft that continues to move even after the shaft has stopped.



Mounted to the rotor

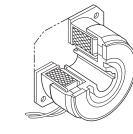


Armature type-3

Product Lineup

Electromagnetic-actuated Micro Clutches - Flange-mounted Type





Stator and rotor are combined and directly mounted on stationary parts, such as frames, and fixed in place. These are short in the axial direction and can use space near walls effectively. Select the armature according to the coupling type used (through-shaft, butt shaft, etc.).

Clutch torque	[N·m]	0.4 ~ 2.4
Operating temperature	[℃]	-10 ∼+40
Backlash		Zero

RoHS-compliant

Flange-mounted type



Electromagnetic-actuated Micro Clutches - Bearing-mounted Type



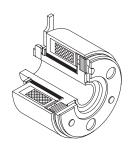


These integrate the stator and rotor, which are held to the stationary parts of the machine by a drive pin arm; the rotor is locked to the rotation shaft by a set screw. They are designed to be relatively easy to mount, reducing the processing work required for mounting. Select the armature according to the coupling type used (through-shaft, butt shaft, etc.).

Clutch torque	[N·m]	0.4 ~ 2.4	
Operating temperature	[℃]	−10 ~+40	
Backlash		Zero	

Electromagnetic-actuated Micro Clutches - Custom Type

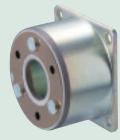




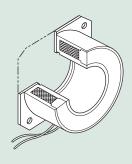
The CYT models are the basic building blocks for customized microclutches. The basic model is bearing mounted. Two types are available for different shaft rotation speeds: a dry metal type and a ball bearing type. Armature type-3 is standard, but many customizations are possible.

Clutch torque	[N·m]	0.4 ~ 1.0	
Operating temperature	[℃]	−10 ~+40	
Backlash		Zero	

112 Electromagnetic-actuated Micro Brakes



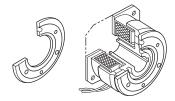




Brakes are used to brake and hold rotating bodies. The flange of the stator is locked securely to a strong stationary part. Select an armature that factors in the mounting space available.

Brake torque	[N·m]	0.4 ~ 2.4
Operating temperature	[℃]	-10 ~+40
Backlash		Zero

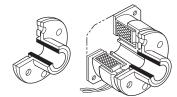
Types for through-shaft or butt shaft



Armature type-3

102- 🗆 -13

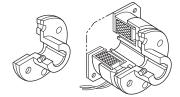
Through-shaft (coupled by winding around parallel shaft) type



Armature type-5

102- 🗆 -15

Butt shaft type

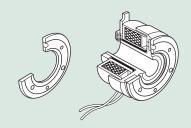


Armature type-1

102- 🗌 -11

ELECTROMAGNETIC **CLUTCHES & BRAKES**

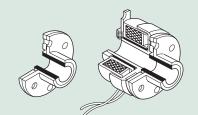
Types for through-shaft or butt shaft



Armature type-3

102- 🗆 -33

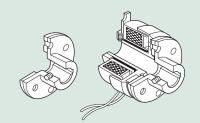
Through-shaft (coupled by winding around parallel shaft) type



Armature type-5

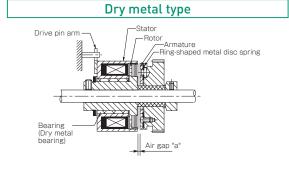
102- 🗆 -35

Butt shaft type



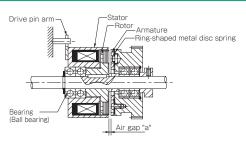
Armature type-1

102- 🗆 -31



CYT- □ -33M

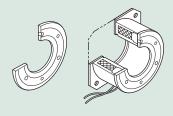
Ball bearing type



CYT- □ -33B



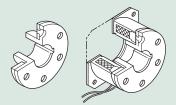
Slim, space-saving type



Types with many applications

Armature type-3

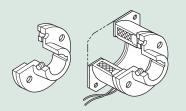
112- 🗆 -13



Armature type-2

112- 🗆 -12

Easy-to-use standard-shape type



Armature type-1

112- 🗆 -11

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES

ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES

ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

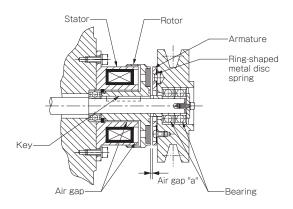
MODELS 102 CYT

112

Mounting and CYT Customization Examples

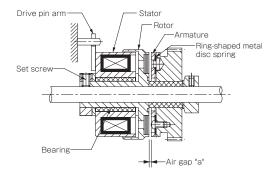
■ Flange-mounting example with 102

The stator is directly mounted on a stationary part, such as a frame, by a mounting flange, and fixed in place. The rotor is locked to the rotation shaft using a key. The stator and rotor are combined via a narrow air gap that serves as part of the magnetic circuit to form a magnetic pole.



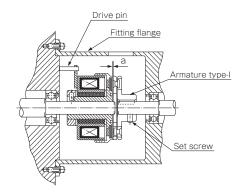
■ Bearing-mounting example with 102.

The stator is integrated with the rotor via a bearing and held to the stationary parts of the machine by a drive pin arm. The rotor is locked to the rotation shaft using a set screw. The stator and rotor form a magnetic pole via the bearing (ferrous oil-impregnated metal).



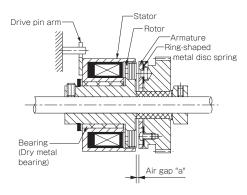
■ Butt shaft mounting example with 102

In designs that use butt shafts, the two shafts can be reliably centered using fitting flanges, as shown in the figure.



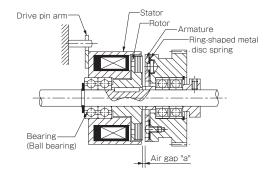
Dry-metal type mounting example with CYT

The stator is integrated with the rotor via dry metal, and held to the stationary parts of the machine by a drive pin arm. The rotor is locked to the rotation shaft using a set screw. The stator and rotor form a magnetic pole via the dry metal.



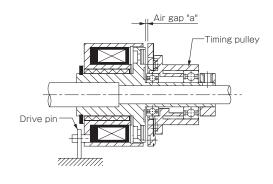
Ball-bearing type mounting example with CYT

The stator is mounted on the shaft via a bearing and held to the stationary parts of the machine by a drive pin arm. The stator and rotor are combined via a narrow air gap that serves as part of the magnetic circuit to form a magnetic pole.



Dry-metal type embedding example with CYT

We design to your requirements using timing pulleys, gears and the like mounted on armature type-3.

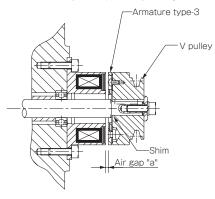


Mounting and CYT Customization Examples

■ Armature type-3 mounting example with 112

Armature type-3 is used by directly mounting it to a transmission element such as a V-pulley or to a rotating body that stops inertial force.

The shaft of the brake part requires no processing. The shaft diameter may also be determined freely. Air gap "a" can be set easily using collars and shims. Corrections are easily accomplished by adding or removing shims.

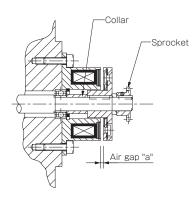


■ Armature type-2 mounting example with 112

Armature type-2 has the smallest mounting-space footprint of any of the armatures, so overhang is not a concern even when a sprocket or the like is mounted on the brake tip.

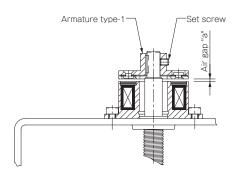
Air gap "a" can be set easily using collars and shims.

Corrections are easily accomplished by adding or removing shims.



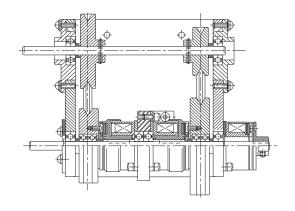
■ Armature type-1 mounting example on vertical shaft with 112

Since there is no restriction on mounting direction, there is no running torque or abnormal wear even when mounted on vertical shafts. It is easy to set air gap a: simply move armature type-1 and lock it in place with a set screw.



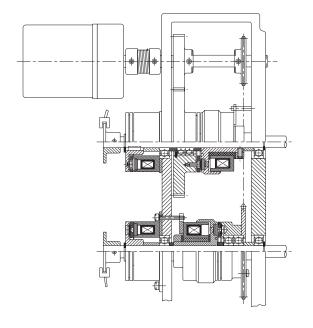
■ Example of the combination of clutches and brakes

This example uses a two-step speed-change mechanism combining two clutches and a brake.



■ Example of the combination of clutches and brakes

Shaft drive is both forward and reverse in combination with a clutch in this example. Start and stop freely by mounting brakes on each shaft.



ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES

FI FCTROMAGNETIC ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC

CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

102

CYT

112

Types Electromagnetic Micro Clutches - Flange-mounted Type

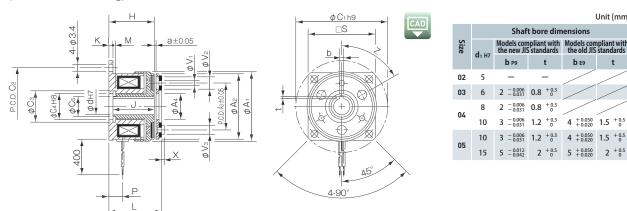
Specifications

		Dynamic	(Coil (a	t 20°C ∶)	He		Rotating part mo	ment of inertia J	AII 11	Total work			_	
Model	Size	friction torque Td [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat resistance class	Max. rotation speed [min ⁻¹]	Armature [kg·m²]	Rotor [kg·m²]	Allowable engaging energy E _{ea} £ [J]	performed until read- justment of the air gap Ετ [J]	Armature pull-in time ta [s]	Torque rise time t _p [s]	Torque extinction time td [s]	Mass [kg]
102-02-13								10000	6.75×10^{-7}							0.075
102-02-15	02	0.4	DC24	6	0.25	96	В	500	1.00×10^{-6}	2.45×10^{-6}	1500	2×10^{6}	0.009	0.019	0.017	0.081
102-02-11								10000	1.00×10^{-6}							0.079
102-03-13								10000	1.30×10^{-6}							0.096
102-03-15	03	0.6	DC24	6	0.25	96	В	500	1.95×10^{-6}	3.25×10^{-6}	2300	3×10^6	0.009	0.022	0.020	0.105
102-03-11								10000	1.95×10^{-6}							0.103
102-04-13								10000	4.38×10^{-6}							0.178
102-04-15	04	1.2	DC24	8	0.33	72	В	500	6.15×10^{-6}	1.41×10^{-5}	4500	6×10^6	0.011	0.028	0.030	0.195
102-04-11								10000	6.15×10^{-6}							0.191
102-05-13								10000	9.08×10^{-6}							0.310
102-05-15	05	2.4	DC24	10	0.42	58	В	500	1.38×10^{-5}	3.15×10^{-5}	9000	9 × 10 ⁶	0.012	0.031	0.040	0.335
102-05-11								10000	1.38×10^{-5}							0.325

^{*} The dynamic friction torque, $T_{\rm d}$, is measured at a relative speed of 100 $\rm min^{\text{-}1}$

Dimensions (102- \square -13)

(For direct mounting)



Si		Radial direction dimensions															Axial direction dimensions								
Size	A ₁	A ₂	A ₃	A ₄	C ₁	C ₂	C ₃	C ₄	C₅	S	V ₁	V ₂	V ₃	Z	Н	J	K	L	Р	M	a	Х			
02	31	28	19.5	10.5	39	33.5	11.4	11	8	_	2-2.1	2-5.3	2-4	4-90°	18	16.5	1.5	20.5	5	1.1	0.1	0.8			
03	34	32	23	12.5	45	38	13.6	13	10	33	3-2.6	3-6	3-4.5	6-60°	22.2	20.2	2	24.5	6.7	1.3	0.15	1.2			
04	43	40	30	18.5	54	47	20	19	15.5	41	3-3.1	3-6	3-5	6-60°	25.4	23.4	2	28.2	7	1.3	0.15	1.5			
05	54	50	38	25.5	65	58	27.2	26	22	51	3-3.1	3-6.5	3-5.5	6-60°	28.1	26.1	2	31.3	8.2	1.5	0.2	1.5			

How to Place an Order

102-03-13 24V 6DIN Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards Rotor bore diameter (dimensional symbol d)

Unit [mm]

*Models for which there are no keyway standards (models marked by [-]) on the Shaft Bore Dimensions table need not be marked with a keyway standards designation. Products with standards marked by diagonal lines are not set as standard products.

^{*} The moment of inertia of a rotating body and mass are measured for the maximum bore diameter.

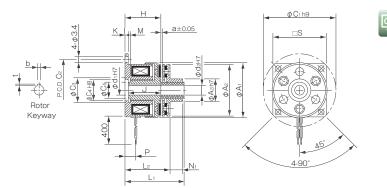
* Keep supply voltage fluctuation to within 10% of coil voltage.

^{*} Size 02 is a rounded flange.

* The rotor of size 02 has no keyway. Lock it in place by press-fitting it onto the shaft or the like.

Dimensions (102- □ **-15)**

(For through-shafts)



						Unit [mm]
			Shaft	bore dime	ensions	
Size	d ₁	d ₂	Models com the new JIS	pliant with standards	Models con the old JIS	npliant with standards
	Н7	Н7	b P9	t	b E9	t
02	5	5	_	_		
03	6	6	$2 {}^{- 0.006}_{- 0.031}$	0.8 + 0.3		
04	8	8	$2\ \ {}^{-\ 0.006}_{-\ 0.031}$	$0.8^{+0.3}_{0}$		
04	10	10	$3 \begin{array}{c} -0.006 \\ -0.031 \end{array}$	$1.2^{+0.3}_{0}$	4 + 0.050 + 0.020	1.5 + 0.5
05	10	10	3 -0.006	1.2 + 0.3	4 + 0.050 + 0.020	1.5 + 0.5
UĐ	15	15	5 -0.012	2 + 0.5	5 +0.050 +0.020	2 + 0.5
* Tho	arma:	turo t	vne-5 hore	d- ic a etraio	ht horo	

The armature type-5 bore d2 is a straight bore

																		Unit [mm]		
Size				Radial di	rection di	mensions				Axial direction dimensions										
ze	A ₁	A ₂	A ₃	C ₁	C ₂	C₃	C ₄	C ₅	S	Н	J	K	L ₁	L ₂	M	Р	N_1	a		
02	31	28	13	39	33.5	11.4	11	8	_	18	16.5	1.5	27.5	22.4	1.1	5	4.8	0.1		
03	34	32	14	45	38	13.6	13	10	33	22.2	20.2	2	34.5	26.5	1.3	6.7	7.8	0.15		
04	43	40	18	54	47	20	19	15.5	41	25.4	23.4	2	40.2	30.8	1.3	7	9.1	0.15		
05	54	50	28	65	58	27.2	26	22	51	28.1	26.1	2	43.3	34.3	1.5	8.2	8.8	0.2		

Size 02 is a rounded flange.

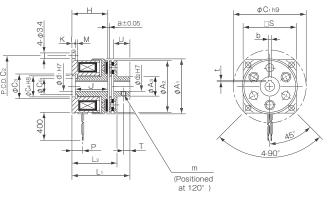
How to Place an Order



*Models for which there are no keyway standards (models marked by [-]) on the Shaft Bore Dimensions table need not be marked with a keyway standards designation. Products with standards marked by diagonal lines are not set as standard products.

Dimensions (102- □ **-11)**

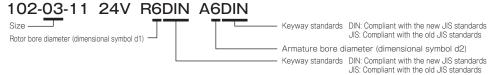
(For butt shafts)



						Unit [mm
			Shaft	bore dime	nsions	
Size	d ₁	d ₂	Models con the new JIS	pliant with standards	Models con the old JIS	npliant with standards
	Н7	Н7	b P9	t	b E9	t
02	5	5	_	_		
03	6	6	$2 \begin{array}{c} -0.006 \\ -0.031 \end{array}$	0.8 + 0.3		
04	8	8	$2 \ \ {}^{- 0.006}_{- 0.031}$	$0.8^{+0.3}_{0}$		
04	10	10	$3 \begin{array}{c} -0.006 \\ -0.031 \end{array}$	$1.2^{+0.3}_{0}$	4 + 0.050 + 0.020	1.5 + 0.5
05	10	10	3 -0.006	1.2 + 0.3	4 + 0.050 + 0.020	1.5 + 0.5
UO	15	15	5 - 0.012 - 0.042	2 + 0.5	5 + 0.050 + 0.020	2 + 0.5

						at 120)°)												ι	Jnit [mm]	
<u>δ</u>	Radial direction dimensions											Axial direction dimensions									
ze	\mathbf{A}_1	A ₂	A ₃	C ₁	C ₂	C ₃	C ₄	C ₅	S	m	Н	J	K	L ₁	L ₂	М	Р	U	T	а	
02	31	28	9.5	39	33.5	11.4	11	8	_	M3	18	16.5	1.5	27.5	22.5	1.1	5	7	2.5	0.1	
03	34	32	12	45	38	13.6	13	10	33	2-M3	22.2	20.2	2	34.5	26.5	1.3	6.7	10	4	0.15	
04	43	40	17	54	47	20	19	15.5	41	2-M3	25.4	23.4	2	40.2	30.8	1.3	7	12	5	0.15	
05	54	50	24	65	58	27.2	26	22	51	2-M4	28.1	26.1	2	43.3	34.3	1.5	8.2	12	5	0.2	

How to Place an Order



^{*}Models for which there are no keyway standards (models marked by [-]) on the Shaft Bore Dimensions table need not be marked with a keyway standards designation. Products with standards marked by diagonal lines are not set as standard products.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNET	ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
TIC-ACTUATED CLU	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
TCHES & BRAKI	ELECTROMAGNETIC CLUTCH & BRAKE

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

112

CYT

^{*} The rotor of size 02 has no keyway. Lock it in place by press-fitting it onto the shaft or the like.

^{*} The rotor of size 02 has no keyway. Lock it in place by press-fitting it onto the shaft or the like.

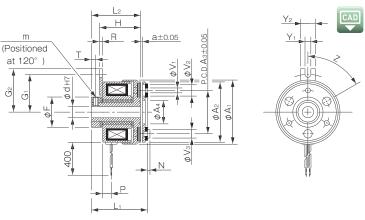
Types Electromagnetic Micro Clutches - Bearing-mounted Type

Specifications

		Dynamic friction		Coil (at	20℃)		res	Max.	Rotating part mo	ment of inertia J	Allowable	Total work per- formed until	Armature	Torque	Torque	
Model	Size	torque T _d [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat resistance class	rotation speed [min ⁻¹]	Armature [kg·m²]	Rotor [kg·m²]	engaging energy E _{ea} ℓ [J]	readjustment of the air gap ET [J]	pull-in time ta [s]	rise time t _p [s]	extinction time td [s]	Mass [kg]
102-02-33									6.75×10^{-7}							0.076
102-02-35	02	0.4	DC24	6	0.25	96	В	500	1.00×10^{-6}	2.75×10^{-6}	1500	2×10^6	0.009	0.019	0.017	0.082
102-02-31									1.00×10^{-6}							0.080
102-03-33									1.30×10^{-6}							0.101
102-03-35	03	0.6	DC24	6	0.25	96	В	500	1.95×10^{-6}	4.08×10^{-6}	2300	3×10^6	0.009	0.022	0.020	0.110
102-03-31									1.95×10^{-6}							0.108
102-04-33									4.38×10^{-6}							0.183
102-04-35	04	1.2	DC24	8	0.33	72	В	500	6.15×10^{-6}	1.44×10^{-5}	4500	6×10^6	0.011	0.028	0.030	0.200
102-04-31									6.15×10^{-6}							0.196
102-05-33									9.08×10^{-6}							0.321
102-05-35	05	2.4	DC24	10	0.42	58	В	500	1.38×10^{-5}	2.90×10^{-5}	9000	9×10^6	0.012	0.031	0.040	0.346
102-05-31									1.38×10^{-5}							0.336

Dimensions (102- □ **-33)**

(For direct mounting)



		Unit [mm]
Size	Shaft bore dimensions	
Size	d н7	
02	5	
03	6	
04	8	
04	10	
05	10	
05	15	

			-		-																Ur	nit [mm]
Size						Radi	al directi	on dimei	nsions								Axial	directio	n dimer	sions		
ze	A_1	A_2	A ₃	A ₄	F	V ₁	V ₂	V ₃	G ₁	G ₂	Y ₁	Y ₂	Z	m	Н	R	L ₁	L ₂	Р	N	Т	а
02	31	28	19.5	10.5	14	2-2.1	2-5.3	2-4	16.8	20	3.1	8	4-90°	2-M3	19.5	1.6	25.9	23.5	5	0.8	2.5	0.1
03	34	32	23	12.5	16	3-2.6	3-6	3-4.5	20	23	3.1	8	6-60°	2-M3	21.9	1.6	28.5	26.2	4.7	1.2	2.3	0.15
04	43	40	30	18.5	22	3-3.1	3-6	3-5	23	26	3.1	8	6-60°	2-M4	25.1	1.6	33.2	30.4	5	1.5	2.8	0.15
05	54	50	38	25.5	30	3-3.1	3-6.5	3-5.5	28	31	3.1	8	6-60°	2-M5	27.9	1.6	37.3	34.1	6	1.5	3.3	0.2

How to Place an Order

102-03-33 24V 6

-Rotor bore diameter (dimensional symbol d)

^{*} The dynamic friction torque, T_d, is measured at a relative speed of 100 min⁻¹.

* The moment of inertia of a rotating body and mass are measured for the maximum bore diameter.

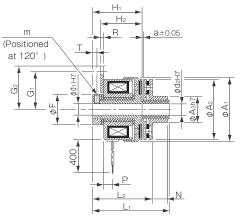
* Keep supply voltage fluctuation to within 10% of coil voltage.

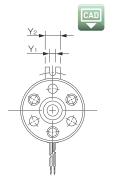
ELECTROMAGNETIC

CLUTCHES & BRAKES

Dimensions (102- □ **-35)**

(For through-shafts)





		Unit [mm]
Size	Shaft bore	dimensions
Ze	d 1 н7	d ₂ H7
02	5	5
03	6	6
04	8	8
04	10	10
05	10	10
US	15	15

	Unit [mm]								
	_								
N	T	a							
4.8	2.5	0.1							
7.8	2.3	0.15							
9.1	2.8	0.15							

ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

ELECTROMAGNETIC-ACTUATED MICRO

CLUTCHES & BRAKES

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SERIES

SPRING-ACTUATED BRAKE

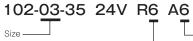
ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

Radial direction dimensions **Axial direction dimensions** Size A₂ Аз G1 H1 H₂ R 02 31 28 13 14 16.8 20 3.1 2-M3 23.5 19.5 1.6 33 27.9 5 03 34 32 14 16 20 23 3.1 8 2-M3 26.2 21.9 1.6 38.5 30.5 4.7 04 43 40 18 22 23 26 3.1 2-M4 30.4 25.1 1.6 45.2 35.8 5 05 50 28 30 31 3.1 2-M5 27.9 1.6 49.3 40.3

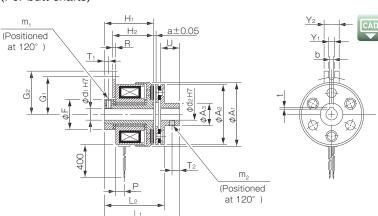
How to Place an Order



Armature bore diameter (dimensional symbol d2) -Rotor bore diameter (dimensional symbol d1)

Dimensions (102- □ **-31)**

(For butt shafts)



						Unit [mm]
			Shaf	t bore dimer	nsions	
Size	d ₁	d ₂	Models com the new JIS	pliant with standards	Models com the old JIS	npliant with standards
	H7	H7	b P9	t	b E9	t
02	5	5	_	_		
03	6	6	$2 {}^{- 0.006}_{- 0.031}$	0.8 + 0.3		
04	8	8	$2 {}^{- 0.006}_{- 0.031}$	0.8 + 0.3		
04	10	10	$3 \begin{array}{c} -0.006 \\ -0.031 \end{array}$	1.2 + 0.3	4 + 0.050 + 0.020	1.5 + 0.5
05	10	10	3 -0.006	1.2 + 0.3	4 + 0.050 + 0.020	1.5 + 0.5
UO	15	15	5 -0.012	2 + 0.5	5 + 0.050 + 0.020	2 + 0.5

Armature bore diameter (dimensional symbol d2)

C001

			r	•		-													U	Init [mm]
Si				Radi	al direction	on dimer	nsions							Axia	l directio	n dimens	ions			
Size	\mathbf{A}_1	A_2	A ₃	F	G ₁	G ₂	Y ₁	Y ₂	m ₁	m ₂	H ₁	H ₂	R	L ₁	L ₂	Р	U	T ₁	T ₂	a
02	31	28	9.5	14	16.8	20	3.1	8	2-M3	М3	23.5	19.5	1.6	33	27.9	5	7	2.5	2.5	0.1
03	34	32	12	16	20	23	3.1	8	2-M3	2-M3	26.2	21.9	1.6	38.5	30.5	4.7	10	2.3	4	0.15
04	43	40	17	22	23	26	3.1	8	2-M4	2-M3	30.4	25.1	1.6	45.2	35.8	5	12	2.8	5	0.15
05	54	50	24	30	28	31	3.1	8	2-M5	2-M4	34.1	27.9	1.6	49.3	40.3	6	12	3.3	5	0.2

How to Place an Order

To download CAD data or product catalogs:

102-03-31 **24V R6 A6DIN** Keyway standards

DIN: Compliant with the new JIS standards

JIS: Compliant with the old JIS standards Rotor bore diameter (dimensional symbol d1)

*Models for which there are no keyway standards (models marked by [-]) on the Shaft Bore Dimensions table need not be marked with a keyway standards designation. Products with standards marked by diagonal lines are not set as standard products.

MODELS

CYT

112

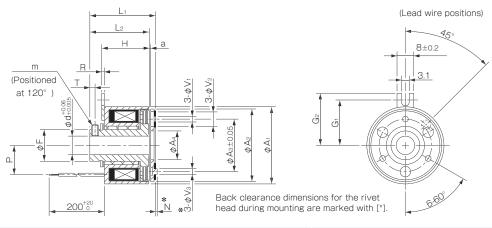
Web code

CYT Models Electromagnetic Micro Clutches - Bearing-mounted Type

Specifications

		Dynamic friction					Heat	Max.	Rotating part m	oment of inertia	Allowable	Total	Armature	Torque	Torque	
Model	Size	friction torque T _d [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	resistance	rotation speed [min ⁻¹]	Armature [kg·m²]	Rotor [kg·m²]	engaging energy E _{ea} ℓ [J]	work E _T [J]	pull-in time ta [s]	rise time t _P [s]	extinction time td [s]	Mass [kg]
CYT-025-33B	025	0.4	DC24	4.5	0.188	128	В	3600	1.00×10^{-6}	1.43×10^{-6}	800	1.0×10^6	0.014	0.028	0.030	0.07
CYT-03-33B	03	0.5	DC24		0.22	105		3600	1 20 × 10-6	1.85×10^{-6}	000	15 × 106	0.015	0.020	0.040	0.13
CYT-03-33M	03	0.5	DC24	5.5	0.23	105	В	500	1.30 × 10 ⁻⁶	1.90×10^{-6}	900	1.5 × 10 ⁶	0.015	0.030	0.040	0.11
CYT-04-33B	0.4	1.0	DC24	F 0	0.25	00		3600	F 1F × 10=6	1.00×10^{-5}	1000	2.0 × 106	0.020	0.040	0.040	0.26
CYT-04-33M	04	1.0	DC24	5.9	0.25	98	В	500	5.15 × 10 ⁻⁶	1.05×10^{-5}	1900	2.0×10^{6}	0.030	0.040	0.040	0.23

Dimensions (CYT- □ -33M)



Size					Radia	al directi	on dime	nsions					Axial direction dimensions									
Size	d	A ₁	A ₂	A ₃	A ₄	F	V ₁	V ₂	V ₃	G ₁	G ₂	m	Н	R	L ₁	L ₂	Р	N	T	a		
03	6 8	34	32	23	12.5	14	3-2.6	3-5.5	3-6	20	23	M3	21	1.2	28.6	26.2	13	3	2.3	0.2 ±0.05		
04	8 10	45	42	30	18.5	18	3-3.1	3-6	3-6	25	27.5	M4	25.3	1.2	35.1	32.4	17.5	3.5	3	0.2 + 0.05		

 $^{^{*}}$ Dimensional symbols N and V3 indicate the clearance dimensions for the rivet head during mounting.

How to Place an Order

CYT-03-33M 24V 6

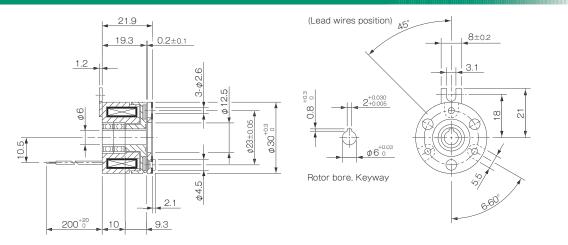
Rotor bore diameter (dimensional symbol d)

Unit [mm]

^{*} The dynamic friction torque, T_d, is measured at a relative speed of 100 min ¹.
* The rotating part moment of inertia and mass are measured for the maximum bore diameter.

^{*} Keep supply voltage fluctuation to within 10% of coil voltage. Also, be careful that energization does not exceed 50%.

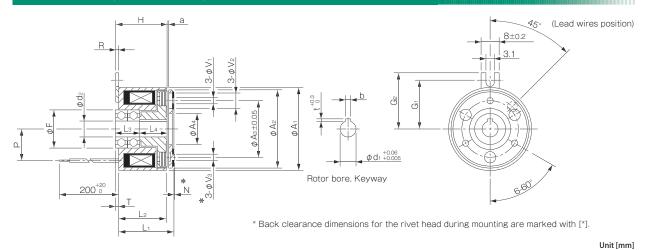
Dimensions (CYT-025-33B)



How to Place an Order

CYT-025-33B 24V 6

Dimensions (CYT- □ -33B)



0.8 + 0.3 0.8 + 0.3 10 11.3 18.5 19 3-3.1 3-6 3-6 25 28 25.3 1.2 26.8 24.1 12 13 17.5 3.5 0.9 0.2 + 0.05 8 2 + 0.030 + 0.005 0.8 + 0.3 42 30 18.5 19 3-3.1 3-6 3-6 25 28 25.3 1.2 26.8 24.1 14 11 17.5 3.5 0.9 0.2 +0.05 10 10 3 +0.025

How to Place an Order

To download CAD data or product catalogs:

CYT-03-33B 24V 6 - Nominal diameter

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

8	ELECTROMAGNETIC-
8	ACTUATED MICRO
2	CLUTCHES & BRAKES
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ELECTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC CLUTCH & BRAKE

SPRING-ACTUATED BRAKE

UNITS

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

CYT

112

C002

Web code

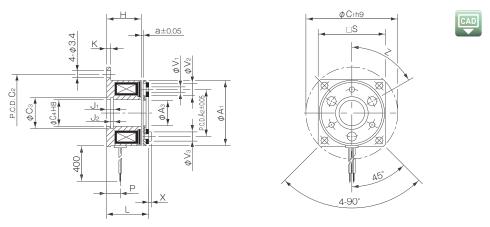
^{*} Dimensional symbols N and V3 indicate the clearance dimensions for the rivet head during mounting.

112 Models Electromagnetic Micro Brakes

Specifications

		Dynamic friction		Coil (at	t 20℃)		Heat	Max.	Armature	Allowable	Total work performed until	Armature	Torque	Torque	
Model	Size	torque T _d [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	resistance class	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	engaging energy E _{ea} ℓ [J]	Readjustment of the air gap ET [J]	pull-in time ta [s]	build-up time t _P [s]	decaying time td [s]	Mass [kg]
112-02-13									6.75×10^{-7}						0.053
112-02-12	02	0.4	DC24	6	0.25	96	В	10000	1.00×10^{-6}	1500	2×10^6	0.004	0.010	0.010	0.057
112-02-11									1.00×10^{-6}						0.057
112-03-13									1.30×10^{-6}						0.072
112-03-12	03	0.6	DC24	6	0.25	96	В	10000	1.95×10^{-6}	2300	3×10^6	0.005	0.012	0.008	0.079
112-03-11									1.95×10^{-6}						0.079
112-04-13									4.38×10^{-6}						0.118
112-04-12	04	1.2	DC24	8	0.33	72	В	10000	6.15×10^{-6}	4500	6×10^6	0.007	0.016	0.010	0.131
112-04-11									6.15×10^{-6}						0.131
112-05-13									9.08×10^{-6}						0.200
112-05-12	05	2.4	DC24	10	0.42	58	В	10000	1.38 × 10 ⁻⁵	9000	9×10^6	0.010	0.023	0.012	0.215
112-05-11									1.38×10^{-5}						0.215

Dimensions (112- □ **-13)**



					1		,											Un	it [mm]
				Radia	l directio	n dimen	sions							Axia	l directio	n dimens	ions		
A ₁	A ₂	A ₃	C ₁	C ₂	C ₃	C ₄	S	V ₁	V ₂	V ₃	Z	Н	K	J ₁	J_2	L	Р	Х	a
28	19.5	10.5	39	33.5	11.4	11	-	2-2.1	2-5.3	2-4	4-90°	13.7	1.5	2.6	1.3	16.1	5	0.8	0.1
32	23	12.5	45	38	13.6	13	33	3-2.6	3-6	3-4.5	6-60°	17	2	3.3	1.3	19.3	6.7	1.2	0.15
40	30	18.5	54	47	20	19	41	3-3.1	3-6	3-5	6-60°	20	2	3.3	1.3	22.8	7	1.6	0.15
50	38	25.5	65	58	27.2	26	51	3-3.1	3-6.5	3-5.5	6-60°	22	2	3.5	1.5	25.2	8	1.6	0.2
	28 32 40	28 19.5 32 23 40 30	28 19.5 10.5 32 23 12.5 40 30 18.5	28 19.5 10.5 39 32 23 12.5 45 40 30 18.5 54	A1 A2 A3 C1 C2 28 19.5 10.5 39 33.5 32 23 12.5 45 38 40 30 18.5 54 47	A1 A2 A3 C1 C2 C3 28 19.5 10.5 39 33.5 11.4 32 23 12.5 45 38 13.6 40 30 18.5 54 47 20	A1 A2 A3 C1 C2 C3 C4 28 19.5 10.5 39 33.5 11.4 11 32 23 12.5 45 38 13.6 13 40 30 18.5 54 47 20 19	28 19.5 10.5 39 33.5 11.4 11 — 32 23 12.5 45 38 13.6 13 33 40 30 18.5 54 47 20 19 41	A1 A2 A3 C1 C2 C3 C4 S V1 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 32 23 12.5 45 38 13.6 13 33 3-2.6 40 30 18.5 54 47 20 19 41 3-3.1	A1 A2 A3 C1 C2 C3 C4 S V1 V2 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 40 30 18.5 54 47 20 19 41 3-3.1 3-6	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60°	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z H 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 13.7 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 17 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60° 20	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z H K 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 13.7 1.5 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 17 2 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60° 20 2	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z H K J1 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 13.7 1.5 2.6 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 17 2 3.3 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60° 20 2 3.3	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z H K J1 J2 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 13.7 1.5 2.6 1.3 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 17 2 3.3 1.3 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60° 20 2 3.3 1.3	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z H K J1 J2 L 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 13.7 1.5 2.6 1.3 16.1 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 17 2 3.3 1.3 19.3 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60° 20 2 3.3 1.3 22.8	A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z H K J1 J2 L P 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 13.7 1.5 2.6 1.3 16.1 5 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 17 2 3.3 1.3 19.3 6.7 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60° 20 2 3.3 1.3 22.8 7	Radial direction dimensions Axial direction dimensions A1 A2 A3 C1 C2 C3 C4 S V1 V2 V3 Z H K J1 J2 L P X 28 19.5 10.5 39 33.5 11.4 11 — 2-2.1 2-5.3 2-4 4-90° 13.7 1.5 2.6 1.3 16.1 5 0.8 32 23 12.5 45 38 13.6 13 33 3-2.6 3-6 3-4.5 6-60° 17 2 3.3 1.3 19.3 6.7 1.2 40 30 18.5 54 47 20 19 41 3-3.1 3-6 3-5 6-60° 20 2 3.3 1.3 22.8 7 1.6

^{*} Size 02 is a rounded flange.

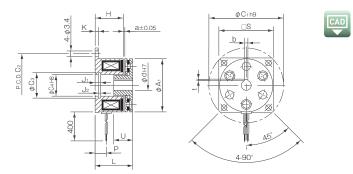
How to Place an Order

112-03-13 24V — Size

^{*} The dynamic friction torque, T_d, is measured at a relative speed of 100 min⁻¹.
* The rotating part moment of inertia and mass are measured for the maximum bore diameter.

^{*} Keep supply voltage fluctuation to within 10% of coil voltage.

Dimensions (112- □ **-12)**



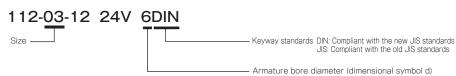
		Sh	aft bore din	ensions	
Size	d	Models com the new JIS	pliant with standards	Models com the old JIS:	pliant with standards
	H7	b P9	t	b E9	t
02	5	_	_		
03	6	$2 \begin{array}{c} -0.006 \\ -0.031 \end{array}$	0.8 + 0.3		
04	8	$2 \begin{array}{c} -0.006 \\ -0.031 \end{array}$	0.8 + 0.3		
04	10	$3 \begin{array}{c} -0.006 \\ -0.031 \end{array}$	1.2 + 0.3	4 + 0.050 + 0.020	1.5 + 0.5
05	10	3 -0.006	1.2 + 0.3	4 + 0.050 + 0.020	1.5 + 0.5
UĐ	15	5 -0.012 -0.042	2 + 0.5	5 + 0.050 + 0.020	2 + 0.5

Unit [mm]

Unit [mm]

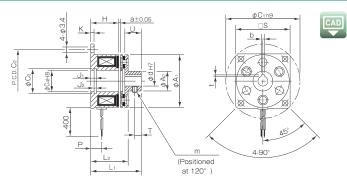
Size		R	adial direction	on dimension	ns				ı	Axial directio	n dimension	s									
Ze	A 1	C ₁	C ₂	C₃	C ₄	S	Н	K	J ₁	J ₂	L	Р	U	a							
02	28	39	33.5	11.4	11	_	13.7	1.5	2.6	1.3	18.1	5	7	0.1							
03	32	45	38	13.6	13	33	17	2	3.3	1.3	21.3	6.7	10	0.15							
04	40	54	47	20	19	41	20	2	3.3	1.3	25.5	7	12	0.15							
05	50	65	58	27.2	26	51	22	2	3.5	1.5	28.2	8	12	0.2							

How to Place an Order



* Models for which there are no keyway standards (models marked by [-]) on the Shaft Bore Dimensions table need not be marked with a keyway standards designation. Products with standards marked by diagonal lines are not set as standard products.

Dimensions (112- ☐ -11)



					Unit [mm]							
		Shaft bore dimensions										
Size	d	Models con the new JIS	ppliant with standards	Models compliant with the old JIS standards								
	Н7	b P9	t	b E9	t							
02	5	_	_									
03	6	2 -0.006 -0.031	0.8 + 0.3									
04	8	$2 \ \ {}^{- 0.006}_{- 0.031}$	0.8 + 0.3									
04	10	3 -0.006	1.2 + 0.3	$4 \ ^{+ \ 0.050}_{+ \ 0.020}$	1.5 + 0.5							
05	10	3 -0.006	1.2 + 0.3	4 + 0.050 + 0.020	1.5 + 0.5							
υĐ	15	5 -0.012 -0.042	2 + 0.5	5 ^{+ 0.050} + 0.020	2 + 0.5							

C003

Size			Radi	ial directio	on dimens	ions			Axial direction dimensions									
ze	A ₁	A ₂	C ₁	C ₂	C ₃	C ₄	S	m	Н	K	J_1	J_2	L ₁	L ₂	Р	U	T	a
02	28	9.5	39	33.5	11.4	11	_	M3	13.7	1.5	2.6	1.3	23.1	18.1	5	7	2.5	0.1
03	32	12	45	38	13.6	13	33	2-M3	17	2	3.3	1.3	29.3	21.3	6.7	10	4	0.15
04	40	17	54	47	20	19	41	2-M3	20	2	3.3	1.3	34.8	25.5	7	12	5	0.15
05	50	24	65	58	27.2	26	51	2-M4	22	2	3.5	1.5	37.2	28.2	8	12	5	0.2

^{*} Size 02 is a rounded flange.

How to Place an Order

To download CAD data or product catalogs:



^{*} Models for which there are no keyway standards (models marked by [-]) on the Shaft Bore Dimensions table need not be marked with a keyway standards designation. Products with standards marked by diagonal lines are not set as standard products.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

LECTROMAGNET	ACTUATED MICRO CLUTCHES & BRAKES
TIC-ACTUATED CLU	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
ПСНЕЅ &	ELECTROMAGNETIC

SPRING-ACTUATED BRAKE

UNITS

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

Unit [mm]

CYT

112

Web code

^{*} The armature hub of size 02 has no keyway. Lock it in place by press-fitting it onto the shaft or the like.

ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES

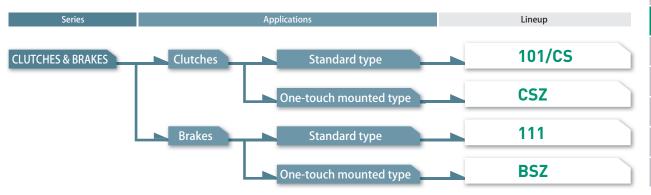
1	I 10	Clutch/	brake torque [N·m] 100
101/CS Models		(5 ~ 320)	
CSZ Models	$(2.4 \sim 10)$		
111 Models		(5 ~ 320)	
BSZ Models	$(2.4 \sim 10)$		
Application	Printing machiner machinery, wrapp	y, bookbindin ing machinery	g machinery, food , textiles machinery

Clutches and Brakes that Accurately Control a Variety of General Industrial Machinery

Clutches accurately connect and release power by being located between the driver and the load. Brakes are used to slow or stop load inertia and machinery and to hold things in stationary positions. Using these basic operations and combining clutches and brakes enable a variety of applications such as stepped speed-changing mechanisms, switching between forward and reverse operation, positioning/indexing, and inching. Part of their appeal is the simplicity of control and ease of maintenance.



Available Models



For details on selection, see P.308 to 315.

Clutches



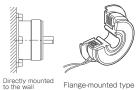


■ Mounting

101

Wall-mounted type

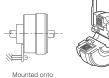
Uses a flange-mounted stator. Designed to be short in the axial direction, requiring less installation space.



CS

Shaft-mounted type

Uses a bearing-mounted stator. Designed to be relatively easy to mount, reducing the processing and work required for mounting.



Bearing-mounted type

■ Shaft Coupling System (Armatures)

101- □ - □ 3, CS- □ - □ 3

Butt and parallel shaft type (Armature type-3)

These incorporate non-armature parts provided by the customer such as V pulleys, enabling use in designs that use either butt shafts or through-shafts.



Armature type-3

101- □ - □ 5, CS- □ - □ 5

Directly coupled type wound around the parallel axis (armature type-5)

Uses an armature assembly designed for use with through-shafts. Ensures that mounting is relatively easy to complete as well as extremely efficient in its approach.



Directly coupled by being wound around the parallel shaft



Armature type-5

101- □ - □ 1, CS- □ - □ 1

Butt type (Armature type-1)

Uses an armature assembly designed for use with butt shafts. May be difficult to mount due to the need for centering and other adjustments, may require the use of a fitting flange, or may require use in combination with flexible couplings.





Armature type-1

Brake



Shaft-mounted type

These use axial braking in most cases, the effectiveness of which depends on how efficiently parts are mounted.



Mounted to the shaft



Armature type-1 Armature type-2

Rotor-mounted type

Uses an armature assembly mounted directly to an inertial body not fastened to the shaft that continues to move even after the shaft has stopped.





Armature type-3

One-touch mounted type

CSZ, BSZ

Designed with the same basic construction as that of the standard type. Comes equipped with a stator armature, eliminating the need for time-consuming gap adjustments. Easy to assemble, guaranteeing dramatic reductions in assembly times.



ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES

ELECTROMAGNETIC **ACTUATED CLUTCHES & BRAKES**

ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

CS

111

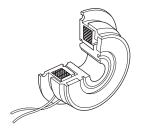
CS7

BSZ

Product Lineup

Electromagnetic-actuated Clutches - Flange-mounted Type





Stator and rotor are combined and directly mounted on stationary parts, such as frames, and fixed in place. These are short in the axial direction and can make effective use of space near windows. Select the armature according to the coupling type used (through-shaft, butt shaft, etc.).

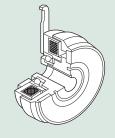
Clutch torque	[N·m]	5 ∼ 320
Operating temperature	[℃]	-10 ~+40
Backlash		Zero

RoHS-compliant

Flange-mounted type

Electromagnetic-actuated Clutches - Bearing-mounted Type





Bearing-mounted type

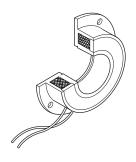
tion shaft by a key. They are designed to be relatively easy to mount, reducing the processing work required for mounting. Clutch torque

These integrate the stator and rotor, which are held to the stationary parts of the machine by a drive pin arm; the rotor is locked to the rota-

Operating temperature [°C] −10 ~+40 Backlash Zero

Electromagnetic-actuated Brakes





Brakes are used to brake and hold rotating bodies. The flange of the stator is locked securely to a strong stationary part. Select an armature that factors in the mounting space available.

Brake torque	[N·m]	5 ∼ 320
Operating temperature	[℃]	-10 ∼+40
Backlash		Zero

RoHS-compliant

CSZ/BSZ Electromagnetic-actuated Clutches & Brakes - One-touch-mounted Type



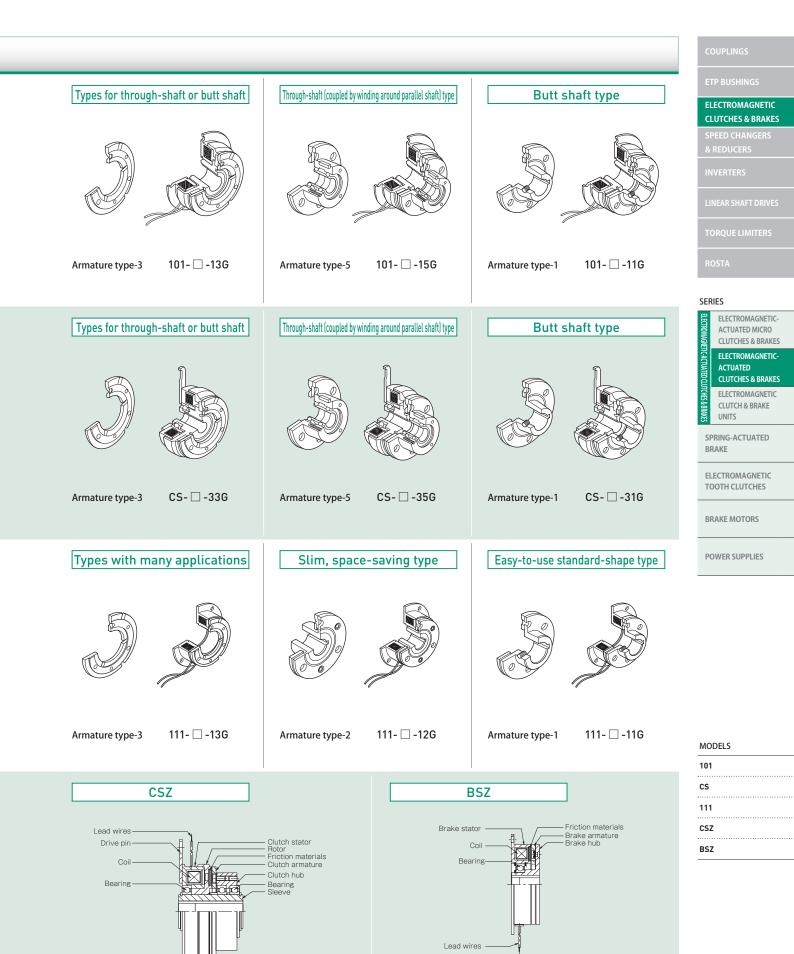




RoHS-compliant

These models adjust the gap to the frictional surface that clutches and brakes require to operate and come pre-assembled. Clutches are simply placed on the shaft and brakes mounted on the flange surface. They do not require gap adjustment or adjustment of concentricity/ parallel misalignment, greatly reducing installation work.

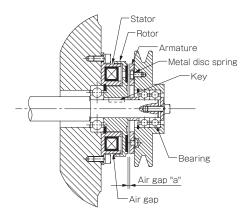
Clutch/brake torque	[N·m]	2.4 ~ 10	
Operating temperature	[℃]	−10 ~+40	
Backlash		Zero	



Mounting Example

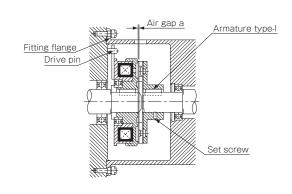
■ Flange-mounting example with 101

The stator is directly mounted on a stationary part, such as a frame, by a mounting flange, and fixed in place. The rotor is locked to the rotation shaft using a key. The stator and rotor are combined via a narrow air gap that serves as part of the magnetic circuit to form a magnetic pole.



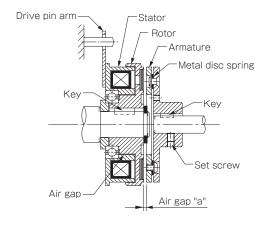
■Butt shaft mounting example with CS

In designs that use butt shafts, the two shafts can be reliably centered using fitting flanges, as shown in the figure.



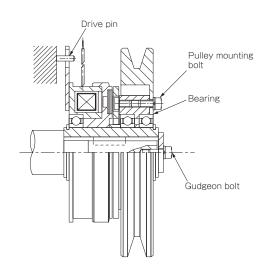
Bearing-mounting example with CS

The stator is integrated with the rotor via a bearing and held to the stationary parts of the machine by a drive pin arm. The rotor is locked to the rotation shaft using a set screw. The stator and rotor form a magnetic pole via the bearing.



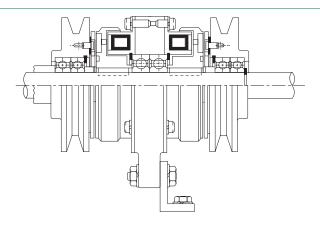
■ Mounting example with CSZ

Simply insert the shaft in the sleeve and fasten a CSZ on the shaft end and mounting is complete.



■ Example of combining clutches

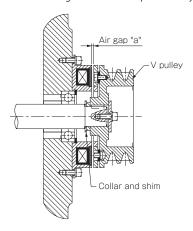
In this example, two clutches are assembled on a through-shaft. This is very effective when controls such as two-step speed changing and forward/reverse operation are needed and space is limited.



Mounting Example

■Armature type-3 mounting example with 111

When armature type-3 is directly mounted on the end face of a V pulley, no armature hub is needed, making for a very efficient design. These are optimal when space is limited or when a shaft overhangs from a wall and the overhang load must be kept extremely low.

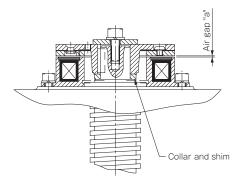


■Armature type-2 mounting example on vertical shaft with 111

Armature type-2 is a special armature that puts the boss part of the armature hub into the space within the stator. That makes it compact. It is short in the axial direction even when a pulley or the like is installed on the tip of the brake. Since running torque is zero, it does not take up space even when mounted on a vertical shaft, and is also easy to install.

Air gap "a" can be set easily using collars and shims.

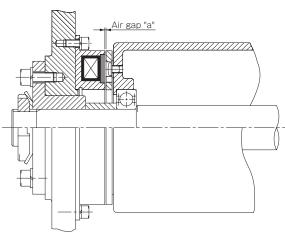
Corrections are easily accomplished by adding or removing shims.



■Armature type-3 mounting example with 111

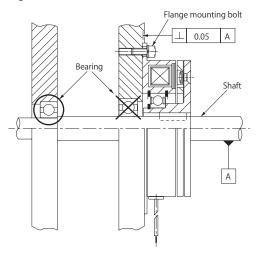
If a rotating body floating above a shaft by means of a bearing (an idler pulley, guide roller, or the like) has an armature type-3 mounted on it directly, it can be assembled easily without taking up a lot of space. Air gap "a" can be set easily using collars and shims.

Corrections are easily accomplished by adding or removing shims.



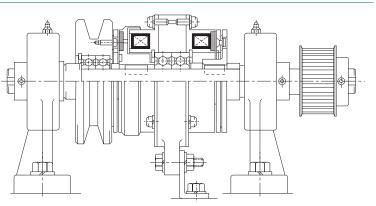
■ Mounting example with BSZ

Simply insert onto the shaft to be braked and lock the BSZ on the wall surface and mounting is complete. Be careful when designing that the mounting shaft does not cantilever and end up a three-point



■ Example of combining clutches and brakes

In this example, a clutch and brake are assembled on a through-shaft. This is effective when mounting space is limited or when there is no wall on which to mount the stator.



ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES ELECTROMAGNETIC ACTUATED

CLUTCHES & BRAKES ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

101

CS

111

CSZ

BSZ

101 Models Electromagnetic Clutches - Flange-mounted Type

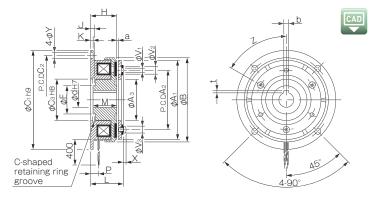
Specifications

		Dvnamic	Static		Coil (at	20℃)		7	Max.	Rotating part mo	oment of inertia J	Total work		Torque	Torque	
Model	Size	friction torque Ta [N·m]	friction torque Ts [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat resistance class	rotation speed [min ⁻¹]	Rotor [kg·m²]	Armature [kg·m²]	performed until readjustment of the air gap E _T [J]	Armature pull-in time t _a [s]	build-up time t _p [s]	decaying time ta [s]	Mass [kg]
101-06-13G											4.23×10^{-5}					0.46
101-06-15G	06	5	5.5	DC24	11	0.46	52	В	8000	7.35×10^{-5}	1.05×10^{-4}	36×10^6	0.020	0.041	0.020	0.66
101-06-11G											6.03×10^{-5}					0.5
101-08-13G											1.18×10^{-4}					0.83
101-08-15G	80	10	11	DC24	15	0.63	38	В	6000	2.24×10^{-4}	3.00×10^{-4}	60×10^{6}	0.023	0.051	0.030	1.19
101-08-11G											1.71×10^{-4}					0.91
101-10-13G											4.78×10^{-4}					1.5
101-10-15G	10	20	22	DC24	20	0.83	29	В	5000	6.78×10^{-4}	9.45×10^{-4}	130×10^{6}	0.025	0.063	0.050	2.11
101-10-11G											6.63×10^{-4}					1.66
101-12-13G											1.31×10^{-3}					2.76
101-12-15G	12	40	45	DC24	25	1.09	23	В	4000	2.14×10^{-3}	2.75×10^{-3}	250×10^{6}	0.040	0.115	0.065	3.8
101-12-11G											1.81×10^{-3}					3.05
101-16-13G											4.80×10^{-3}					5.1
101-16-15G	16	80	90	DC24	35	1.46	16	В	3000	6.30×10^{-3}	9.05×10^{-3}	470×10^{6}	0.050	0.160	0.085	6.9
101-16-11G											6.35×10^{-3}					5.4
101-20-13G											1.37×10^{-2}					9.3
101-20-15G	20	160	175	DC24	45	1.88	13	В	2500	1.93×10^{-2}	2.65×10^{-2}	10 × 10 ⁸	0.090	0.250	0.130	13
101-20-11G											1.90×10^{-2}					10.5
101-25-13G											3.58×10^{-2}					17
101-25-15G	25	320	350	DC24	60	2.5	9.6	В	2000	4.48×10^{-2}	7.45×10^{-2}	20×10^{8}	0.115	0.335	0.210	23.6
101-25-11G											4.83×10^{-2}					18.7

^{*} The dynamic friction torque, Td, is measured at a relative speed of 100 min-1.

Dimensions (101- ☐ -13G)

(For direct mounting)



									-
			S	haft bo	ore din	nensi	ons		
Size	d	Mod	els comp new JIS	oliant w standar	ith the ds	Mode	els comp old JIS s	oliant w tandar	ith the
	H7	- 1) P9		t	ŀ) E9	1	t
06	12	4	- 0.012 - 0.042	1.5	+ 0.5 0	4	+ 0.050 + 0.020	1.5	+ 0.5 0
UO	15	5	- 0.012 - 0.042	2	+ 0.5	5	+ 0.050 + 0.020	2	+ 0.5
08	15	5	- 0.012 - 0.042	2	+ 0.5 0	5	+ 0.050 + 0.020	2	+ 0.5 0
UO	20	6	- 0.012 - 0.042	2.5	+ 0.5	5	+ 0.050 + 0.020	2	+ 0.5
10	20	6	- 0.012 - 0.042	2.5	+ 0.5	5	+ 0.050 + 0.020	2	+ 0.5 0
10	25	8	- 0.015 - 0.051	3	+ 0.5	7	+ 0.061 + 0.025	3	+ 0.5
12	25	8	- 0.015 - 0.051	3	+ 0.5	7	+ 0.061 + 0.025	3	+ 0.5
12	30	8	- 0.015 - 0.051	3	+ 0.5 0	7	+ 0.061 + 0.025	3	+ 0.5 0
16	30	8	- 0.015 - 0.051	3	+ 0.5	7	+ 0.061 + 0.025	3	+ 0.5
10	40	12	- 0.018 - 0.061	3	+ 0.5 0	10	+ 0.061 + 0.025	3.5	+ 0.5 0
20	40	12	- 0.018 - 0.061	3	+ 0.5	10	+ 0.061 + 0.025	3.5	+ 0.5
20	50	14	- 0.018 - 0.061	3.5	+ 0.5 0	12	+ 0.075 + 0.032	3.5	+ 0.5 0
25	50	14	- 0.018 - 0.061	3.5	+ 0.5	12	+ 0.075 + 0.032	3.5	+ 0.5
25	60	18	- 0.018 - 0.061	4	+ 0.5 0	15	+ 0.075 + 0.032	5	+ 0.5 0

Unit [mm]

																					Unit [mm]
Size						Radia	l directi	ion dime	ensions					Axial direction dimensions							
Ze	A 1	A ₂	A ₃	В	C ₁	C ₂	C ₃	F	V ₁	V ₂	V ₃	Υ	Z	Н	J	K	L	М	Р	Х	a
06	63	46	34.5	67.5	80	72	35	23	3-3.1	3-6.3	3-5.5	5	6-60°	24	3.5	2.1	28	22	7.3	2.5	$0.2 \ \pm 0.05$
08	80	60	41.5	85	100	90	42	28.5	3-4.1	3-8	3-7	6	6-60°	26.5	4.3	2.6	31	24	8.3	2.85	0.2 ± 0.05
10	100	76	51.5	106	125	112	52	40	3-5.1	3-10.5	3-9	7	6-60°	30	5	3.1	36	27	9	3.3	0.2 ± 0.05
12	125	95	61.5	133	150	137	62	45	3-6.1	3-12	3-11	7	6-60°	33.5	5.5	3.6	40.5	30	9.3	3.3	$0.3^{+0.05}_{-0.1}$
16	160	120	79.5	169	190	175	80	62	3-8.1	3-15	3-14	9.5	6-60°	37.5	6	4.1	46.5	34	11.7	3.5	$0.3^{+0.05}_{-0.1}$
20	200	158	99.5	212.5	230	215	100	77	3-10.2	3-18	3-17	9.5	6-60°	44	7	5.1	55.5	40	13.4	4.9	0.5 _0.2
25	250	210	124.5	264	290	270	125	100	4-12.2	4-22	4-20	11.5	8-45°	51	8	6.1	64	47	16	5.5	0.5 _0.2

How to Place an Order

101-06-13G 24V 12DIN Size —

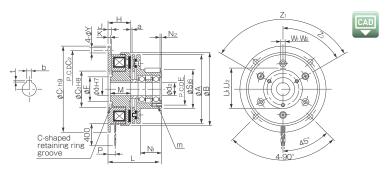
Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards

-Rotor bore diameter (dimensional symbol d)

^{*} The rotating part moment of inertia and mass are measured for the maximum bore diameter.

Dimensions (101- □ -15G)

(For through-shafts)



						Unit [mm]
			Shaf	t bore dimer	nsions	
Size	d ₁	d ₂	Models complia JIS stai		Models complia JIS star	
	H7	u2	b P9	t	b E9	t
06	12	12	4 -0.012	1.5 + 0.5	4 + 0.050 + 0.020	1.5 + 0.5
08	15	15	5 -0.012	2 + 0.5	5 + 0.050 + 0.020	2 + 0.5
10	20	20	6 -0.012	2.5 + 0.5	5 + 0.050 + 0.020	2 + 0.5
12	25	25	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	30	30	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
20	40	40	12 -0.018	3 + 0.5	10 + 0.061 + 0.025	3.5 + 0.5
25	50	50	14 -0.018	3.5 + 0.5	12 + 0.075 + 0.032	3.5 + 0.5

Unit [mm]

Size				Rad	iial dir	rection	dime	nsions	ة									Axia	l direc	tion di	mens	ions			
ze	Α	В	C ₁	C ₂	C ₃	E	F	Υ	S	Z ₁	Z ₂	Н	J	K	L	M	N ₁	N_2	Р	U ₁	W_1	U ₂	W_2	a	m
06	63	67.5	80	72	35	33	23	5	38	3-120°	60°	24	3.5	2.1	51.5	22	20	2	7.3	39.5	4	39.5	4	0.2 ±0.05	$3-M4 \times 0.7$, length: 4
08	80	85	100	90	42	37	28.5	6	45	3-120°	60°	26.5	4.3	2.6	60	24	25	2	8.3	47	5	47	5	0.2 ± 0.05	$3-M4 \times 0.7$, length: 6
10	100	106	125	112	52	47	40	7	55	4-90°	45°	30	5	3.1	71	27	30	3	9	57	5	57.5	6	0.2 ± 0.05	$4\text{-M4} \times 0.7$, length: 8
12	125	133	150	137	62	52	45	7	64	4-90°	45°	33.5	5.5	3.6	86.5	30	40	2	9.3	67	7	67	8	0.3 + 0.05	$4\text{-M4} \times 0.7$, length: 8
16	160	169	190	175	80	62	62	9.5	75	6-60°	30°	37.5	6	4.1	103.5	34	50	3	11.7	78	7	78	8	$0.3^{+0.05}_{-0.1}$	$6\text{-M5} \times 0.8$, length: 8
20	200	212.5	230	215	100	74.5	77	9.5	90	4-90°	45°	44	7	5.1	124.5	40	60	5	13.4	93.5	10	93	10	0.5 -0.2	4-M6 × 1, length: 12
25	250	264	290	270	125	101.5	100	11.5	115	8-45°	22.5°	51	8	6.1	145	47	70	6	16	118.5	12	118	12	0.5 _0.2	8-M6 × 1, length: 12

How to Place an Order

101-06-15G 24V R12DIN A12JIS

Armature type-5 keyway standards Dimensional symbol U2, W2: Compliant with the new JIS standards: DIN Dimensional symbol U1, W1: Compliant with the old JIS standards: JIS Armature bore diameter (dimensional symbol d2)

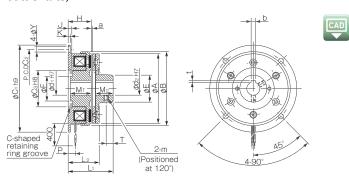
Keyway standards DIN: Compliant with the new JIS standards

Rotor bore diameter (dimensional symbol d1) -

JIS: Compliant with the old JIS standards

Dimensions (101- ☐ -11G)

(For butt shafts)



Radial direction di

						Unit [mm]
			Shaft	bore dimer	nsions	
Size	d ₁	d ₂	Models complia JIS star	nt with the new ndards	Models complia	ant with the old ndards
	H7	H7	b P9	t	b E9	t
06	12	12	4 -0.012	1.5 + 0.5	4 ^{+ 0.050} + 0.020	1.5 + 0.5
00	15	15	5 -0.012	2 + 0.5	5 ^{+ 0.050} + 0.020	2 + 0.5
08	15	15	5 -0.012	2 + 0.5	5 ^{+ 0.050} + 0.020	2 + 0.5
08	20	20	6 -0.012	2.5 + 0.5	5 + 0.050 + 0.020	2 + 0.5
10	20	20	6 -0.012	2.5 + 0.5	5 + 0.050 + 0.020	2 + 0.5
10	25	25	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
12	25	25	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
12	30	30	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	30	30	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
10	40	40	$12 \begin{array}{c} -0.018 \\ -0.061 \end{array}$	3 + 0.5	10 + 0.061 + 0.025	3.5 + 0.5
20	40	40	12 -0.018	3 + 0.5	10 + 0.061 + 0.025	3.5 + 0.5
20	50	50	14 - 0.018	3.5 + 0.5	12 + 0.075 + 0.032	3.5 + 0.5
25	50	50	14 -0.018	3.5 + 0.5	12 + 0.075 + 0.032	3.5 + 0.5
23	60	60	18 -0.018	4 + 0.5	15 + 0.075 + 0.032	5 + 0.5

imension	s					A	cial direct	ion dime	nsions			
Е	Е	v	 ш	1	V	1	1	NA.	NA.	D	т	_

Web code

<u>S:</u>			- 1	Radial dir	ection di	mension	s						A	cial direct	ion dime	nsions			
ze	Α	В	C ₁	C ₂	C₃	E	F	Υ	m	Н	J	K	L ₁	L ₂	M ₁	M ₂	Р	T	a
06	63	67.5	80	72	35	26	23	5	M4	24	3.5	2.1	43	31.5	22	15	7.3	6	0.2 ± 0.05
08	80	85	100	90	42	31	28.5	6	M5	26.5	4.3	2.6	51	35	24	20	8.3	8	0.2 ± 0.05
10	100	106	125	112	52	41	40	7	M5	30	5	3.1	61	41	27	25	9	10	0.2 ± 0.05
12	125	133	150	137	62	49	45	7	M6	33.5	5.5	3.6	70.5	46.5	30	30	9.3	12	0.3 + 0.05
16	160	169	190	175	80	65	62	9.5	M8	37.5	6	4.1	84.5	53.5	34	38	11.7	15	0.3 + 0.05
20	200	212.5	230	215	100	83	77	9.5	M8	44	7	5.1	100.5	64.5	40	45	13.4	18	0.5 0
25	250	264	290	270	125	105	100	11.5	M10	51	8	6.1	118	75	47	54	16	22	0.5 0 0 0 0 0 0

How to Place an Order

101-06-11G 24V R12DIN A12DIN

Rotor bore diameter (dimensional symbol d1) -

Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards

Armature bore diameter (dimensional symbol d2) Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards

C004

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC

ACTUATED

CLUTCHES & BRAKES ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

CS 111

BSZ

CSZ

Unit [mm]

CS Models Electromagnetic Clutches - Bearing-mounted Type

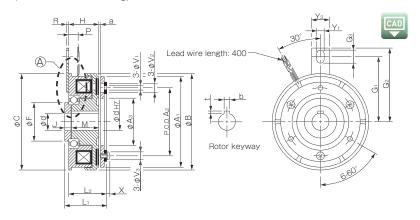
Specifications

		Dvnamic	Static		Coil (at	20°C)			Max.	Rotating part mo	ment of inertia J	Total work performed		Torque	Torque	
Model	Size	friction torque Td [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance $[\Omega]$	Heat resistance class	rotation speed [min ⁻¹]	Rotor [kg·m²]	Armature [kg·m²]	until readjustment of the air gap E _T [J]	Armature pull-in time ta [s]	build-up time tp [s]	decaying time td [s]	Mass [kg]
CS-06-33G											4.23×10^{-5}					0.50
CS-06-35G	06	5	5.5	DC24	11	0.46	52	В	3000	7.35×10^{-5}	1.05×10^{-4}	36×10^6	0.020	0.041	0.020	0.70
CS-06-31G											6.03×10^{-5}					0.54
CS-08-33G											1.18×10^{-4}					0.87
CS-08-35G	08	10	11	DC24	15	0.63	38	В	3000	2.24×10^{-4}	3.00×10^{-4}	60×10^{6}	0.023	0.051	0.030	1.23
CS-08-31G											1.71×10^{-4}					0.95
CS-10-33G											4.78×10^{-4}					1.57
CS-10-35G	10	20	22	DC24	20	0.83	29	В	3000	6.78×10^{-4}	9.45×10^{-4}	130×10^{6}	0.025	0.063	0.050	2.18
CS-10-31G											6.63×10^{-4}					1.73
CS-12-33G											1.31×10^{-3}					2.89
CS-12-35G	12	40	45	DC24	25	1.09	23	В	2000	2.14×10^{-3}	2.75×10^{-3}	250×10^{6}	0.040	0.115	0.065	3.93
CS-12-31G											1.81×10^{-3}					3.18
CS-16-33G											4.80×10^{-3}					5.3
CS-16-35G	16	80	90	DC24	35	1.46	16	В	2000	6.30×10^{-3}	9.05×10^{-3}	470×10^6	0.050	0.160	0.085	7.1
CS-16-31G											6.35×10^{-3}					5.6
CS-20-33G	20	160	175	DC24	45	1.88	13	В	1500	1.93×10^{-2}	1.37×10^{-2}	10×10^{8}	0.090	0.250	0.130	9.8
CS-25-33G	25	320	350	DC24	72	3.00	8	В	1500	4.48×10^{-2}	3.58×10^{-2}	20×10^8	0.115	0.335	0.210	17.5

 $^{^{\}ast}$ The dynamic friction torque, Td, is measured at a relative speed of 100 min 1

Dimensions (CS- ☐ -33G)

(For direct mounting)



					Unit [mm]
		Sł	naft bore din	nensions	
Size	d н7	Models complia JIS star	nt with the new ndards	Models complia JIS star	int with the old indards
	u H/	b P9	t	b E9	t
06	12	4 - 0.012	1.5 + 0.5	4 + 0.050 + 0.020	1.5 + 0.5
08	15	5 -0.012	2 + 0.5	5 ^{+0.050} _{+0.020}	2 + 0.5
10	20	6 - 0.012	2.5 + 0.5	5 + 0.050 + 0.020	2 + 0.5
12	25	8 - 0.015 - 0.051	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	30	8 -0.015	3 + 0.5	$7 \begin{array}{c} +0.061 \\ +0.025 \end{array}$	3 + 0.5
20	40	12 -0.018	3 + 0.5	10 +0.061 +0.025	3.5 + 0.5
25	50	14 -0.018	3.5 + 0.5	12 + 0.075 + 0.032	3.5 + 0.5



Size	L ₃
20	9
25	6.8

Unit [mm]

^{*}On sizes 20 and 25, the head of the bolt for pressing down the bearing will stick out. See the above dimensions

Size						Radial	directio	on dime	nsions									Axial di	rection	dimens	ions		
ze	A ₁	A ₂	A ₃	В	C	F	G ₁	G ₂	G₃	V ₁	V ₂	V ₃	Y ₁	Y ₂	Н	L ₁	L ₂	М	J	Р	R	Х	a
06	63	46	34.5	67.5	67.5	24	42.5	50	9.5	3.1	6.3	5.5	4.5	14	24	31	28	22	5	7.3	2	2.5	0.2 ± 0.05
08	80	60	41.5	85	85	34	57.5	65	11.5	4.1	8	7	6.5	16	26.5	34.5	31	24	6	8.3	2	2.85	0.2 ± 0.05
10	100	76	51.5	106	106	40	62.5	70	11.5	5.1	10.5	9	6.5	16	30	39.5	36	27	6.5	9	2	3.3	0.2 ± 0.05
12	125	95	61.5	133	133	45	77.5	85	11.5	6.1	12	11	6.5	16	33.5	44.5	40.5	30	7.5	9.3	2	3.3	$0.3^{+0.05}_{-0.1}$
16	160	120	79.5	169	169	58	100	112	18.5	8.1	15	14	8.5	25	37.5	50.5	46.5	34	7.5	11.7	3.2	3.5	$0.3 \begin{array}{c} +0.05 \\ -0.1 \end{array}$
20	200	158	99.5	212.5	212	75	125	138	18.5	10.2	18	16.2	8.5	25	44	60.5	55.5	40	9	13.4	3	5	$0.5_{-0.2}^{0}$
25	250	210	124.5	264	250	100	155	173	24	12.2	22	20	12	30	53	69	66	47	9	18	6	4.5	0.5 _0.2
		111																					

^{*} The $V_1, \, V_2, \, \text{and} \, \, V_3$ dimensions of size 25 are located in four places 90° apart.

How to Place an Order

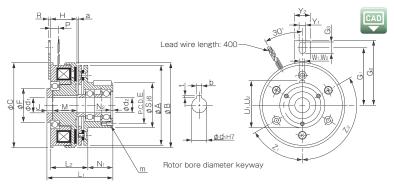


Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards

^{*} The moment of inertia of a rotating body and mass are measured for the maximum bore diameter.

Dimensions (CS- ☐ -35G)

(For through-shafts)



						Unit [mm]
			Shaf	t bore dimer	nsions	
Size	d ₁	d ₂	Models complia JIS sta	nt with the new ndards	Models complia	ent with the old endards
	H7	u ₂	b P9	t	b E9	t
06	12	12	4 -0.012	1.5 + 0.5	4 + 0.050 + 0.020	1.5 + 0.5
80	15	15	5 -0.012 -0.042	2 + 0.5	5 ^{+ 0.050} + 0.020	2 + 0.5
10	20	20	6 -0.012	2.5 + 0.5	5 + 0.050 + 0.020	2 + 0.5
12	25	25	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	30	30	8 -0.015 -0.051	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5

		-			-																							Unit [mm]
Size					Radi	al dire	ction	dime	nsion	S										- 1	Axial d	lirect	ion di	mens	ions			
ze	Α	В	C	Ε	F	G_1	G ₂	G ₃	S	Y ₁	Y ₂	Z ₁	\mathbf{Z}_2	Н	L ₁	L ₂	M	J	N_1	N ₂	Р	R	U ₁	\mathbf{W}_1	U ₂	W_2	a	m
06	63	67.5	67.5	33	24	42.5	50	9.5	38	4.5	14	3-120°	0°	24	54.5	31.5	22	5	20	2	7.3	2	39.5	4	39.5	4	0.2 ± 0.05	3-M4 × 0.7, length: 4
08	80	85	85	37	34	57.5	65	11.5	45	6.5	16	3-120°	0°	26.5	63.5	35	24	6	25	2	8.3	2	47	5	47	5	0.2 ±0.05	$3-M4 \times 0.7$, length: 6
10	100	106	106	47	40	62.5	70	11.5	55	6.5	16	4-90°	45°	30	74.5	41	27	6.5	30	3	9	2	57	5	57.5	6	0.2 ± 0.05	4-M4 × 0.7, length: 8
12	125	133	133	52	45	77.5	85	11.5	64	6.5	16	4-90°	45°	33.5	90.5	46.5	30	7.5	40	2	9.3	2	67	7	67	8	$0.3^{+0.05}_{-0.1}$	4-M4 $ imes$ 0.7, length: 8
16	160	169	169	62	58	100	112	18.5	75	8.5	25	6-60°	30°	37.5	107.5	53.5	34	7.5	50	3	11.7	3.2	78	7	78	8	$0.3^{+0.05}_{-0.1}$	6-M5 × 0.8, length: 8

How to Place an Order

CS-06-35G 24V R12DIN A12JIS

Armature type-5 keyway standards Dimensional symbol U2, W2: Compliant with the new JIS standards: DIN Dimensional symbol U1, W1: Compliant with the old JIS standards: JIS

Armature bore diameter (dimensional symbol d2)

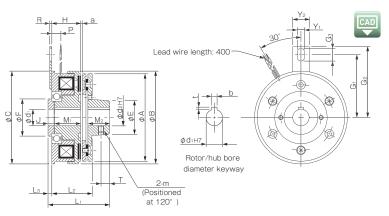
new JIS standards
JIS: Compliant with the old JIS standards

Rotor bore diameter (dimensional symbol)

Keyway standards DIN: Compliant with the

Dimensions (CS- ☐ -31G)

(For butt shafts)



						Unit [mm]
			Shaf	t bore dimer	nsions	
Size	d ₁	d ₂	Models com the new JIS	pliant with standards	Models com the old JIS	pliant with standards
	H7	H7	b P9	t	b E9	t
06	12	12	$4 \ \ {}^{- 0.012}_{- 0.042}$	1.5 + 0.5	4 + 0.050 + 0.020	1.5 + 0.5
08	15	15	5 -0.012	2 + 0.5	5 + 0.050 + 0.020	2 + 0.5
10	20	20	$\begin{array}{cc} -0.012 \\ -0.042 \end{array}$	2.5 + 0.5	5 ^{+ 0.050} + 0.020	2 + 0.5
12	25	25	8 -0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	30	30	8 -0.015 -0.051	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	30	30		-		-

Size				Ra	dial dir	ection d	imensio	ns								Axial di	rection	dimens	ions			
ze	Α	В	С	E	F	G ₁	G ₂	G₃	Y ₁	Y ₂	m	Н	L ₁	L ₂	L ₃	M ₁	M ₂	J	Р	R	T	a
06	63	67.5	67.5	26	24	42.5	50	9.5	4.5	14	M4	24	46	31.5	3	22	15	5	7.3	2	6	0.2 ±0.05
08	80	85	85	31	34	57.5	65	11.5	6.5	16	M5	26.5	54.5	35	3.5	24	20	6	8.3	2	8	0.2 ±0.05
10	100	106	106	41	40	62.5	70	11.5	6.5	16	M5	30	64.5	41	3.5	27	25	6.5	9	2	10	0.2 ±0.05
12	125	133	133	49	45	77.5	85	11.5	6.5	16	M6	33.5	74.5	46.5	4	30	30	7.5	9.3	2	12	$0.3^{+0.05}_{-0.1}$
16	160	169	169	65	58	100	112	18.5	8.5	25	M8	37.5	88.5	53.5	4	34	38	7.5	11.7	3.2	15	0.3 + 0.05

How to Place an Order

To download CAD data or product catalogs:

CS-06-31G 24V R12DIN A12DIN

Size Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards Rotor bore diameter (dimensional symbol d1) -

Web code

· Armature bore diameter (dimensional symbol d2) Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards

C004

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES

ELECTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC

CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

Unit [mm]

Unit [mm]

CS

CSZ BSZ

MODELS

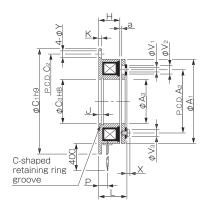
111

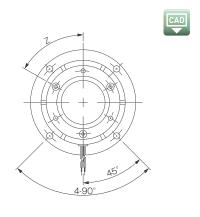
111 Models **Electromagnetic Brakes**

Specifications

		Dynamic friction	Static friction		Coil (at	20℃)		Heat	Max.	Armature	Total work performed	Armature	Torque	Torque	
Model	Size	torque Td [N·m]	torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	resistance	rotation speed [min ⁻¹]	Moment of inertia J [kg·m²]	until readjustment of the air gap ET [J]	pull-in time ta [s]	rise time t _p [s]	extinction time td[s]	Mass [kg]
111-06-13G										4.23×10^{-5}					0.28
111-06-12G	06	5	5.5	DC24	11	0.46	52	В	8000	6.03×10^{-5}	36×10^{6}	0.015	0.033	0.015	0.32
111-06-11G										6.03×10^{-5}					0.32
111-08-13G										1.18×10^{-4}					0.5
111-08-12G	80	10	11	DC24	15	0.63	38	В	6000	1.71×10^{-4}	60×10^{6}	0.016	0.042	0.025	0.58
111-08-11G										1.71×10^{-4}					0.58
111-10-13G										4.78×10^{-4}					0.91
111-10-12G	10	20	22	DC24	20	0.83	29	В	5000	6.63×10^{-4}	130×10^{6}	0.018	0.056	0.030	1.07
111-10-11G										6.63 × 10 ⁻⁴					1.07
111-12-13G										1.31×10^{-3}					1.68
111-12-12G	12	40	45	DC24	25	1.09	23	В	4000	1.81×10^{-3}	250×10^{6}	0.027	0.090	0.050	1.97
111-12-11G										1.81×10^{-3}					1.97
111-16-13G	16	00	90	DC24	35	1.46	16	D	2000	4.80×10^{-3}	470 > 106	0.035	0.127	0.055	3.15
111-16-12G	16	80	90	DC24	35	1.46	16	В	3000	6.35×10^{-3}	470×10^{6}	0.035	0.127	0.055	3.45
111-16-11G										6.35×10^{-3}					3.45
111-20-13G 111-20-12G	20	160	175	DC24	45	1.88	13	В	2500	1.37×10^{-2} 1.90×10^{-2}	10 × 10 ⁸	0.065	0.200	0.070	5.9 7.1
111-20-126 111-20-11G	20	100	1/3	DC24	43	1.00	13	Ь	2300	1.90×10^{-2} 1.90×10^{-2}	10 × 10	0.003	0.200	0.070	7.1
111-20-11G 111-25-13G										1.90×10^{-2} 3.58×10^{-2}					10.5
111-25-13G 111-25-12G	25	320	350	DC24	60	2.5	9.6	В	2000	4.83×10^{-2}	20 × 10 ⁸	0.085	0.275	0.125	12.2
111-25-126 111-25-11G	23	320	550	DC24	00	2.3	7.0	J	2000	4.83×10^{-2}	20 / 10	0.005	0.273	0.123	12.2
111-23-110										7.05 /\ 10					12.2

Dimensions (111- □ **-13G)**





Un	it	ſπ	۱n

Size					Ra	adial dire	ction dime	nsions						Axial dire	ection dir	nensions		
Ze	A ₁	A ₂	A ₃	C ₁	C ₂	C ₃	V ₁	V ₂	V ₃	Υ	Z	Н	J	K	L	P	Х	a
06	63	46	34.5	80	72	35	3-3.1	3-6.3	3-5.5	5	6-60°	18	3.5	2.1	22	7.3	2.5	$\textbf{0.2} \pm \textbf{0.05}$
80	80	60	41.5	100	90	42	3-4.1	3-8	3-7	6	6-60°	20	4.3	2.6	24.5	8.3	2.85	0.2 ± 0.05
10	100	76	51.5	125	112	52	3-5.1	3-10.5	3-9	7	6-60°	22	5	3.1	28	9	3.3	$\textbf{0.2} \pm \textbf{0.05}$
12	125	95	61.5	150	137	62	3-6.1	3-12	3-11	7	6-60°	24	5.5	3.6	31	9.3	3.3	$0.3^{+0.05}_{-0.1}$
16	160	120	79.5	190	175	80	3-8.1	3-15	3-13	9.5	6-60°	26	6	4.1	35	11.7	3.5	$0.3^{+0.05}_{-0.1}$
20	200	158	99.5	230	215	100	3-10.2	3-18	3-17	9.5	6-60°	30	7	5.1	41.5	13.4	4.9	$0.5^{-0}_{-0.2}$
25	250	210	124.5	290	270	125	4-12.2	4-22	4-20	11.5	8-45°	35	8	6.1	48	16	5.5	$0.5^{-0}_{-0.2}$

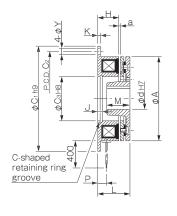
How to Place an Order

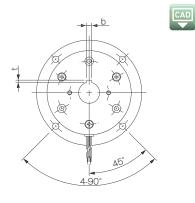
111-06-13G 24V Size -

^{*} The dynamic friction torque, T_d, is measured at a relative speed of 100 min¹.
* The rotating part moment of inertia and mass are measured for the maximum bore diameter.

ELECTROMAGNETIC **CLUTCHES & BRAKES**

Dimensions (111- □ **-12G)**





					· []
		Sha	ft bore dim	ensions	
Size	d H7	Models complia JIS star	nt with the new ndards	Models complia	ant with the old ndards
	u n/	b P9	t	b E9	t
٠,	12	4 - 0.012	1.5 + 0.5	4 + 0.050 + 0.020	1.5 + 0.5
06	15	5 - 0.012	2 + 0.5	5 ^{+0.050} _{+0.020}	2 + 0.5
	15	5 - 0.012	2 + 0.5	5 + 0.050 + 0.020	2 + 0.5
80	20	6 - 0.012	2.5 + 0.5	5 + 0.050 + 0.020	2 + 0.5
10	20	6 - 0.012	2.5 + 0.5	5 ^{+0.050} _{+0.020}	2 + 0.5
10	25	8 - 0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
10	25	8 - 0.015	3 + 0.5	7 +0.061 +0.025	3 + 0.5
12	30	8 - 0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
47	30	8 - 0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	40	$12 {}^{- 0.018}_{- 0.061}$	3 + 0.5	10 +0.061 +0.025	3.5 + 0.5
	40	12 - 0.018	3 + 0.5	10 + 0.061 + 0.025	3.5 + 0.5
20	50	14 - 0.018	3.5 + 0.5	$12^{+0.075}_{+0.032}$	3.5 + 0.5
25	50	14 - 0.018 - 0.061	3.5 + 0.5	12 + 0.075 + 0.032	3.5 + 0.5
25	60	$18 {}^{- 0.018}_{- 0.061}$	4 + 0.5	15 +0.075 +0.032	5 + 0.5

Unit [mm]	SEI
	=

Unit [mm]

SERIES ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

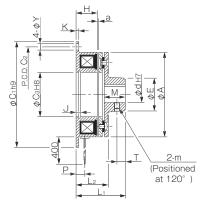
POWER SUPPLIES

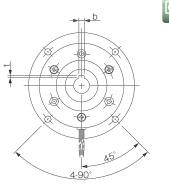
Size		Radial	direction dime	nsions				Axial d	irection dimens	ions		
Size	Α	C ₁	C ₂	C₃	Υ	Н	J	К	L	M	P	a
06	63	80	72	35	5	18	3.5	2.1	25.5	15	7.3	0.2 ± 0.05
08	80	100	90	42	6	20	4.3	2.6	28.5	20	8.3	0.2 ± 0.05
10	100	125	112	52	7	22	5	3.1	33	25	9	0.2 ± 0.05
12	125	150	137	62	7	24	5.5	3.6	37	30	9.3	0.3 + 0.05
16	160	190	175	80	9.5	26	6	4.1	42	38	11.7	0.3 + 0.05
20	200	230	215	100	9.5	30	7	5.1	50.5	45	13.4	0.5 _0.2
25	250	290	270	125	11.5	35	8	6.1	59	54	16	0.5 -0.2

How to Place an Order

111-06-12G 24V 12DIN - Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards Armature bore diameter (dimensional symbol d)

Dimensions (111- ☐ -11G)





					Unit [mm]
		Sha	ft bore dim	ensions	
Size	d H7		nt with the new ndards	Models complia	ant with the old ndards
	u H/	b P9	t	b E9	t
06	12	4 - 0.012	1.5 + 0.5	4 + 0.050 + 0.020	1.5 + 0.5
06	15	5 - 0.012	2 + 0.5	5 +0.050 +0.020	2 + 0.5
08	15	5 - 0.012	2 + 0.5	5 + 0.050 + 0.020	2 + 0.5
08	20	6 - 0.012	2.5 + 0.5	5 +0.050 +0.020	2 + 0.5
40	20	6 - 0.012	2.5 + 0.5	5 + 0.050 + 0.020	2 + 0.5
10	25	8 - 0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
12	25	8 - 0.015	3 + 0.5	7 +0.061 +0.025	3 + 0.5
12	30	8 - 0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
.,	30	8 - 0.015	3 + 0.5	7 + 0.061 + 0.025	3 + 0.5
16	40	$12 {}^{- 0.018}_{- 0.061}$	3 + 0.5	10 +0.061	3.5 + 0.5
20	40	12 - 0.018	3 + 0.5	10 +0.061	3.5 + 0.5
20	50	14 - 0.018	3.5 + 0.5	12 + 0.075 + 0.032	3.5 + 0.5
25	50	14 - 0.018	3.5 + 0.5	12 + 0.075 + 0.032	3.5 + 0.5
25	60	$18 {}^{- 0.018}_{- 0.061}$	4 + 0.5	15 +0.075 +0.032	5 + 0.5

																Unit [mm]
Size			Radial di	rection din	nensions						Axial di	rection dim	ensions			
ze	Α	C ₁	C ₂	C ₃	E	Υ	M	Н	J	K	L ₁	L ₂	M	Р	T	а
06	63	80	72	35	26	5	M4	18	3.5	2.1	37	25.5	15	7.3	6	0.2 ± 0.05
08	80	100	90	42	31	6	M5	20	4.3	2.6	44.5	28.5	20	8.3	8	0.2 ± 0.05
10	100	125	112	52	41	7	M5	22	5	3.1	53	33	25	9	10	0.2 ± 0.05
12	125	150	137	62	49	7	M6	24	5.5	3.6	61	37	30	9.3	12	0.3 + 0.05
16	160	190	175	80	65	9.5	M8	26	6	4.1	73	42	38	11.7	15	0.3 + 0.05
20	200	230	215	100	83	9.5	M8	30	7	5.1	86.5	50.5	45	13.4	18	0.5 -0.2
25	250	290	270	125	105	11.5	M10	35	8	6.1	102	59	54	16	22	0.5 _0.2

CS 111 CSZ

BSZ

MODELS

How to Place an Order

111-06-11G 24V 12DIN Armature bore diameter (dimensional symbol d) -

Keyway standards DIN: Compliant with the new JIS standards JIS: Compliant with the old JIS standards

C006

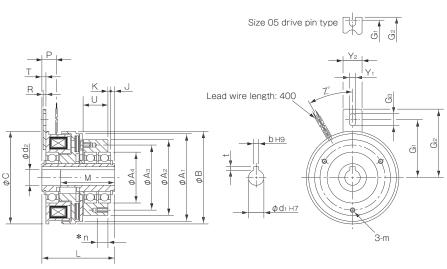
CSZ Models Electromagnetic Clutches - One-touch-mounted Type

Specifications

		Dynamic	Static	Co	oil (at	: 20℃)	Heat	M	Rotating part m	oment of inertia	Total work	A	T	T		
Model	Size	friction torque T _d [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	eat resistance class	Max. rotation speed [min ⁻¹]	Rotor [kg·m²]	Armature [kg·m²]	until readjustment of the air gap ET [J]	Armature pull-in time t _a [s]	Torque build-up time t _p [s]	Torque decaying time ta [s]	Mass [kg]	Bearing used
CSZ-05-3	5 05	2.4	2.4	DC24	10	0.42	57	В	1800	2.87×10^{-5}	2.43×10^{-5}	9 × 10 ⁶	0.017	0.035	0.023	0.38	6902ZZ
CSZ-06-35	5 06	5	5.5	DC24	11	0.46	52	В	1800	8.94×10^{-5}	7.57×10^{-5}	29 × 10 ⁶	0.023	0.050	0.010	0.67	6904ZZ
CSZ-08-35	5 08	10	11	DC24	15	0.63	38	В	1800	2.41×10^{-4}	2.08×10^{-4}	60 × 10 ⁶	0.025	0.064	0.020	1.23	6906ZZ

 $^{^{\}ast}$ The dynamic friction torque, Td, is measured at a relative speed of 100 min $^{\text{-}1}$

Dimensions



			Uı	nit [mm
Size	Sha	ft bore	dimensi	ons
Size	d ₁ H7	d ₂	b н9	t
05	10	10.2	$3^{+0.030}_{$	1.2 + 0.3
06	12	12.2	4 + 0.030	1.8 + 0.3
08	15	15.5	5 + 0.030	2.3 + 0.3

																					UI	nit [mm]	
Size				Ra	dial dire	ection d	imensio	ns								Axial dir	ection d	imensio	าร				
ze	A ₁	A ₂	A ₃	A ₄	В	C	G ₁	G ₂	G₃	Y ₁	Y ₂	J	K	L	М	Р	R	T	U	Z	m	n*	
05	50	47	38	$28_{-0.009}^{0}$	54	50	28	31	_	3.1	8	2.1	2	47.2	33	7.9	1.6	1.9	14	180	M4	6	
06	63	55	46	$37_{-0.011}^{0}$	67.5	67.5	42.5	50	9.5	4.5	14	2.5	2.3	53.5	40	9.8	2	2.5	18	30	M4	6	
08	80	70	60	47 0	85	85	57.5	65	11.5	6.5	16	3	2.5	58	43	11.5	2	3	18.5	30	M4	8	

 $^{^{*}}$ For bolts mounted on clutch hubs marked with an asterisk, select a length no greater than the n dimension.

How to Place an Order

CSZ-<u>05</u>-35

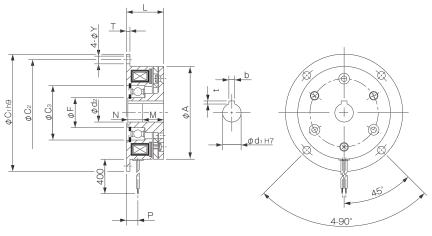
BSZ Models Electromagnetic Brakes - One-touch-mounted Type

Specifications

		Dynamic	Static	Co	oil (at	20°C)	Heat		A	Total work		T	T		
Model	Size	friction torque T _d [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	eat resistance class	Max. rotation speed [min ⁻¹]	Armature Moment of inertia J [kg·m²]	performed until readjustment of the air gap E _T [J]	Armature pull-in time ta [s]	Torque build-up time t _p [s]	Torque decaying time td [s]	Mass [kg]	Bearing used
BSZ-05-12	05	2.4	2.4	DC24	10	0.42	57	В	1800	1.46×10^{-5}	9×10^6	0.020	0.030	0.010	0.25	6902ZZ
BSZ-06-12	06	5	5.5	DC24	11	0.46	52	В	1800	5.77×10^{-5}	29×10^{6}	0.017	0.033	0.010	0.36	6904ZZ
BSZ-08-12	08	10	11	DC24	15	0.63	38	В	1800	1.63×10^{-4}	60×10^{6}	0.020	0.052	0.015	0.67	6905ZZ

^{*} The dynamic friction torque, T_d , is measured at a relative speed of 100 min $^{-1}$.

Dimensions



														Unit [ı	mm]
Radial direction dimensions			Axial direction dimensions				Shaft bore dimensions								
Ze	Α	C ₁	C ₂	C ₃	F	L	М	N	Р	T	Υ	d ₁ H7	d ₂	b н9	t
05	50	65	58	28	15	28.3	18	9.8	8.2	2	3.4	10	10.2	3 ^{+0.030} 1.2	+ 0.3
06	63	80	72	37	20	25.5	15	10	7.3	2	5	12	12.2	4 ^{+0.030} 1.8	3 ⁺ 0.3
08	80	100	90	42	25	28.5	20	8	8.3	2.6	6	15	15.5	5 ^{+0.030} 2.3	+ 0.3

How to Place an Order

BSZ-<u>05</u>-12

COLIPLINGS

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SPEED CHANGERS

INVERTERS

LINEAR SHAFT DRIVES

TOPOLIE LIMITERS

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ACTUATED
CLUTCHES & BRAKES

ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

101

CS

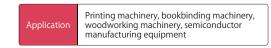
111

CSZ

BSZ

C008

ELECTROMAGNETIC CLUTCH AND BRAKE UNITS

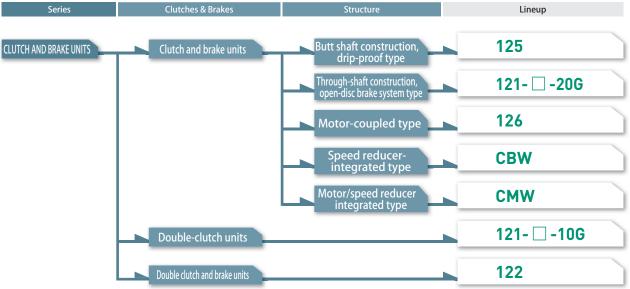


Connection and Release, Required Functions Integrated in a Compact Form Factor, Electromagnetic Clutch and Brake Units

Multiple clutches and brakes are required when designing complex actions. You can select from our clutch and brake units to get the operation you require rather than just combine as many clutches and brakes you need. We provide not just clutch and brake combinations, but total solutions that also include motors, speed reducers and the like.



Available Models



Model Selection

Model/Type	Torque	Dev	ice	Shaft st	Shaft structure		Unitized construction		Forward/ reverse	Two-step speed
riouct, type	[N·m]	Clutch	Brake	Through-shaft	Butt shaft	Motor	Speed reducer	control	operation	changing
125	2.4 ~ 160	0	0					0		
121- 🗆 -20G	5 ∼ 320		0	0				0		
126	5 ~ 80	0	0		0	0		0		
CBW	5 ~ 40		0	0			0	0		
смw	5 ~ 40	0		0		0	0	0		
121- □ -10G	5 ∼ 320	(Double clutch)		0						0
122	5 ~ 160	(Double clutch)	0	0				0	0	0

ELECTROMAGNETIC **CLUTCHES & BRAKES** SERIES ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES ELECTROMAGNETIC CLUTCH & BRAKE UNITS SPRING-ACTUATED BRAKE ELECTROMAGNETIC TOOTH CLUTCHES BRAKE MOTORS

POWER SUPPLIES

For details on selection, see P.308.

122

Product Lineup

125



RoHS-compliant (125- -12G only)

Butt shaft construction, drip-proof type

Handling is made simpler by drip-proof construction that encloses clutch and brake inside a light alloy

| Mounting direction freedom

Disc springs are used, so this clutch/brake unit can be used vertically.

This design preserves the performance of clutch and brake to the maximum extent. Its construction is sturdy, yet lightmass. Its easy-to-use butt-connected construction is drip proof, making it suitable for a variety of general industrial machinery applications. The base can be either steel plate or cast (E type made to order). Mounting is simple and service life is long.

Unit types		125- 🗆 -12G	125- 🗆 -12E
Clutch/brake torque	[N·m]	$2.4 \sim 80$	$5\sim160$
Operating temperature	[℃]	-10 ~	~ + 40
Backlash		Ze	ro

121- □ -20G



Through-shaft construction, open-disc brake system type

These are open-disc brake system type with clutch and brake mounted on the outside of a light alloy drum. They use through-shaft construction.

Ideal for winding or geared transmission

The construction holds up well under radial loads due to a wide bearing span, so they can be used under high tension when mounted with V pulleys, spur gears

Output shaft can be used in many applications

Through-shaft construction means that output is available on both sides of the shaft. Many mechanism layouts are possible, including using both ends in split driving or mounting a detection disc or the like on one This design preserves the performance of clutch and brake to the maximum extent. Its construction is sturdy, yet lightmass. Its compact through-shaft construction is open, making it suitable for a variety of general industrial machinery applications. Mounting is simple and service life is long.

Clutch/brake torque	[N·m]	5 ~ 320
Operating temperature	[℃]	$-10 \sim +40$
Backlash		Zero

126



I Easy to mount and handle

These types directly connect 3-phase induction motors to clutch/brake units, requiring less installation space and eliminating cumbersome tasks such as centering and processing of mounts. Since the output shaft is simply engaged to the load, handling is easy

Capable of high-frequency operation

These can repeatedly start and stop the output shaft without stopping the motor, so they can operate intermittently at a higher frequency than on/off operation of the motor.

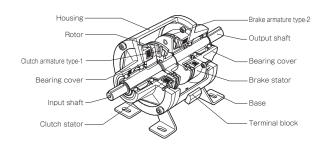
Two ways to mount

Base and flange types are available. Decide which to use based on your installation location. Flange mountings have the same shape mounting surface as general-purpose flange motors, so they can be integrated with speed reducers.

These are practical units in which induction motors are directly connected to clutch/brake units in advance. Base and flange types are available.

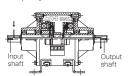
Unit types		126- □ -4B	126- 🗆 -4F-N	
Clutch/brake torque [N·m]		5 ~ 80		
Operating temperature [°C]		$-10 \sim +40$		
Backlash		Ze	ero	
Motor output	[kW]	0.2 to 3.7 3-p fully-sealed ex	ohase 4-pole ternal fan type	

Structure



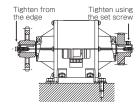
Power transmission

Input and output shafts are isolated. A pulley or the like is mounted on the input shaft, connecting it to the driver so it is always rotating. When electricity flows to the clutch, the two shafts are connected, and rotation is transmitted. If the brake mounted on the output shaft is supplied with electricity simultaneous with clutch current being shut off, the input and output shaft is quickly braked.



Mounting

The end faces of the input and output shafts are equipped with screw holes, so pulleys and the like can be easily mounted using jig accessories. They are attached by screwing them in from the end face or by using a set screw.



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CLUTCHES & BRAKES

ELECTROMAGNETIC CLUTCH & BRAKE UNITS

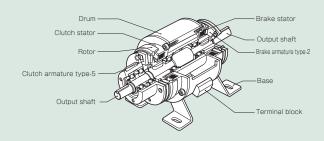
SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

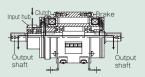
POWER SUPPLIES

Structure



Power transmission

The input hub floats on the shaft on bearings, is connected to the drive by mounting pulleys or the like, and is always rotating. When electricity flows to the clutch, the output shaft is connected, and rotation is transmitted. If a brake mounted on the output shaft is supplied with electricity simultaneous with clutch current being shut off, the input and output shaft is quickly braked. They have excellent response performance, so they are capable of high-frequency intermittent operation.



by pressing from the end face.

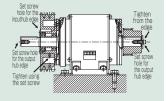
The input hub and output shaft end face

have screw holes, so they are pushed into

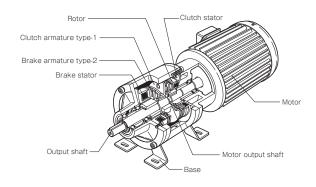
each other using a jig accessory. Lock

them in place either using a set screw or

Mounting

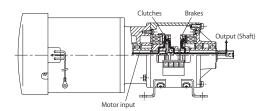


Structure



Power transmission

The motor shaft serves as the clutch input shaft, while the output shaft is isolated. When current flows to the clutch, the motor's rotation is transmitted to the output shaft via the clutch. If the brake is supplied with electricity simultaneous with clutch current being shut off, the output shaft is isolated from the motor side and instantly stopped.



MODELS

121- 🗆 -20G

126 CBW

CMW

.....

121- 🗌 -10G

122

Product Lineup

CBW



Compact, space saving

These are very compact units that combine a worm reducer and clutch/brake in a single unit. They can greatly save on space required for mounting.

Leasy to mount and handle

A V pulley comes mounted as standard on the input part, so simply connect it to a drive with a belt. Install the speed reducer to complete the mounting. No troublesome centering or processing is needed.

I Efficient starting and stopping

Integration keeps self-inertia low, so the efficiency of starting and stopping is good. It can be combined with a speed changer for a wide range of speed changes, and excellent performance can be achieved in many applications, such as 360° rotation stop of the output These are practical units in which worm reducers are directly connected to clutch/brake units in advance. A standard V belt pulley is installed on the input part of the clutch. Two models are available, based on worm reducer type.

Unit types		CBW- □ N-H □	CBW- □ N-B □
Speed reducer manufacturer		Hirai Reduction Gear Manufacturing Co.	Bellpony Co., Ltd.
Clutch/brake torque	[N·m]	5 ~	40
Operating temperature	[℃]	0~	+40
Backlash		Zero (clutch,	/brake units)



Leasy to mount and handle

These types integrate induction motors, clutch/ brake units, couplings, and speed reducers in a single unit, requiring less installation space and eliminating cumbersome tasks such as centering and processing of mounts. Since the output shaft is simply engaged to the load, handling is easy.

I Efficient starting and stopping

Integration keeps self-inertia low, so the efficiency of starting and stopping is good.

Capable of high-frequency operation

These can repeatedly start and stop the output shaft without stopping the motor, so they can operate intermittently at a higher frequency than on/off operation of the motor

These are practical units in which motors, clutch/brake units, and speed reducers are combined into a single unit in advance. An induction motor and a clutch are coupled by a MIKI PULLEY CENTAFLEX coupling, which features shock absorption, and then combined in a unit with a worm reducer to make a multifunction drive unit.

Clutch/brake torque	[N·m]	5 ~ 40
Operating temperature	[℃]	$0 \sim +40$
Backlash		Zero (clutch/brake units)
Motor output	[kW]	0.2 to 1.5 3-phase 4-pole fully-sealed external fan type

121- □ -10G



RoHS-compliant

Compact through-shaft construction

This is an efficient unit whose basic design is the same as that of clutch/brake type 121. It is a strong construction for winding, gear transmission, and the

Multi-function unit

This single unit can perform functions such as twostep speed changing, forward/reverse operation, and power distribution, so the transmission mechanism can be simplified.

These are compact, open units that place two clutches (101- -15) on a through-shaft. Since one unit can perform many functions, and is also easy to install and handle, the transmission mechanism can be simplified.

Clutch torque	[N·m]	5 ∼ 320
Operating temperature	[℃]	$-10 \sim +40$
Backlash		Zero

122



RoHS-compliant

Compact through-shaft construction

These unique units have everything placed extremely skilfully on the through-shaft. They are suitable for winding, gear transmission, and the like.

Multi-function unit

These multifunction units perform complex and precision control in a single unit, including two-step speed changing, stopping at predetermined positions, and high-frequency forward/reverse operation. The transmission mechanism can be greatly simplified.

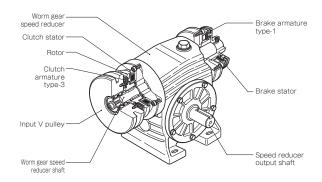
Easy handling

They not only perform many functions, they also are easy to build into machinery, just like other units

These are units unlike any other, which combine two clutches (101- □ -15G) with a brake (111- \square -12G) in a compact form factor. They provide high-precision positioning and applied control of complex operations from a single unit. Installation and handling are as easy as on other units.

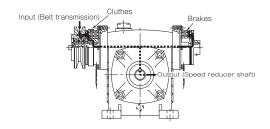
Clutch/brake torque	[N·m]	5 ~ 160
Operating temperature	[℃]	$-10 \sim +40$
Backlash		Zero

Structure



I Power transmission

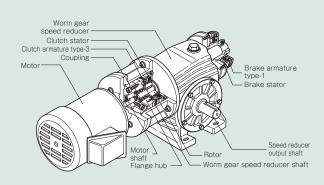
A V pulley is installed on the input part of the clutch, connected by a belt to the drive, and rotates continuously. When current flows to the clutch, rotation is transmitted to the worm shaft, and the output shaft of the speed reducer rotates. If the brake is supplied with electricity when clutch current is shut off, the output shaft stops.



ETP BUSHINGS

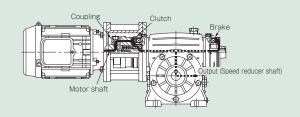
ELECTROMAGNETIC **CLUTCHES & BRAKES**

Structure



I Power transmission

The motor shaft becomes the clutch input shaft via a CENTAFLEX coupling, and the worm shaft is isolated. When current flows to the clutch, the motor's rotation is transmitted to the worm shaft via the clutch, and the output shaft of the speed reducer rotates. If the brake is supplied with electricity when clutch current is shut off, the output shaft stops.



SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** FI FCTROMAGNETIC ACTUATED

> **CLUTCHES & BRAKES** ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

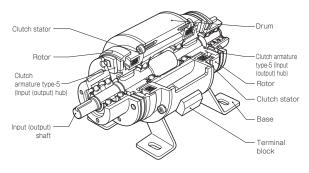
SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

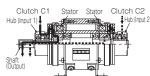
POWER SUPPLIES

Structure



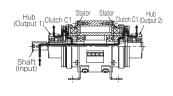
Power transmission

Two clutches, C1 and C2, have a hub shape on the armature side; a V pulley or the like is installed on each. When the hub is used as the input, different force power is connected to the two hubs and they rotate continously. When current runs to clutch C1, power is transmitted to the shaft via the rotor. When C1 current is shut off and current simultaneously sent to C2, the power switches quickly and the new power is transmitted to the shaft. When the shaft is used as the input, the drive and shaft engage and rotation is continuous. When current flows to the clutches, power is transmitted via the armature to the hub that serves as output.

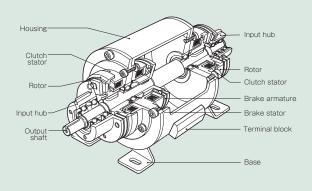


Mounting

Installation of these units and mounting of components and the like is the same as for 121- \square -20G type clutch/brake units.

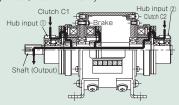


Structure



I Power transmission

Different force power is connected to the input hubs of the two clutches C1 and C2 to make them rotate continuously. When current flows to clutch C1, that power is transmitted and the output shaft rotates. When C1 current is shut off and current simultaneously sent to C2, power switches quickly and the new power is transmitted to the shaft. If the brake is supplied with electricity simultaneous with clutch current being shut off, the shaft is instantly stopped.



Mounting

Installation of these units and mounting of components and the like is the same as for 121- \square -20G type clutch/brake units.

125 121- -20G 126 CBW CMW 121- 🗌 -10G 122

MODELS

Customization

Examples of Special Cases

■ Special friction material (lining) specifications

In addition to standard friction materials, high-torque friction materials and long-life friction materials can also be handled. When using nonstandard friction materials, the friction torque and total work will differ from catalog specifications tables. Contact Miki Pulley for details.

■ Special voltage specifications

The standard voltage of clutch and brakes is DC 24 V. Special voltages such as DC 12 V, 90 V and 180 V can also be handled.

■ New JIS standard compliance for input and output shafts

Input/output shaft parts other than those of 126- \square -4F-N, CBW- \square N- \square , and CMW- \square N-H \square H are compliant with old JIS standards. They can also be made compliant with new JIS standards. Contact Miki Pulley for details.

* Please understand that we may not be able to meet all such special specifications, depending on the usage conditions, dimensional restrictions, clutch and brake sizes, mounting restrictions and the like.

How to Place an Order

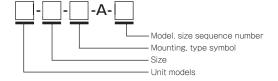
After exchanging delivery specifications for designing a product to meet your particular requirements (special production), we will custom manufacture it using the type name at right.

■ V pulleys, sprockets, etc.

Input and output components that meet your needs, for example, by having V pulleys (including with different pulley diameters), sprockets, or timing pulleys, can be designed and produced.

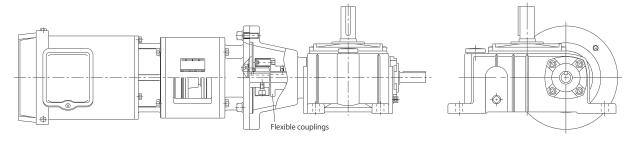
■ Integrated or unitized products

We can also produce units that combine motors, speed reducers, couplings and the like to meet your needs.

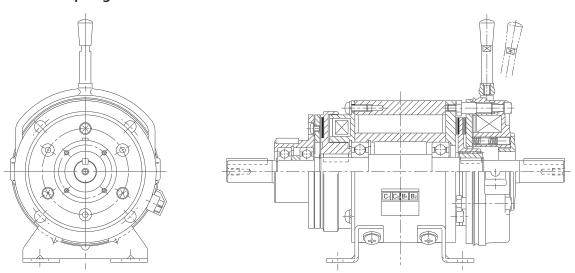


Special Application Examples

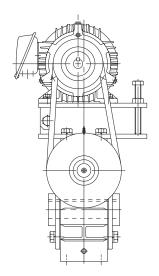
Integrated unit that uses a coupling to connect a 126 model with an above-shaft worm reducer

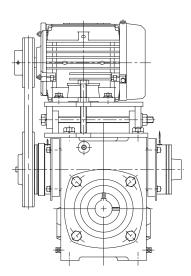


Unit that uses a spring-actuated brake as the brake of a model 121 clutch/brake unit

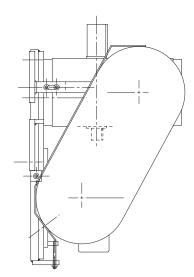


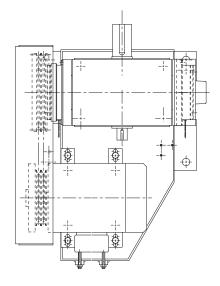
Integrated drive unit that connects a motor and special type of CBW model (hollow-shaft worm reducer) with a belt





Integrated drive unit, covered with a safety cover, that connects a motor and a special CBW model worm reducer with a belt





ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS 121- 🗆 -20G 126 CBW CMW 121- 🗌 -10G 122

For inquiries on customization

Z001

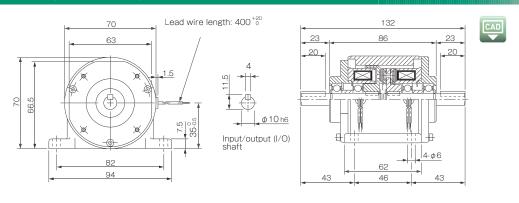
Web code

125 Models Clutch/Brake Units

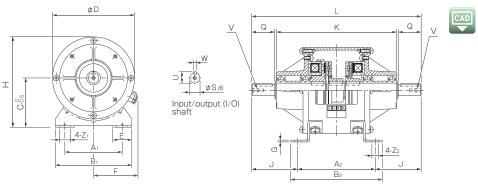
Specifications (125- □ -12G)

		Dynamic	Static		Coil (at	t 20℃)		Heat	Max.	Rotating part	Total work performed		Torque	Torque	
Model	Size	friction torque T _d [N·m]	friction torque Ts [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	nt resistance class	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	until readjustment of the air gap ET [J]	Armature pull-in time t _a [s]	Torque build-up time t _P [s]	decaying time td [s]	Mass [kg]
125-05-12G	05	2.4	-	DC24	10	0.42	58	В	3000	2.4×10^{-5}	9 × 10 ⁶	C:0.012 B:0.010	C:0.031 B:0.023	C:0.040 B:0.012	1.2
125-06-12G	06	5	5.5	DC24	11	0.46	52	В	3000	1.28 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	2.1
125-08-12G	08	10	11	DC24	15	0.63	38	В	3000	3.70 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	4.2
125-10-12G	10	20	22	DC24	20	0.83	29	В	3000	1.40 × 10 ⁻³	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	6.8
125-12-12G	12	40	45	DC24	25	1.09	23	В	3000	3.85×10^{-3}	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	12
125-16-12G	16	80	90	DC24	35	1.46	16	В	3000	1.35 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	22

Dimensions (125-05-12G)



Dimensions (125- □ **-126)**



Size							Dime	nsions o	f part								- 1	Dimens	ions of shaft	
Size	A ₁	A ₂	B ₁	B ₂	С	D	E	F	G	Н	J	K	L	Z ₁	Z ₂	Q	S	U	V	W
06	65	90	90	105	65	100	27.5	61	2.6	115	48.5	132	187	13.5	6.5	25	11	12.5	M4 \times 0.7, length: 8	4
08	80	110	110	130	80	125	32.5	72	3.2	142.5	63	171	236	15.5	9	30	14	16	M4 \times 0.7, length: 8	5
10	105	135	140	160	90	150	35	81	3.2	165	80	210	295	20	11.5	40	19	21	$M6 \times 1$, length: 11	5
12	135	160	175	185	112	190	42.5	97	4.5	207	108	270	376	24	11	50	24	27	$M6 \times 1$, length: 11	7
16	155	200	200	230	132	230	45	109	6	247	145	362	490	28	14	60	28	31	$M6 \times 1$, length: 11	7

Unit [mm]

How to Place an Order

125-06-12G

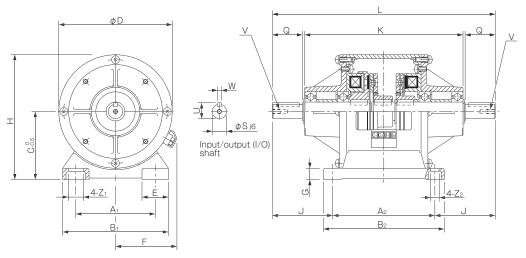
^{*} The input/output shaft keyways are old JIS standard class 2 while the key is old JIS standard class 1.
* When inserting pulleys or the like onto input/output shafts, use the supplied insertion set.

Specifications (125- \square -12E) Made to Order

		Dynamic	Static		Coil (at	20℃)		Heat	Max.	Rotating part	Total work performed			Torquo	
Model	Size	friction torque T _d [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	nt resistance class	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	until readjustment of the air gap ET [J]	Armature pull-in time t _a [s]	Torque rise time t _p [s]	Torque extinction time td [s]	Mass [kg]
125-06-12E	06	5	5.5	DC24	11	0.46	52	В	3000	1.28 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	2.1
125-08-12E	08	10	11	DC24	15	0.63	38	В	3000	3.70 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	4.2
125-10-12E	10	20	22	DC24	20	0.83	29	В	3000	1.40×10^{-3}	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	6.8
125-12-12E	12	40	45	DC24	25	1.09	23	В	3000	3.85 × 10 ⁻³	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	12
125-16-12E	16	80	90	DC24	35	1.46	16	В	3000	1.35 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	22
125-20-12E	20	160	175	DC24	45	1.86	13	В	2500	4.08 × 10 ⁻²	10 × 10 ⁵	C:0.090 B:0.065	C:0.250 B:0.207	C:0.130 B:0.070	49

^{*}The dynamic friction torque, T_d , is measured at a relative speed of 100 min $^{\text{-}1}$.

Dimensions (125- □ **-12E)** Made to Order



																			Un	nit [mm]
Size							Dime	nsions o	f part								- 1	Dimens	ions of shaft	
Size	A_1	A_2	B ₁	B ₂	С	D	E	F	G	Н	J	K	L	Z ₁	Z ₂	Q	S	U	V	W
06	65	90	90	105	65	100	27.5	61	10	115	48.5	132	187	13.5	6.5	25	11	12.5	M4 $ imes$ 0.7, length: 8	4
08	80	110	110	130	80	125	32.5	72	12	142.5	63	171	236	15.5	9	30	14	16	M4 \times 0.7, length: 8	5
10	105	135	140	160	90	150	35	81	15	165	80	210	295	20	11.5	40	19	21	$M6 \times 1$, length: 11	5
12	135	160	175	185	112	190	42.5	97	15	207	108	270	376	24.5	11	50	24	27	$M6 \times 1$, length: 11	7
16	155	200	200	230	132	230	45	109	18	247	145	362	490	28	14	60	28	31	$M6 \times 1$, length: 11	7
20	195	240	240	270	160	290	47.5	124	20	305	188	448	616	28	14	80	38	41.5	M10 $ imes$ 1.5, length: 17	10

^{*} The input/output shaft keyways are old JIS standard class 2 while the key is old JIS standard class 1.

* When inserting pulleys or the like onto input/output shafts, use the supplied insertion set.

How to Place an Order



ELECTROMAGNETIC **CLUTCHES & BRAKES** SERIES ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

121- 🗆 -20G 126 CBW

CMW

MODELS

121- 🗆 -10G

122

MIKIPULLEY 289

C009

Web code

125 Models

List of Stand-alone Clutches and Brakes Used

Model	Chand along dutch sustans	Chand along bushing quature	Bearing	number
Model	Stand-alone clutch system	Stand-alone braking system	Input part	Output part
125-05-12	-	-	6000	6000
125-06-12	101-06-11G 24V R15JIS A15JIS	111-06-12G 24V 15JIS	6202	6202
125-08-12	101-08-11G 24V R20JIS A20JIS	111-08-12G 24V 20JIS	6004	6004
125-10-12	101-10-11G 24V R25JIS A25JIS	111-10-12G 24V 25JIS	6205	6205
125-12-12	101-12-11G 24V R30JIS A30JIS	111-12-12G 24V 30JIS	6206	6206
125-16-12	101-16-11G 24V R40JIS A40JIS	111-16-12G 24V 40JIS	6208	6208
125-20-12	101-20-11G 24V R50JIS A50JIS	111-20-12G 24V 50JIS	6211	6211

Recommended Power Supplies and Accessory Parts

	De sammen de dinavier		Accessor	v parts	
Model	Recommended power supplies	Circuit protector (Varistor), qty. 2	Tightening collar	Screw stock	Hexagonal nut
125-05-12	BEH-10G	NVD07SCD082 or an equivalent	-	-	-
125-06-12	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$ (hex-socket bolt), qty. 1	M4, qty. 1
125-08-12	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$ (hex-socket bolt), qty. 1	M4, qty. 1
125-10-12	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M6 × 100, qty. 1	M6, qty. 2
125-12-12	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M6 × 100, qty. 1	M6, qty. 2
125-16-12	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M6 × 100, qty. 1	M6, qty. 2
125-20-12	BEH-20G	NVD07SCD082 or an equivalent	Qty. 1	M10 × 160, qty. 1	M10, qty. 2

^{*} NVD SCD parts are manufactured by KOA Corporation.

* Varistors need not be used when a BEH model overexcitation electromagnetic power supply is used. For details, refer to the section on power supplies.

Mounting Example

In Combination with Speed Changers

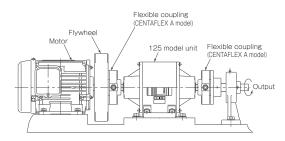
Clutches and brakes are generally used after motors and speed changers. This unit was designed so that it can be used in combination with a Miki Pulley belt-type stepless speed changer.

We provide items precombined into sets. Contact Miki Pulley for details.

speed change PDS model 125 model unit (CENTAFLEX A model)

Examples of Direct Connection to Motors

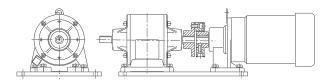
Couplings generally have small inertial moments compared to pulleys, sprockets and the like, so they are often used in combination with clutches and brakes. This unit is often combined with our flexible couplings (CENTAFLEX) in particular. It is very effective to mount it on the motor side in combination with a flywheel.

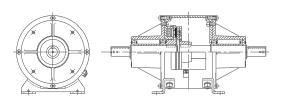


Special Types

In addition to the special application examples shown below, drivers can also be set, and units can be provided with pulleys, sprockets, and the like. Contact Miki Pulley for details.

One-piece Unit Connected to Geared Motor Clutch Unit (No Brake) and Coupling





ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** FLECTROMAGNETIC ACTUATED

CLUTCHES & BRAKES ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

121- -20G 126 CBW CMW

121- 🗌 -10G 122

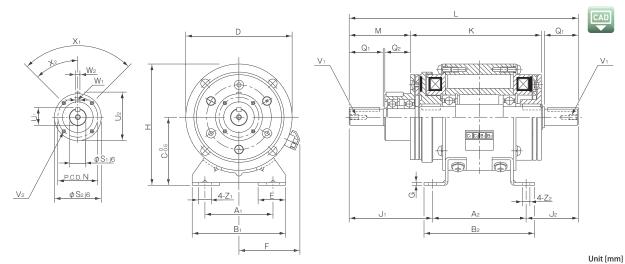
-20G Types Clutch/Brake Units

Specifications

		Dynamic	Static		Coil (a	t 20℃)		Heat	Max.	Potating part	Total work performed		Torque	Torque	
Model	Size	friction torque T _d [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	at resistance class	rotation speed [min ⁻¹]	Rotating part moment of inertia J [kg·m²]	until readjustment of the air gap ET [J]	Armature pull-in time ta [s]	Torque build-up time t _p [s]	Torque decaying time td [s]	Mass [kg]
121-06-20G	06	5	5.5	DC24	11	0.46	52	В	3000	1.43 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	1.5
121-08-20G	08	10	11	DC24	15	0.63	38	В	3000	4.23 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	2.7
121-10-20G	10	20	22	DC24	20	0.83	29	В	3000	1.42×10^{-3}	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	5.5
121-12-20G	12	40	45	DC24	25	1.09	23	В	3000	4.18 × 10 ⁻³	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	9.6
121-16-20G	16	80	90	DC24	35	1.46	16	В	3000	1.34 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	18.5
121-20-20G	20	160	175	DC24	45	1.88	13	В	2500	4.13 × 10 ⁻²	10 × 10 ⁸	C:0.090 B:0.065	C:0.250 B:0.200	C:0.130 B:0.070	35
121-25-20G	25	320	350	DC24	60	2.50	9.6	В	2000	1.02×10^{-1}	20 × 10 ⁸	C:0.115 B:0.085	C:0.335 B:0.275	C:0.210 B:0.125	64

^{*}The dynamic friction torque, T_d, is measured at a relative speed of 100 min⁻¹.

Dimensions



Size								Dir	nens	ions o	f part	:													Dimensions of s	haft			
ze	A ₁	A ₂	В1	B ₂	C	D	Ε	F	G	Н	J ₁	J ₂	K	L	М	N	Zı	Z 2	Q ₁	\mathbf{Q}_2	S ₁	S ₂	U ₁	U ₂	V 1	V ₂	X 1	X ₂	W _{1,2}
06	52.5	75	80	90	55	80	27.5	53	2.6	95	65.5	40.5	105.5	181	47	33	13.5	6.5	25	20	11	38	12.5	39.5	$M4 \times 0.7$, length: 8	3-M4 × 0.7, length: 4	3-120°	60°	4
80	65	90	90	105	65	100	27.5	61	2.6	115	78.5	48.5	126.5	217	57	37	13.5	6.5	30	25	14	45	16	47	$M4 \times 0.7$, length: 8	3-M4 × 0.7, length: 6	3-120°	60°	5
10	80	110	110	130	80	125	32.5	72	3.2	142.5	98	62	154	270	72	47	15.5	9	40	30	19	55	21	57	$M6 \times 1$, length: 11	4-M4 × 0.7, length: 8	4-90°	45°	5
12	105	135	140	160	90	150	35	81	3.2	165	121	73.5	184	330	92	52	20	11.5	50	40	24	64	27	67	M6 × 1, length: 11	4-M4 × 0.7, length: 8	4-90°	45°	7
16	135	160	175	185	112	190	43	97	4.5	207	149	90	221	399	113	62	24.5	11.5	60	50	28	75	31	78	M6 × 1, length: 11	6-M5 × 0.8, length: 8	6-60°	30°	7
20	155	200	200	230	132	230	45	109	6	247	187	117	276	504	142	74.5	28	14	80	60	38	90	41.5	93.5	M10 × 1.5, length: 17	4-M6 × 1, length: 12	4-90°	45°	10
25	195	240	240	270	160	290	47.5	124	20	305	238	154	334	632	183	101.5	28	14	110	70	42	115	45.5	118.5	M10 × 1.5, length: 17	8-M6 × 1, length: 12	8-45°	22.5°	12

^{*} The input/output shaft keyways are old JIS standard class 2 while the key is old JIS standard class 1. Note that the keyway dimensions of the unit hub part do not conform to the old JIS standard. Check them on the dimensions table above.

How to Place an Order

121-06-20G

^{*} When inserting pulleys or the like onto input/output shafts, use the supplied insertion set.

* The 121-25-20G base is a casting.

List of Stand-alone Clutches and Brakes Used

Model	Stand along distals asstant	Stand along bushing gretom	Bearing	number
Model	Stand-alone clutch system	Stand-alone braking system	Main shaft part	Hub part
121-06-20G	101-06-15G 24V R15JIS A12JIS	111-06-12G 24V 15JIS	6202	6001
121-08-20G	101-08-15G 24V R20JIS A15JIS	111-08-12G 24V 20JIS	6004	6002
121-10-20G	101-10-15G 24V R25JIS A20JIS	111-10-12G 24V 25JIS	6205	6004
121-12-20G	101-12-15G 24V R30JIS A25JIS	111-12-12G 24V 30JIS	6206	6005
121-16-20G	101-16-15G 24V R40JIS A30JIS	111-16-12G 24V 40JIS	6208	6006
121-20-20G	101-20-15G 24V R50JIS A40JIS	111-20-12G 24V 50JIS	6211	6008
121-25-20G	101-25-15G 24V R60JIS A50JIS	111-25-12G 24V 60JIS	6214	6010

Recommended Power Supplies and Accessory Parts

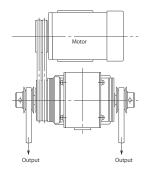
Model	Recommended			Accessory parts		
Model	power supplies	Circuit protector (Varistor), qty. 2	Tightening collar	Screw stock	Presser foot	Hexagonal nut
121-06-20G	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$, qty. 3	Qty. 1	M4, qty. 3
121-08-20G	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$, qty. 3	Qty. 1	M4, qty. 3
121-10-20G	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$, qty. 3	Qty. 1	M4, qty. 3
121-12-20G	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M4 \times 55, qty. 2/M6 \times 100, qty. 1	Qty. 1	M4, qty. 2/M6, qty. 1
121-16-20G	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M5 \times 70, qty. 2/M6 \times 100, qty. 1	Qty. 1	M5, qty. 2/M6, qty. 1
121-20-20G	BEH-20G	NVD07SCD082 or an equivalent	Qty. 1	$M6 \times 160$, qty. $2/M10 \times 220$, qty. 1	Qty. 1	M6, qty. 4/M10, qty. 2
121-25-20G	BEH-20G	NVD07SCD082 or an equivalent	Qty. 1	$M6 \times 160$, qty. $2/M10 \times 220$, qty. 1	Qty. 1	M6, qty. 4/M10, qty. 2

^{*} NVD \square SCD \square parts are manufactured by KOA Corporation.

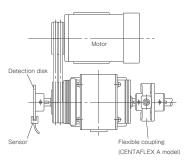
Mounting Example

This clutch/brake unit allows the output shaft to be used in two locations, so both outputs can be used simultaneously, or one can be connected to a load and a rotation detection disk mounted to the other. A variety of transmission paths can be used in layouts.

I Example with Two Outputs



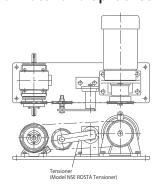
Example with Detection Disk on One Side



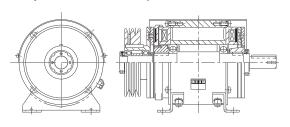
Special Types

In addition to the special application examples shown below, drivers can also be set, and units can be provided with pulleys, sprockets, and the like. Contact Miki Pulley for details.

I One-piece Unit Connected by Geared Motor and Sprocket



Clutch/Brake Unit with V Pulley Mounted on Input Side



C010

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
THE CTROMA CHITTIE
ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

121- -20G

126 CBW

CMW

121- 🗌 -10G

122

Web code

^{*} Varistors need not be used when a BEH model overexcitation electromagnetic power supply is used. For details, refer to the section on power supplies.

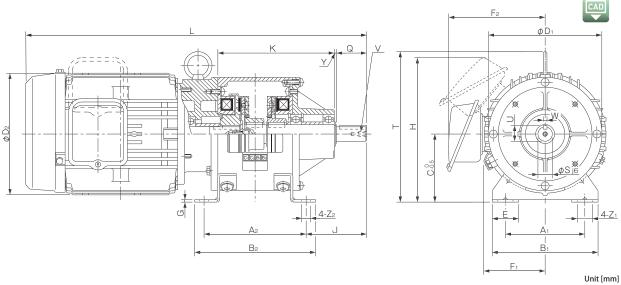
126 Models Clutch/Brake Units - Motor-coupled Type

Specifications (126- -4B)

		Motor	Dynamic	Static		Coil (a	t 20℃)		Heat	Potating part	Total work		Torque	Torque	
Model	Size	output [kW] 4-poles	friction torque T _d [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	at resistance class	Rotating part moment of inertia J [kg·m²]	until readjustment of the air gap ET [J]	Armature pull-in time ta [s]	Torque build-up time t _p [s]	Torque decaying time td [s]	Mass [kg]
126-06-4B-0.2kW	06	0.2	5	5.5	DC24	11	0.46	52	В	1.28 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	8.9
126-08-4B-0.4kW	08	0.4	10	11	DC24	15	0.63	38	В	3.70 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	13
126-10-4B-0.75kW-IE3	10	0.75	20	22	DC24	20	0.83	29	В	1.40×10^{-3}	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	20
126-12-4B-1.5kW-IE3	12	1.5	40	45	DC24	25	1.09	23	В	3.85 × 10 ⁻³	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	41
126-16-4B-2.2kW-IE3	16	2.2	80	90	DC24	35	1.46	16	В	1.35 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	54
126-16-4B-3.7kW-IE3	16	3.7	80	90	DC24	35	1.46	16	В	1.35 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	69

^{*} The induction motors are fully sealed external fan motors that conform to the JIS C4210 standard (for 0.2 kW and 0.4 kW models) or the JIS C 4213 standard (for 0.75 kW models or higher).

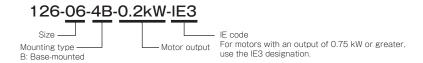
Dimensions (126- ☐ -4B)



Madal								- 1	Dimer	nsions (of part	t									D	imens	ions of shaft	
Model	A ₁	A ₂	B ₁	B ₂	С	D ₁	D ₂	Е	F ₁	F ₂	G	J	K	L	Н	T	Υ	Z ₁	Z ₂	Q	S	U	V	W
126-06-4B-0.2kW	65	90	90	105	65	100	130	27.5	61	-	2.6	48.5	102	335	-	-	3	13.5	6.5	25	11	12.5	M4 × 0.7, length: 8	4
126-08-4B-0.4kW	80	110	110	130	80	125	145	32.5	72	126.5	3.2	63	127.5	389	167.5	_	2.5	15.5	9	30	14	16	M4 \times 0.7, length: 8	5
126-10-4B-0.75kW-IE3	105	135	140	160	90	150	163	35	81	136	3.2	80	154	462	184	-	3	20	11.5	40	19	21	M6 × 1, length: 11	5
126-12-4B-1.5kW-IE3	135	160	175	185	112	190	182/176	42.5	97	148.5	15	108	194	550.5	-	244.5	3	24.5	11.5	50	24	27	M6 × 1, length: 11	7
126-16-4B-2.2kW-IE3	155	200	200	230	132	230	198/195	45	109	155.5	18	135	256	649.5	-	286	4	28	14	50	24	27	M6 × 1, length: 11	7
126-16-4B-3.7kW-IE3	155	200	200	230	132	230	225/215	45	109	168.5	18	145	256	681	-	295	4	28	14	60	28	31	M6 × 1, length: 11	7

^{*} The output shaft keyways are old JIS standard class 2 while the key is old JIS standard class 1.

How to Place an Order



 $^{^{\}ast}$ The power supplies for the motors are 3-phase, 200 V AC at 50 Hz, or 200/220 V AC at 60 Hz.

^{*} If you desire a special voltage (5 Power Supply Specifications), different number of poles, or the like for the induction motor, contact Miki Pulley.

^{*} The dynamic friction torque, T_d, is measured at a relative speed of 100 min⁻¹.

^{*} When inserting pulleys or the like onto output shafts, use the supplied insertion set.

* These models are cast basded on a motor output of 1.5 kW or greater.

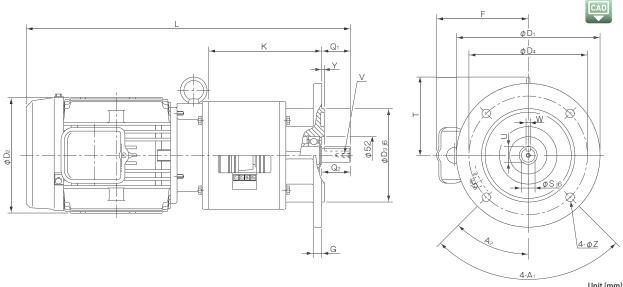
Specifications (126- -4F-N)

		Motor	Dynamic	Static		Coil (at	t 20℃)		Hea	Rotating part	Total work performed		Torque	Torque	
Model	Size	output [kW] 4-poles	friction torque T _d [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat resistance class	moment of inertia J [kg·m²]	until readjustment of the air gap ET [J]	Armature pull-in time t _a [s]	build-up time t _P [s]	decaying time td [s]	Mass [kg]
126-06-4F-N-0.2kW	06	0.2	5	5.5	DC24	11	0.46	52	В	1.28 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	8.9
126-08-4F-N-0.4kW	08	0.4	10	11	DC24	15	0.63	38	В	3.70 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	13
126-10-4F-N-0.75kW-IE3	10	0.75	20	22	DC24	20	0.83	29	В	1.40×10^{-3}	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	20
126-12-4F-N-1.5kW-IE3	12	1.5	40	45	DC24	25	1.09	23	В	3.85 × 10 ⁻³	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	41
126-16-4F-N-2.2kW-IE3	16	2.2	80	90	DC24	35	1.46	16	В	1.35 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	54
126-16-4F-N-3.7kW-IE3	16	3.7	80	90	DC24	35	1.46	16	В	1.35 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	69

- * The induction motors are fully sealed external fan motors that conform to the JIS C4210 standard (for 0.2 kW and 0.4 kW models) or the JIS C 4213 standard (for 0.75 kW models or higher).
- * The power supplies for the motors are 3-phase, 200 V AC at 50 Hz, or 200/220 V AC at 60 Hz.
- *If you desire a special voltage (5 Power Supply Specifications), different number of poles, or the like for the induction motor, contact Miki Pulley.

 * The dynamic friction torque, Ta_i is measured at a relative speed of 100 min⁻¹.

Dimensions (126- -4F-N)

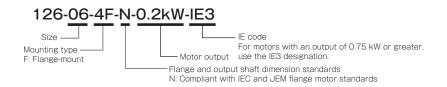


																		Oil	nt [mm]
Model						Dime	nsions o	f part								Dime	ensions	of shaft	
Model	A ₁	A ₂	D ₁	D ₂	\mathbf{D}_3	D ₄	F	G	K	L	T	Υ	Z	\mathbf{Q}_1	\mathbf{Q}_2	S	U	V	W
126-06-4F-N-0.2kW	90°	45°	160	130	110	130	_	8	107	335	-	3.5	10	23	25	11	12.5	M4 \times 0.7, length: 8	4
126-08-4F-N-0.4kW	90°	45°	160	145	110	130	124	10	130.5	389	-	3.5	10	30	30	14	16	M4 \times 0.7, length: 8	5
126-10-4F-N-0.75kW-IE3	90°	45°	200	163	130	165	131	12	157.5	463	-	3.5	12	40	40	19	21.5	$M6 \times 1$, length: 11	6
126-12-4F-N-1.5kW-IE3	90°	45°	200	182/176	130	165	148.5	12	197.5	551	133	3.5	12	50	50	24	27	$M6 \times 1$, length: 11	8
126-16-4F-N-2.2kW-IE3	90°	45°	250	198/195	180	215	155.5	16	260.5	660	154	4	15	60	60	28	31	$M6 \times 1$, length: 11	8
126-16-4F-N-3.7kW-IE3	90°	45°	250	225/215	180	215	168.5	16	260.5	681.5	163	4	15	60	60	28	31	$M6 \times 1$, length: 11	8

- * The flange and output shaft dimensions conform to IEC and JEM standard flange motors. (Size 06 has a key and a keyway.)
- * When inserting pulleys or the like onto output shafts, use the supplied insertion set.

How to Place an Order

To download CAD data or product catalogs:



ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** FI FCTROMAGNETIC-

ACTUATED **CLUTCHES & BRAKES**

ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS 121- 🗆 -20G 126 CBW CMW 121- 🗌 -10G 122

C012

Web code

126 Models

List of Stand-alone Clutches and Brakes Used

Model	Chand along distals assets as	Stand along bushing gretom	Bearing	number
Model	Stand-alone clutch system	Stand-alone braking system	Input part	Output part
126-06-4 🗆 -0.2kW	101-06-11G 24V R11JIS A15JIS	111-06-12G 24V 15JIS	6202	6202
126-08-4 🗆 -0.4kW	101-08-11G 24V R14DIN A20JIS	111-08-12G 24V 20JIS	6203	6004
126-10-4 🗆 -0.75kW-IE3	101-10-11G 24V R19DIN A25JIS	111-10-12G 24V 25JIS	6204	6205
126-12-4 🗆 -1.5kW-IE3	101-12-11G 24V R24DIN A30JIS	111-12-12G 24V 30JIS	6205	6206
126-16-4 🗆 -2.2kW-IE3	101-16-11G 24V R28DIN A40JIS	111-16-12G 24V 40JIS	6206	6208
126-16-4 🗆 -3.7kW-IE3	101-16-11G 24V R28DIN A40JIS	111-16-12G 24V 40JIS	6306	6208

Recommended Power Supplies and Accessory Parts

Model	Recommended		Accessory	parts	
Model	power supplies	Circuit protector (Varistor), qty. 2	Tightening collar	Screw stock	Hexagonal nut
126-06-4 □ -0.2kW	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M4 $ imes$ 55 (hex-socket bolt), qty. 1	M4, qty. 1
126-08-4 □ -0.4kW	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$ (hex-socket bolt), qty. 1	M4, qty. 1
126-10-4 🗆 -0.75kW-IE3	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M6 \times 100$, qty. 1	M6, qty. 2
126-12-4 🗆 -1.5kW-IE3	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M6 × 100, qty. 1	M6, qty. 2
126-16-4 🗆 -2.2kW-IE3	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	$M6 \times 100$, qty. 1	M6, qty. 2
126-16-4 -3.7kW-IE3	BEH-10G	NVD07SCD082 or an equivalent	Qty. 1	M6 × 100, qty. 1	M6, qty. 2

^{*} NVD SCD parts are manufactured by KOA Corporation.

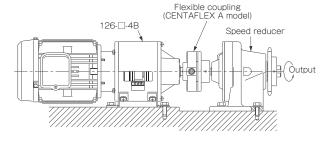
* Varistors need not be used when a BEH model overexcitation electromagnetic power supply is used. For details, refer to the section on power supplies.

Mounting Example

In Combination with Speed Reducers

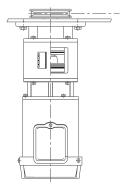
In the example on right, a clutch/brake unit of the motorcoupled type is combined with a speed reducer by a flexible coupling.

Since the motor is directly coupled, the build-up of the rotation shaft is sharp. That makes it desirable in design to keep inertia on the load side as small as possible. We recommend a flexible coupling with low inertia for connecting to the speed reducer.



Example Using Flange-mounted Type Vertically

They can be mounted in any direction, providing layout freedom and saving space.



COUPLINGS

FTP RUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

SPEED CHANGER

INVERTER

LINEAR SHAFT DRIVES

TOPOLIE I IMITEDS

POSTA

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
ELECTROMAGNETIC-

ACTUATED
CLUTCHES & BRAKES
ELECTROMAGNETIC
CLUTCH & BRAKE

SPRING-ACTUATED
BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

.....

121- 🗆 -20G

126 CBW

CMW

121- 🗆 -10G

122

CBW Models Clutch/Brake Units - Speed Reducer-integrated Type

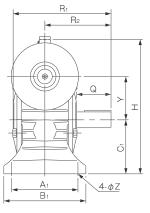
Specifications (CBW- \square N-H \square)

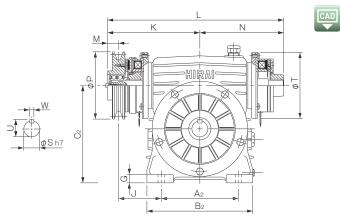
		Dynamic	Static		Coil (at	:20℃)		Heat	Max.	Datating yout	Total work		T	T
Model	Size	friction Torque T _d [N·m]	friction Torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	at resistance class	rotation speed [min ⁻¹]	Rotating part moment of inertia J [kg·m²]	performed readjustment of the air gap E _T [J]	Armature pull-in time ta [s]	Torque build-up time t _p [s]	Torque decaying time td [s]
CBW-06N-H□	06	5	5.5	DC24	11	0.46	52	В	1800	1.66 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015
CBW-08N-H□	08	10	11	DC24	15	0.63	38	В	1800	4.78 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025
CBW-10N-H□	10	20	22	DC24	20	0.83	29	В	1800	1.71 × 10 ⁻³	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030
CBW-12N-H□	12	40	45	DC24	25	1.09	23	В	1800	4.53 × 10 ⁻³	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050

^{*} The dynamic friction torque, T_d , is measured at a relative speed of 100 min $^{-1}$.

		Input par	rt				Speed	l reducer					
Model	Size	Pulley diameter	Belt	Model	Output shaft		Sp	eed reduct	tion ratio 1/			Oil volume	Mass [kg]
		[mm]	type	Model	rated values	10	20	30	40	50	60		. 32
CBW-06N-H □	06	76.2	A-1	N-1A	Torque [N·m]	45.3	53.4	46.7	54.7	54.2	55.4	0.25	6.5
CBW-00N-H	00	(3 in.)	A-1	IN-1A	O.H.L. [N]	1560	1760	1760	1760	1760	1760	0.23	0.5
CBW-08N-H □	08	101.6	A-1	N-2A	Torque [N·m]	79.8	102	86.9	104	98.5	100	0.5	15
CBW-00N-H	00	(4 in.)	Α-1	IN-ZA	O.H.L. [N]	1760	2240	2630	2880	3140	3230	0.5	13
CBW-10N-H □	10	127	B-1	N-3A	Torque [N·m]	165	180	180	188	187	164	1.0	24
CBW-10N-H	10	(5 in.)	D-1	IN-3M	O.H.L. [N]	2250	2900	3370	3720	4040	4370	1.0	24
CDW-12N-U	152.4	B-1	N-4A	Torque [N·m]	292	293	301	302	-	-	2.0	38	
CBW-12N-H		(6 in.)	ו-ט	IN-4A	O.H.L. [N]	2780	3640	4210	4680	-	-	2.0	30

Dimensions (CBW- ☐ N-H ☐)





, ,			- 1															7				Uni	it [mm]
Model									Dime	nsions o	of part									Dir	nensio	ns of sh	aft
Model	A ₁	A ₂	B ₁	B ₂	C ₁	C ₂	G	Н	J	K	L	М	N	Р	R ₁	R ₂	T	Υ	Z	Q	S	U	W
CBW-06N-H□	95	95	117	136	65	115.8	11	157	58	120.5	225	15	104.5	76.2	135	90	80	50.8	9.5	45	20	22.5	6
CBW-08N-H□	115	112	140	165	82	146	15	212	75	149	284	18	135	101.6	160	105	100	64	11	50	25	28	8
CBW-10N-H□	125	146	155	205	102	184	16	255	80.5	174.5	333	21	158.5	127	185	125	125	82	12	65	30	33	8
CBW-12N-H□	150	168	185	245	118	213	20	289	93	203	388	25.5	185	152.4	225	150	150	95	14	75	35	38	10

How to Place an Order

CBW-06N-HR-10

Size ______ Speed reduction ratio 1/□: 10, 20, 30, 40, 50, 60

Speed reducer _____ Output shaft direction

HIRAI REDUCTION GEAR MFG. CO.: H

R: Right side of the output shaft as viewed from the input pulley

H: Right side of the output shaft as viewed from the input pulleyL: Left side of the output shaft as viewed from the input pulley

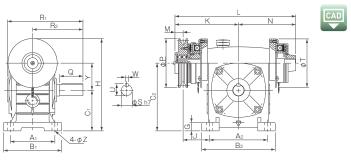
Specifications (CBW- \square N-B \square)

		Dynamic			Coil (at	20°C)		res	Max.	Rotating part	Total work until	Armature	Torque	Torque
Model	Size	friction torque Td [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat sistance class	rotation speed [mim -1]	Moment of inertia J [kg·m²]	readjustment of the air gap Et [J]	pull-in time	build-up time t _p [s]	decaying time td [s]
CBW-06N-B \square -10 \sim 30	06	5	5.5	DC24	11	0.46	52	В	1800	1.56×10^{-4}	36 × 10 ⁶	C:0.020	C:0.041	C:0.020
CBW-06N-B \square -40 \sim 60	00	3	3.3	DC24	- '''	0.40	32	Б	1000	1.76×10^{-4}	30 × 10-	B:0.015	B:0.033	B:0.015
CBW-08N-B □ -10 ~ 30	08	10	11	DC24	15	0.63	38	В	1800	4.70×10^{-4}	60 × 10 ⁶	C:0.023	C:0.051	C:0.030
CBW-08N-B □ -40 ~ 60	00	10	11	DC24	13	0.03	30	Б	1000	4.85×10^{-4}	00 × 10-	B:0.016	B:0.042	B:0.025
CBW-10N-B \square -10 \sim 30	10	20	22	DC24	20	0.83	29	В	1000	1.48×10^{-3}	130 × 10 ⁶	C:0.025	C:0.063	C:0.050
CBW-10N-B \square -40 \sim 60	10	20	22	DC24	20	0.83	29	D	1800	1.61×10^{-3}	130 × 10°	B:0.018	B:0.056	B:0.030
CBW-12N-B □ -10 ~ 30	12	40	45	DC24	25	1.09	23	В	1000	4.23×10^{-3}	250 × 10 ⁶	C:0.040	C:0.115	C:0.065
CBW-12N-B □ -40 ~ 60	12	40	45	DC24	25	1.09	23	В	1800	4.35×10^{-3}	250 × 10°	B:0.027	B:0.090	B:0.050

^{*}The dynamic friction torque, T_d , is measured at a relative speed of 100 min $^{-1}$.

		Input par	t				Speed	l reducer					
Model	Size	Pulley diameter	Belt	Model	Output shaft		Sp	eed reduct	ion ratio 1/			Oil volume	Mass [kg]
		[mm]	Model	Model	rated values	10	20	30	40	50	60		
CBW-06N-B □ -10 ~ 30				N-PR-12	Torque [N·m]	35	38	44	-	_	-	0.3	9
CBM-00M-B - 10 30	06	76.2	A-1	N-F N-12	O.H.L. [N]	950	1313	1548	-	_	-	0.5	,
CBW-06N-B □ -40 ~ 60	00	(3 in.)	A-1	N-PR-15	Torque [N·m]	_	_	_	64	56	56	0.4	11
CBW-00N-B40 ** 60				N-FN-13	O.H.L. [N]	_	_	_	2450	2450	2450	0.4	
CBW-08N-B □ -10 ~ 30				N-PR-15	Torque [N·m]	56	57	72	_	_	-	0.4	11.5
CBM-09M-B - 10 - 20	08	101.6	A-1	IN-FN-13	O.H.L. [N]	1421	1862	2322	_	_	-	0.4	11.5
CBW-08N-B □ -40 ~ 60	00	101.6 (4 in.)	A-1	N-PR-18	Torque [N·m]	_	_	-	143	136	138	0.7	16.5
CBW-06N-B40 . 00				N-F N-10	O.H.L. [N]	_	_	-	2646	2646	2646	0.7	10.5
CBW-10N-B □ -10 ~ 30				N-PR-18	Torque [N·m]	120	126	150	_	_	_	0.7	17.5
CBM-10M-B -10 - 30	10	127	B-1	N-F N-10	O.H.L. [N]	1490	2077	2440	-	_	-	0.7	17.5
CBW-10N-B □ -40 ~ 60	10	(5 in.)	D-1	N-PR-22	Torque [N·m]	_	_	_	191	187	167	1.2	23.5
CBW-TUN-B -40 · 00				N-F N-22	O.H.L. [N]	_	_	-	3057	3146	3155	1.2	23.5
CBW-12N-B □ -10 ~ 30				N-PR-22	Torque [N·m]	166	167	213	_	_	_	1.2	25
CD#12H-D = 10 . 0 30	12	152.4	B-1	14-1-11-22	O.H.L. [N]	1715	2528	2871	-	_	-	1.2	23
CBW-12N-B □ -40 ~ 60	12	(6 in.)	D-1	N-PR-25	Torque [N·m]	_	-	-	373	352	336	2.9	40
CBW-12N-B40 ** 60				IN-F N-23	O.H.L. [N]	_	_	-	3665	3783	4126	2.9	40

Dimensions (CBW- ☐ N-B ☐)



			-																				
																						Uni	t [mm]
Model									Dimen	sions	of part									Din	nensio	ns of sh	aft
Wodel	A ₁	A ₂	B ₁	B ₂	C ₁	C ₂	G	Н	J	K	L	М	N	Р	R ₁	R ₂	T	Υ	Z	Q	S	U	W
CBW-06N-B □ -10 ~ 30	95	110	130	140	80	130	15	175	56	126	236	15	110	76.2	145	95	80	50	11	40	17	19	5
CBW-06N-B □ -40 ~ 60	105	120	130	150	90	150	20	200	56	131	246	15	115	76.2	165	110	80	60	11	50	22	24.5	6
CBW-08N-B \square -10 \sim 30	105	120	130	150	90	150	20	201	59	137	260	18	123	101.6	165	110	100	60	11	50	22	24.5	6
CBW-08N-B □ -40 ~ 60	115	150	150	190	105	175	25	230	61	154	294	18	140	101.6	195	130	100	70	15	60	28	31	8
CBW-10N-B \square -10 \sim 30	115	150	150	190	105	175	25	238.5	68	164	312	21	148	127	195	130	125	70	15	60	28	31	8
CBW-10N-B □ -40 ~ 60	135	180	170	220	120	200	25	265	63	174	332	21	158	127	210	140	125	80	15	65	32	35	10
CBW-12N-B \square -10 \sim 30	135	180	170	220	120	200	25	276	67.5	179	345	21	166	152.4	210	140	150	80	15	65	32	35	10
CBW-12N-B □ -40 ~ 60	155	220	190	270	150	250	25	370	76.5	210	405	23.5	195	152.4	260	170	150	100	15	75	38	41	10

How to Place an Order

CBW-06N-BR-10

Bellpony Co., Ltd.: B

Speed reduction ratio 1/\(\subseteq: 10, 20, 30, 40, 50, 60\) Speed reducer Output shaft direction

R: Right side of the output shaft as viewed from the input pulley L: Left side of the output shaft as viewed from the input pulley

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES ELECTROMAGNETIC CLUTCH & BRAKE

UNITS SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS 121- 🗆 -20G 126 CBW CMW 121- 🗆 -10G 122

C013

CBW Models

List of Stand-alone Clutches and Brakes Used and Recommended Power Supplies and Accessory Parts [CBW- 🗆 N-H 🔲]

Model	Stand-alone clutch	Stand-alone braking	Dagwing wound as	Recommended power	Accessory parts
Model	system	system	Bearing number	supplies	Circuit protector (Varistor), qty. 2
CBW-06N-H □	101-06-13-A-110	111-06-11G 24V 15JIS	6002	BEH-10G	NVD07SCD082 or an equivalent
CBW-08N-H □	101-08-13-A-102	111-08-11G 24V 17JIS	6003	BEH-10G	NVD07SCD082 or an equivalent
CBW-10N-H □	101-10-13-A-113	111-10-11G 24V 20JIS	6004	BEH-10G	NVD07SCD082 or an equivalent
CBW-12N-H □	101-12-13-A-134	111-12-11G 24V 25JIS	6005	BEH-10G	NVD07SCD082 or an equivalent

^{*} NVD

SCD

parts are manufactured by KOA Corporation.

List of Stand-alone Clutches and Brakes Used and Recommended Power Supplies and Accessory Parts (CBW- 🗆 N-B 🔲)

Model	Stand-alone clutch	Stand-alone braking	Bearing number	Recommended power	Accessory parts
Model	system	system	bearing number	supplies	Circuit protector (Varistor), qty. 2
CBW-06N-B \square -10 \sim 30	101-06-13-A-110	111-06-11G 24V 15JIS	6002	BEH-10G	NVD07SCD082 or an equivalent
CBW-06N-B □ -40 ~ 60	101-06-13-A-110	111-06-11G 24V 15JIS	6002	BEH-10G	NVD07SCD082 or an equivalent
CBW-08N-B \square -10 \sim 30	101-08-13-A-102	111-08-11G 24V 17JIS	6003	BEH-10G	NVD07SCD082 or an equivalent
CBW-08N-B □ -40 ~ 60	101-08-13-A-102	111-08-11G 24V 17JIS	6003	BEH-10G	NVD07SCD082 or an equivalent
CBW-10N-B \square -10 \sim 30	101-10-13-A-113	111-10-11G 24V 20JIS	6004	BEH-10G	NVD07SCD082 or an equivalent
CBW-10N-B □ -40 ~ 60	101-10-13-A-114	111-10-11G 24V 25JIS	6005	BEH-10G	NVD07SCD082 or an equivalent
CBW-12N-B \square -10 \sim 30	101-12-13-A-134	111-12-11G 24V 25JIS	6005	BEH-10G	NVD07SCD082 or an equivalent
CBW-12N-B □ -40 ~ 60	101-12-13-A-135	111-12-11G 24V 30JIS	6006	BEH-10G	NVD07SCD082 or an equivalent

^{*} NVD

SCD

parts are manufactured by KOA Corporation.

^{*} Varistors need not be used when a BEH model overexcitation electromagnetic power supply is used. For details, refer to the section on power supplies.

^{*} Varistors need not be used when a BEH model overexcitation electromagnetic power supply is used. For details, refer to the section on power supplies.

Selecting a CBW Worm Reducer

For speed reducers with clutches/brakes, loads start and stop abruptly, so load inertia and the like place large loads on worm wheels. Select a worm reducer based on frequency of use, load inertia, usage time, and the like, with due consideration to safety rates.

• Determining speed reduction ratio I

Speed of output shaft rotation N₂ [min ⁻¹] Speed reduction ratio I = Speed of input shaft rotation N₁ [min - 1]

· Calculating equivalent torque

Equivalent torque Te $[N \cdot m]$ = Load torque Tf $[N \cdot m] \times$ Load coefficient Sf × Frequency coefficient Sh

9550 × kW × E Load torque Tf [N·m] = N₂

kW: Input Wattage [kW]

E: Speed reducer efficiency [%]/100

* See the speed reducer manufacturer's catalog for the speed reducer efficiency.

N2: Output rotation speed [min⁻¹]

· Load coefficient Sf and frequency coefficient Sh Find the equivalent value for conditions such as load type, time, and frequency of use.

Load coefficient Sf

Load type Continuous time	Uniform load	Normal shock	Sharp shock
Up to 2 hrs.	0.80	1.00	1.25
Up to 8 hrs.	1.00	1.25	1.50
Up to 24 hrs.	1.25	1.50	1.75

Frequency coefficient Sh

For sharp starts and stops due to clutch/brake 1.5
--

· Provisional selection of speed reducer Select a speed reducer from the specifications table for which equivalent torque Te \leq rated output torque T.

• Calculating the equivalent overhang load (O.H.L.) O.H.L. refers to the load that acts to bend the shaft when transmitting power using a chain or the like.

Equivalent O.H.L.= $\frac{\text{Te} \times \text{K} \times (\text{L+0.57} \times \text{Ls})}{\text{R} \times 1.07 \times \text{Ls}}$

Te: Equivalent torque [N•m]

- K: Factor based on type of transmission tool
- R: Pitch radius of transmission tool [m]
- Ls: Length of standard shaft [mm]
- L: Distance from shaft base to load center [mm]

Transmission tool	Chain timing belt	Gear	V belt	Flat belt
K	1.00	1.25	1.50	2.50

Use the specifications to confirm that equivalent O.H.L \leq rated O.H.L. If this condition is not satisfied, change Te, L or R, or increase the selected output.

Operational Cautions

- Before starting, check that the speed reducer has a good amount of oil.
- Loosen or remove the air vent screw or pin.
- Break in the reducer, guided by the manual from the speed reducer
- Periodically replace the oil. Be careful when doing this to not get any oil whatsoever on the clutch and brake parts.

Recommended speed reducer lubricants table

Ambient temperature [°C]	0 ~ 40				
ISO viscosity grade	VG320				
Idemitsu Kosan	Daphne Super Gear Oil 320				
JX Nippon Oil & Energy	Bonnock 320				
Cosmo Oil	Cosmo Gear SE320				
Showa Shell Sekiyu	Omara 320				
Jomo Oil	Reductus 320				
Mobil Oil	Mobilgear 632 (320)				

^{*} Check the volume of oil for speed reducers on the specifications table.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** FI FCTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES**

> **ELECTROMAGNETIC CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS 121- -20G 126 CBW CMW 121- 🗌 -10G 122

CMW Models Clutch/Brake Units - Motor/Speed Reducer-integrated Type

Specifications

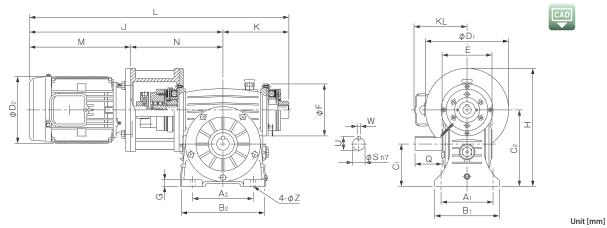
		Dynamic	Static		Coil (at	t 20℃)		Heat	Rotating part	Total work performed				
Model	Size	friction torque T _d [N·m]	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	at resistance class	moment of until readjustment of J [kg·m²] the air gap		Armature pull-in time ta [s]	Torque build-up time t _P [s]	Torque decaying time td [s]	
CMW-06N-H□H	06	5	5.5	DC24	11	0.46	52	В	1.66 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	
CMW-08N-H□H	08	10	11	DC24	15	0.63	38	В	4.78 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	
CMW-10N-H□H	10	20	22	DC24	20	0.83	29	В	1.71 × 10 ⁻³	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	
CMW-12N-H□H	12	40	45	DC24	25	1.09	23	В	4.53 × 10 ⁻³	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	

^{*} The dynamic friction torque, $T_{\rm d}$, is measured at a relative speed of 100 $\rm min^{\text{-}1}$

		Motor output	Speed reducer									
Model	Size	[kW]	Model	Output shaft rated		S	peed reduct	ion ratio 1/[Oil volume	Mass [kg]
		3-phase 4-pole	Model	values	10	20	30	40	50	60	[ℓ]	- 3-
CMW-06N-H□H	06	0.2	N-2SA	Torque [N·m]	78.2	79.9	85.3	78.6	88.9	76.1	0.5	16
CMW-UON-H L H	00	0.2	N-23A	O.H.L. [N]	1770	2280	2620	2930	3160	3230	0.5	10
CMW-08N-H □ H	08	0.4	N-2A	Torque [N·m]	79.8	102	86.9	104	98.5	100	0.5	32
CMW-00N-H L H	06	0.4	IN-ZA	O.H.L. [N]	1760	2240	2630	2880	3140	3230	0.5	32
CMW-10N-H □ H	10	0.75	N-3A	Torque [N·m]	165	180	180	188	187	164	1.0	4.4
CMW-TUN-H H	10	0.75	IN-3A	O.H.L. [N]	2250	2900	3370	3720	4040	4370	1.0	44
CMW-12N-H□H	12	1.5	N-4A	Torque [N·m]	292	293	301	302	-	-	2.0	72
CMW-IZN-H □ H	12	1.5	N-4A	O.H.L. [N]	2780	3640	4210	4680	_	_	2.0	72

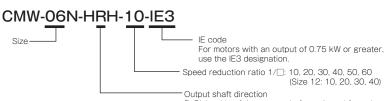
- * The induction motors are fully sealed external fan motors that conform to the JIS C4210 standard (for 0.2 kW and 0.4 kW models) or the JIS C 4213 standard (for 0.75 kW mode
- * The power supplies for the motors are 3-phase, 200 V AC at 50 Hz, or 200/220 V AC at 60 Hz.
 * If you desire a special voltage (5 Power Supply Specifications), different number of poles, or the like for the induction motor, contact Miki Pulley.

Dimensions



Model										Dimensions of part								Dimensions of shaft					
Model	A ₁	A ₂	B ₁	B ₂	C ₁	C ₂	D ₁	D ₂	E	F	G	Н	J	K	KL	L	M	N	Z	Q	S	U	W
CMW-06N-H ☐ H	105	105	132	157	75	135	160	130	110	86	15	215	375	117	-	492	205	170	12	50	25	28	8
CMW-08N-H ☐ H	115	112	140	165	82	146	160	145	110	100	15	226	412	135	124	547	225	187	11	50	25	28	8
CMW-10N-H ☐ H	125	146	155	200	102	184	200	163	120	125	16	284	465	159	131	636	243	222	12	65	30	33	8
CMW-12N-H ☐ H	150	168	186	245	118	213	210	182/176	150	150	20	318	529	185	148.5	726	274	255	14	75	35	38	10

How to Place an Order



R: Right side of the output shaft as viewed from the motor side L: Left side of the output shaft as viewed from the motor side

^{*} Speed reducer is made by Hirai Reduction Gear Manufacturing Co.

List of Stand-alone Clutches and Brakes Used and Recommended Power Supplies and Accessory Parts (CBW- 🗆 N-H 🗔)

Model	Stand-alone clutch system	Stand-alone braking	Bearing	Counting tops	Recommended	Accessory parts
Model	Stand-alone clutch system	system	number	Coupling type	power supplies	Circuit protector (Varistor), qty. 2
CMW-06N-H ☐ H	101-06-13G 24V 15JIS	111-06-11G 24V 15JIS	6002	CF-A-001-01-T5	BEH-10G	NVD07SCD082 or an equivalent
CMW-08N-H ☐ H	101-08-13G 24V 17JIS	111-08-11G 24V 17JIS	6003	CF-A-002-01-1360-14N	BEH-10G	NVD07SCD082 or an equivalent
CMW-10N-H ☐ H	101-10-13G 24V 20JIS	111-10-11G 24V 20JIS	6004	CF-A-002-01-1360-19N	BEH-10G	NVD07SCD082 or an equivalent
CMW-12N-H ☐ H	101-12-13G 24V 25JIS	111-12-11G 24V 25JIS	6005	CF-A-004-01-1360-24N	BEH-10G	NVD07SCD082 or an equivalent

NVD SCD parts are manufactured by KOA Corporation

Selecting a CMW Worm Reducer

For speed reducers with clutches/brakes, loads start and stop abruptly, so load inertia and the like place large loads on worm wheels. Select a worm reducer based on frequency of use, load inertia, usage time, and the like, with due consideration to safety rates.

• Determining speed reduction ratio I

Speed of output shaft rotation N₂ [min⁻¹] Speed reduction ratio I = Speed of input shaft rotation N₁ [min - 1]

· Calculating equivalent torque

Equivalent torque Te $[N \cdot m]$ = Load torque Tf $[N \cdot m] \times$ Load coefficient Sf × Frequency coefficient Sh

 $9550 \times kW \times E$ Load torque Tf [N·m] =

kW: Input Wattage [kW]

E: Speed reducer efficiency [%]/100

* See the speed reducer manufacturer's catalog for the speed reducer efficiency.

N₂: Output rotation speed [min⁻¹]

• Load coefficient Sf and frequency coefficient Sh Find the equivalent value for conditions such as load type, time, and frequency of use.

■ Load coefficient Sf

	Load type	Uniform load	Normal shock	Sharp shock		
	Continuous time	Officialiticau	NOTHIAI SHOCK	Sharp shock		
	Up to 2 hrs.	0.80	1.00	1.25		
	Up to 8 hrs.	1.00	1.25	1.50		
	Up to 24 hrs.	1.25	1.50	1.75		

■ Frequency coefficient Sh

For sharp starts and stops due to clutch/brake	1.5
--	-----

• Provisional selection of speed reducer Select a speed reducer from the specifications table for which equivalent torque $Te \le rated$ output torque T.

· Calculating the equivalent overhang load (O.H.L.) O.H.L. refers to the load that acts to bend the shaft when transmitting power using a chain or the like.

Equivalent O.H.L.= $\frac{\text{Te} \times \text{K} \times (\text{L+0.57} \times \text{Ls})}{\text{R} \times 1.07 \times \text{Ls}}$

Te: Equivalent torque [N•m]

- K: Factor based on type of transmission tool
- R: Pitch radius of transmission tool [m]
- Ls: Length of standard shaft [mm]
- Distance from shaft base to load center [mm]

Transmission tool	Chain timing belt	Gear	V belt	Flat belt
K	1.00	1.25	1.50	2.50

Use the specifications to confirm that equivalent O.H.L \leq rated O.H.L. If this condition is not satisfied, change Te, L or R, or increase the selected output.

Operational Cautions

- Before starting, check that the speed reducer has a good amount of oil.
- Loosen or remove the air vent screw or pin.
- \bullet Break in the reducer, guided by the manual from the speed reducer manufacturer.
- Periodically replace the oil. Be careful when doing this to not get any oil whatsoever on the clutch and brake parts.

Recommended speed reducer lubricants table

Ambient temperature [°C]	0 ~ 40
ISO viscosity grade	VG320
Idemitsu Kosan	Daphne Super Gear Oil 320
JX Nippon Oil & Energy	Bonnock 320
Cosmo Oil	Cosmo Gear SE320
Showa Shell Sekiyu	Omara 320
Jomo Oil	Reductus 320
Mobil Oil	Mobilgear 632 (320)

■ List of speed reducer oil volumes

Speed reducer type	Oil volume [ℓ]
N-2SA	0.5
N-2A	0.5
N-3A	1.0
N-4A	2.0

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES FLECTROMAGNETIC ACTUATED **CLUTCHES & BRAKES**

> ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS 121- -20G 126 CBW CMW 121- 🗌 -10G 122

C014

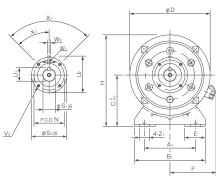
Varistors need not be used when a BEH model overexcitation electromagnetic power supply is used. For details, refer to the section on power supplies

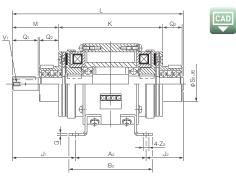
-10G Types Double Clutch Units

Specifications

Model Si			friction			t 20°C)		Heat re	Max. rotation	Rotating part moment of inertia J [kg·m²]		Total work performed until	Armature	Torque build-up	Torque decaying	Mass
Model	ze	T _d [N·m]	T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	: resistance class	speed [min ⁻¹]	For hub input	For shaft input	readjustment of the air gap E _T [J]	pull-in time ta [s]	time t _p [s]	time td [s]	[kg]
121-06-10G	06	5	5.5	DC24	11	0.46	52	В	3000	1.55 × 10 ⁻⁴	1.05 × 10 ⁻⁴	36 × 10 ⁶	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	1.7
121-08-10G	08	10	11	DC24	15	0.63	38	В	3000	4.75 × 10 ⁻⁴	3.00 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	3.1
121-10-10G	10	20	22	DC24	20	0.83	29	В	3000	1.44 × 10 ⁻³	9.45 × 10 ⁻⁴	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	6.5
121-12-10G	12	40	45	DC24	25	1.09	23	В	3000	4.50 × 10 ⁻³	2.75×10^{-3}	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	10.5
121-16-10G	16	80	90	DC24	35	1.46	16	В	3000	1.34 × 10 ⁻²	9.05×10^{-3}	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	21
121-20-10G	20	160	175	DC24	45	1.88	13	В	2500	4.18 × 10 ⁻²	2.65 × 10 ⁻²	10 × 10 ⁸	C:0.090 B:0.065	C:0.250 B:0.200	C:0.130 B:0.070	38.5
121-25-10G	25	320	350	DC24	60	2.50	9.6	В	2000	9.80 × 10 ⁻²	7.45 × 10 ⁻²	20 × 10 ⁸	C:0.115 B:0.085	C:0.335 B:0.275	C:0.210 B:0.125	70

Dimensions





																	ı	Jnit [mm]
Size									Dimensio	ns of part								
ze	A ₁	A ₂	B ₁	B ₂	С	D	E	F	G	Н	J ₁	J_2	K	L	M	N	Z ₁	Z ₂
06	52.5	75	80	90	55	80	27.5	53	2.6	95	65.5	40.5	111.5	181	47	33	13.5	6.5
08	65	90	90	105	65	100	27.5	61	2.6	115	78.5	48.5	133	217	57	37	13.5	6.5
10	80	110	110	130	80	125	32.5	72	3.2	142.5	98	58	162	266	72	47	15.5	9
12	105	135	140	160	90	150	35	81	3.2	165	121	71	193	327	92	52	20	11.5
16	135	160	175	185	112	190	42.5	97	4.5	207	149	87.5	232	397	113	62	24.5	11.5
20	155	200	200	230	132	230	45	109	6	247	187	105	290	492	142	74.5	28	14
25	195	240	240	270	160	290	47.5	124	20	305	238	125	350	603	183	101.5	28	14

Size	Dimensions of shaft												
ze	\mathbf{Q}_1	\mathbf{Q}_2	S ₁	S ₂	U ₁	U ₂	V ₁	V ₂	X ₁	X ₂	W _{1,2}		
06	25	20	11	38	12.5	39.5	M4 \times 0.7, length: 8	3-M4 imes 0.7, length: 4	3-120°	60°	4		
08	30	25	14	45	16	47	M4 × 0.7, length: 8	3-M4 × 0.7, length: 6	3-120°	60°	5		
10	40	30	19	55	21	57	M6 × 1, length: 11	$4\text{-M4} \times 0.7$, length: 8	4-90°	45°	5		
12	50	40	24	64	27	67	M6 × 1, length: 11	4-M4 × 0.7, length: 8	4-90°	45°	7		
16	60	50	28	75	31	78	M6 × 1, length: 11	6-M5 × 0.8, length: 8	6-60°	30°	7		
20	80	60	38	90	41.5	93.5	M10 × 1.5, length: 17	4-M6 × 1, length: 12	4-90°	45°	10		
25	110	70	42	115	45.5	118.5	M10 × 1.5, length: 17	8-M6 × 1, length: 12	8-45°	22.5°	12		

^{*} The input/output keyways are old JIS standard class 2 while the key is old JIS standard class 1. Note that the keyway dimensions of the unit hub part do not conform to the old JIS standard. Check them on the dimensions table above.

How to Place an Order

121-<u>06</u>-10G

 $^{^{\}star}$ The rotating part moment of inertia for shaft input is the value with one armature type-5.

^{*} When inserting pulleys or the like onto input/output shafts, use the supplied insertion set.

* The 121-25-10G base is a casting.

List of Stand-alone Clutches Used

Model	Chand alone ships because	Bearing	number
Model	Stand-alone clutch system	Main shaft part	Hub part
121-06-10G	101-06-15G 24V R15JIS A12JIS	6202	6001
121-08-10G	101-08-15G 24V R20JIS A15JIS	6004	6002
121-10-10G	101-10-15G 24V R25JIS A20JIS	6205	6004
121-12-10G	101-12-15G 24V R30JIS A25JIS	6206	6005
121-16-10G	101-16-15G 24V R40JIS A30JIS	6208	6006
121-20-10G	101-20-15G 24V R50JIS A40JIS	6211	6008
121-25-10G	101-25-15G 24V R60JIS A50JIS	6214	6010

Recommended Power Supplies and Accessory Parts

Model	Recommended			Accessory parts		
Wodei	power supplies	Circuit protector (Varistor), qty. 2	Tightening collar	Screw stock	Presser foot	Hexagonal nut
121-06-10G	BES-20-10	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$, qty. 3	Qty. 1	M4, qty. 3
121-08-10G	BES-20-10	NVD07SCD082 or an equivalent	Qty. 1	M4 × 55, qty. 3	Qty. 1	M4, qty. 3
121-10-10G	BES-20-10	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$, qty. 3	Qty. 1	M4, qty. 3
121-12-10G	BES-20-16	NVD07SCD082 or an equivalent	Qty. 1	M4 \times 55, qty. 2/M6 \times 100, qty. 1	Qty. 1	M4, qty. 2/M6, qty. 1
121-16-10G	BES-20-16	NVD07SCD082 or an equivalent	Qty. 1	M5 $ imes$ 70, qty. 2/M6 $ imes$ 100, qty. 1	Qty. 1	M5, qty. 2/M6, qty. 1
121-20-10G	BES-20-20	NVD07SCD082 or an equivalent	Qty. 1	$M6 \times 160$, qty. $2/M10 \times 220$, qty. 1	Qty. 1	M6, qty. 4/M10, qty. 2
121-25-10G	BES-40-25	NVD07SCD082 or an equivalent	Qty. 1	$M6 \times 160$, qty. $2/M10 \times 220$, qty. 1	Qty. 1	M6, qty. 4/M10, qty. 2

^{*} NVD \square SCD \square parts are manufactured by KOA Corporation.

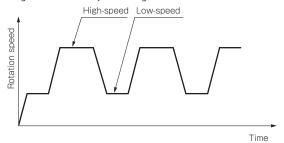
Mounting Example

■ Example When Used in Two-step Speed Change

In two-step speed changing, two hubs are linked respectively to highspeed and low-speed power; by switching the clutches, the output shaft is made to rotate at high speed or low speed.

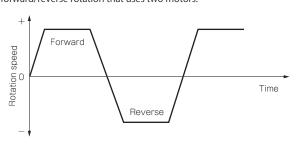
Caution

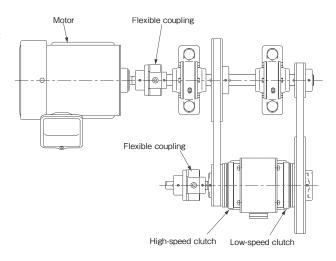
Conversely, when using the shaft as the input, one of the clutches is made to rotate at very high speed at some speed change ratios, so the bearings and the like may be damaged.

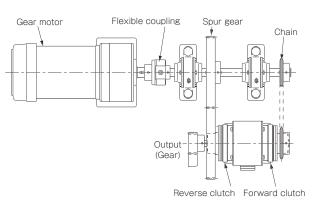


Example When Used in Forward/Reverse Operation

This unit does not have a brake, so forward/reverse operation is effective at relatively low speeds and light loads. In the example depicted, forward/reverse rotation is obtained from the drive-side rotation shaft with a chain and spur gear, and engages the individual hubs. By switching the clutches, the output shaft goes back and forth between forward and reverse rotation. There is also a method of forward/reverse rotation that uses two motors.







C015

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BRAKE MOTORS

POWER SUPPLIES

MODELS

125

121- 🗌 -20G

126 CBW

CMW

121- 🗆 -10G

122

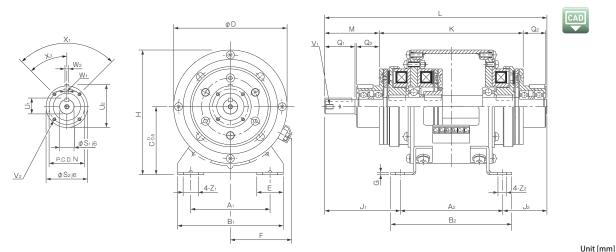
^{*} Recommended BES model power supplies are required for each clutch. Varistors need not be used when a BES model is used. For details, refer to the section on power supplies

122 Models Double Clutch/Brake Units

Specifications

		Dynamic	Static	Co	oil (at	20°C)	Ŧ			Total work				
Model	Size	friction torque T _d [N·m]	friction torque Ts [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat resistance class	Max. rotation speed [min ⁻¹]	Rotating part moment of inertia J [kg·m²]	performed until readjustment of the air gap Et [J]	Armature pull-in time ta [s]	Torque build-up time t _P [s]	Torque decaying time td [s]	Mass [kg]
122-06-20G	06	5	5.5	DC24	11	0.46	52	В	3000	2.19 × 10 ⁻⁴	36×10^6	C:0.020 B:0.015	C:0.041 B:0.033	C:0.020 B:0.015	4
122-08-20G	08	10	11	DC24	15	0.63	38	В	3000	6.55 × 10 ⁻⁴	60 × 10 ⁶	C:0.023 B:0.016	C:0.051 B:0.042	C:0.030 B:0.025	6
122-10-20G	10	20	22	DC24	20	0.83	29	В	3000	2.12×10^{-3}	130 × 10 ⁶	C:0.025 B:0.018	C:0.063 B:0.056	C:0.050 B:0.030	9
122-12-20G	12	40	45	DC24	25	1.09	23	В	3000	6.35 × 10 ⁻³	250 × 10 ⁶	C:0.040 B:0.027	C:0.115 B:0.090	C:0.065 B:0.050	17
122-16-20G	16	80	90	DC24	35	1.46	16	В	3000	1.99 × 10 ⁻²	470 × 10 ⁶	C:0.050 B:0.035	C:0.160 B:0.127	C:0.085 B:0.055	29
122-20-20G	20	160	175	DC24	45	1.88	13	В	2500	6.15 × 10 ⁻²	10 × 10 ⁸	C:0.090 B:0.065	C:0.250 B:0.200	C:0.130 B:0.070	58

Dimensions



																		····· []
Size	Dimensions of part																	
Ze	\mathbf{A}_1	A ₂	B ₁	B ₂	С	D	E	F	G	Н	J ₁	J_2	K	L	M	N	Z ₁	Z ₂
06	65	90	90	105	65	100	27.5	61	2.6	115	73	48	142	211	47	33	13.5	6.5
08	80	110	110	130	80	125	32.5	72	3.2	142.5	83	53	162	246	57	37	15.5	9
10	105	135	140	160	90	150	35	81	3.2	165	100	59	190	294	72	47	20	11.5
12	135	160	175	185	112	190	42.5	97	4.5	207	124	74	222	358	93	52	24.5	11.5
16	155	200	200	230	132	230	45	109	6	247	150.5	89.5	272	440	114.5	62	28	14
20	195	240	240	270	160	290	47.5	124	20	305	197	114	348	551	143	74.5	28	14

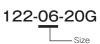
Size	Dimensions of shaft											
ze	\mathbf{Q}_1	\mathbf{Q}_2	S ₁	S ₂	U ₁	U ₂	V ₁	V ₂	X ₁	X ₂	W _{1,2}	
06	25	20	11	38	12.5	39.5	M4 \times 0.7, length: 8	$3-M4 \times 0.7$, length: 4	3-120°	60°	4	
08	30	25	14	45	16	47	M4 \times 0.7, length: 8	3-M4 × 0.7, length: 6	3-120°	60°	5	
10	40	30	19	55	21	57	M6 \times 1, length: 11	$4\text{-M4} \times 0.7$, length: 8	4-90°	45°	5	
12	50	40	24	64	27	67	M6 × 1, length: 11	4-M4 × 0.7, length: 8	4-90°	45°	7	
16	60	50	28	75	31	78	M6 × 1, length: 11	6-M5 × 0.8, length: 8	6-60°	30°	7	
20	80	60	38	90	41.5	93.5	M10 × 1.5, length: 17	4-M6 × 1, length: 12	4-90°	45°	10	

^{*} The output keyways are old JIS standard class 2 while the key is old JIS standard class 1. Note that the keyway dimensions of the unit hub part do not conform to the old JIS standard. Check them on the dimensions table above.

* When inserting pulleys or the like onto output shafts, use the supplied insertion set.

* The 122-20-20G base is a casting.

How to Place an Order



List of Stand-alone Clutches and Brakes Used

Model	Stand-alone clutch system	Stand-alone braking system	Bearing number			
Model	Stand-alone clutch system	Stand-alone braking system	Main shaft part	Hub part		
122-06-20G	101-06-15G 24V R15JIS A12JIS	111-06-12G 24V 15JIS	6202	6001		
122-08-20G	101-08-15G 24V R20JIS A15JIS	111-08-12G 24V 20JIS	6004	6002		
122-10-20G	101-10-15G 24V R25JIS A20JIS	111-10-12G 24V 25JIS	6205	6004		
122-12-20G	101-12-15G 24V R30JIS A25JIS	111-12-12G 24V 30JIS	6206	6005		
122-16-20G	101-16-15G 24V R40JIS A30JIS	111-16-12G 24V 40JIS	6208	6006		
122-20-20G	101-20-15G 24V R50JIS A40JIS	111-20-12G 24V 55JIS	6211	6008		

Recommended Power Supplies and Accessory Parts

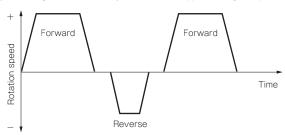
Model	Recommended			Accessory parts		
wodei	power supplies	Circuit protector (Varistor), qty. 3	Tightening collar	Screw stock	Presser foot	Hexagonal nut
122-06-20G	BES-20-10	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$, qty. 3	Qty. 1	M4, qty. 3
122-08-20G	BES-20-10	NVD07SCD082 or an equivalent	Qty. 1	$M4 \times 55$, qty. 3	Qty. 1	M4, qty. 3
122-10-20G	BES-20-10	NVD07SCD082 or an equivalent	Qty. 1	M4 $ imes$ 55, qty. 2/M6 $ imes$ 100, qty. 1	Qty. 1	M4, qty. 2/M6, qty. 2
122-12-20G	BES-20-16	NVD07SCD082 or an equivalent	Qty. 1	M4 × 55, qty. 2/M6 × 100, qty. 1	Qty. 1	M4, qty. 2/M6, qty. 2
122-16-20G	BES-20-16	NVD07SCD082 or an equivalent	Qty. 1	M5 \times 70, qty. 2/M6 \times 100, qty. 1	Qty. 1	M5, qty. 2/M6, qty. 2
122-20-20G	BES-20-20	NVD07SCD082 or an equivalent	Qty. 1	$M6 \times 160$, qty. $2/M10 \times 220$, qty. 1	Qty. 1	M6, qty. 2/M10, qty. 2
			/-			3.13

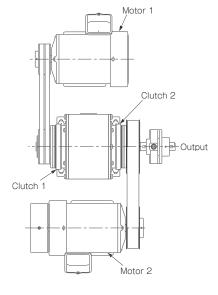
^{*} NVD \square SCD \square parts are manufactured by KOA Corporation.

Mounting Example

■ Example When Used in Forward/Reverse Operation

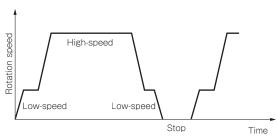
This is an example of forward/reverse rotation using two motors. The motor rotates continuously, forward and reverse operation are achieved by switching clutches, and any load can be stopped during that period.

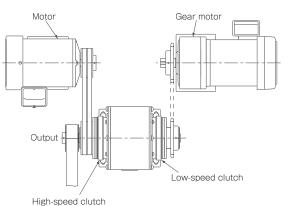




Example When Used in Two-step Speed Change/Stop

High-precision stopping at a predetermined position, winding control on winders, and the like can be controlled simply and with high precision by using this unit to perform a series of operations: slow, fast, slow, stop.





Web code

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SPRING-ACTUATED BRAKE

UNITS

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BRAKE MOTORS

POWER SUPPLIES

MODELS

125

121- 🗌 -20G

126

CBW

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121- 🗆 -10G

122

^{*} Recommended BES power supplies are available for each clutch/brake. Varistors need not be used when a BES model is used. For details, refer to the section on power supplies

The Selection Process

Key Issues for Selection

Because of their good controllability, clutches and brakes are often used for complex controls rather than simple on/off operations.

If a size is chosen based solely on torque, problems can unexpectedly result

When choosing a size, many factors must be considered, including load properties and the layout of the mechanism that incorporates the clutch or brake. In this section on selecting sizes, we explain how to make selections for a variety of situations, and also give calculation examples and data needed for selections.

■ Motors and clutches/brakes

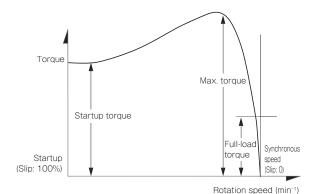
· Relationship between motor output and torque Motor size is expressed as output, but clutches and brakes are expressed as torque. The following relationship obtains between this torque and motor output.

- P: Motor output [kW]
- nr: Rotation speed of clutch/brake shaft [min-1]
- η : Transmission efficiency from motor to clutch/brake
- Variance of characteristics

Motors have different torque characteristics from clutches and brakes. That requires that the various characteristics be factored in when using a motor as the drive source and starting and stopping loads with a clutch/brake.

Motor characteristics

Motors can generate torque of 200% of total load torque or more at startup, pass through maximum torque while accelerating, and drive the load near the full load torque that enables stable operation. If load increases during rotation, the motor can lower its own rotation speed and drive the load at a rotation speed that generates high torque. The figure below shows the relationship between motor torque and rotation speed characteristics.



Clutch/brake torque characteristics

The clutch/brake characteristics are determined by the upper limits of engaging and braking torque, as described in the section on torque characteristics. Load torque beyond that causes slipping at the frictional surface.

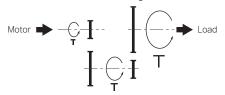
Knowing these differences in characteristics from the beginning enables you to select the clutch/brake suited for your load conditions. A clutch/brake that has a torque value that is 200 to 250% of the full load torque of the motor will normally be suited to a wide range of applications, factoring in reasonable safety considerations when selecting it.

■ Relationship between torque and rotation speed

• Torque and rotation speed are inversely proportional

Shafts within machinery that are rotating the fastest can be made to rotate with little force, but decelerated slow-rotating shafts require large amounts of force to make them rotate.

In other words, torque and rotation speed are inversely proportional. This is very important for the selection of clutches and brakes. The size and service life of a clutch or brake can change depending on how fast the shaft it is used on is rotating



· In combination with speed changers

If you are using the clutch/brake within a mechanism that can change rotation speed, such as a stepless speed changer, you must select a clutch/brake that does not fall short on torque at low speeds and that satisfies needs for response and service life at high speeds.

Ascertaining load properties

Clutch and brake engaging time, wear life, and the like will vary with the properties of the load being engaged or braked. For that reason, if the load is not ascertained as accurately as possible, even slight changes in load conditions can mean the system will not work adequately.

As it happens, such load properties are quite diverse, and thus difficult to ascertain. Often, users today will determine them empirically.

· Importance of safety factor

When determining the size of the clutch or brake, determine the required torque by multiplying by an empirically derived factor. Once the drive part has been determined, we use an empirical factor K based on the type of drive source used.

If this factor is too small, slipping and other problems can occur when conditions deteriorate; if it is too large, the load on the driver increases, which can cause driver problems when overloads occur.

Types of drivers	Motor/ turbine	Gasoline engine	Diesel engine (1 or 2 cylinder gasoline engine)
Factor K	2 ~ 2.5	2.5 ~ 2.8	2.8 ~ 3.4

• Load torque and moment of inertia

Load torque comes from resistance from the machinery and from resistance applied after engagement (cutting resistance, etc.).

Load torque is generally difficult to determine and is therefore sometimes ignored during size selection. For clutches, however, this can lead to inadequate torque, so it requires attention.

Moment of inertia is also called the flywheel effect. It is a quantity that represents the difficulty of getting an object to move or the difficulty of stopping it.

When designing a mechanism, the work of the clutch and brake are lessened by making the load on the clutch as small as possible while making the brake load somewhat larger. If the moment of inertia is made as small as possible, response and service life are improved.

And since the clutch and brake have inertia of their own, that inertia must be added to calculations.

Selection

Simple Selection Graph

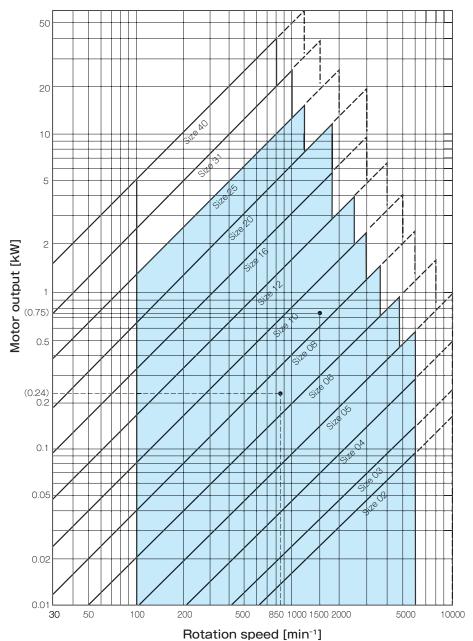
This selection graph applies to cases in which the drive source is a motor, load is relatively light, and frequency is low. The clutch/brake size can be determined easily when the motor used is appropriate to the load, the mechanism between motor and clutch/brake is not complex, and there is no high-inertia body to assist drive.

This table is for a safety factor K of 2.5 (ordinary use). You can use this table to select a clutch/brake with other factors. For the vertical axis [kW], use the value obtained by multiplying the motor output by K/2.5. Selection example

- If the motor output is 0.75 kW and the clutch/brake rotation speed is $1500 \, \text{min}^{-1}$, select the size at their intersection, which is size 10.
- \bullet To get K = 1.5 when the motor output is 0.4 kW and the clutch/brake rotation speed is 850 min $^{-1}$:

$$0.4 \, [kW] \times \frac{1.5}{2.5} = 0.24 \, [kW]$$

Find 0.24 kW on the vertical axis of the table and find the intersection with 850 min⁻¹. The size to select is size 08.



area. Inside the dotted line area on the right, the amount of energy, heat dissipation, friction or the like may not satisfy requirements, so check them.
Within the bold line under 100 min⁻¹, use the equation to check the required torque.

* Contact Miki Pulley regarding sizes 31 and 40.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ACTUATED MICRO **CLUTCHES & BRAKES** FLECTROMAGNETIC ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC CLUTCH & BRAKE UNITS

ELECTROMAGNETIC-

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

Consideration of Torque

■ Total load torque of motor (TM)

The total load torque translated to the clutch/brake mounting shaft is:

$$T_{M} = \frac{9550 \cdot P}{n_{r}} \eta [N \cdot m] \cdots (1)$$

P: Motor output [kW]

nr: Rotation speed of clutch/brake shaft [min-1]

 η : Transmission efficiency from motor to clutch/brake

\blacksquare Load torque (T ℓ)

Load torque is difficult to determine through calculations, so it is either determined empirically or by direct measurement.

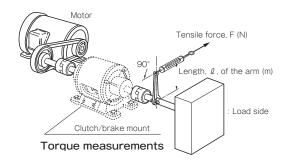
· When determined from motor capacity To select a motor correctly for a load, the TM of Eq. (1) is used as the load torque.

$$\mathsf{T} \ell = \mathsf{T} \mathsf{M} \left[\mathsf{N} \cdot \mathsf{m} \right] \cdots (2)$$

• When measured and then determined

The load can be actually measured to find an accurate $T\ell$. It can be measured using a torque wrench, or, as in the figure below, the shaft where the clutch or brake will be mounted can be rotated and the value found as the product of the force F to start the load rotating and the length of the arm $\,\ell\,$.

$$\mathsf{T}\ell = \ell \cdot \mathsf{F} [\mathsf{N} \cdot \mathsf{m}] \cdots (3)$$



· Sign of load torque

Load torque in the equation is shown with a plus or minus sign. For a clutch, it is applied in the direction that opposes rotation, so it is subtracted from clutch torque Ta; for a brake, it is applied in the direction that assists braking, so it is added to brake torque Ta. (In the rare cases in which it works the opposite way, change the signs when calculating.) In the equation, it is expressed as $\pm\,T\,\ell\,$. Use the value as appropriate.

■ Acceleration/deceleration torque (T_a)

• The torque required to accelerate a load is:

$$T_a = \frac{J \cdot n_r}{9.55 t_{ae}} [N \cdot m] \qquad (4)$$

tae: Actual engagement time (acceleration time) of clutch [s]

J: Total moment of inertia engaged by the clutch [kg·m²]

• The torque required to decelerate a load is:

$$T_a = \frac{J \cdot n_r}{9.55 t_{ab}} [N \cdot m] \cdots (5)$$

tab: Actual braking time (deceleration time) of brake [s]

J: Total moment of inertia braked by the brake [kg·m²]

■ Required torque (T)

Torque required to drive (brake) a load may be as follows, depending on conditions.

• When J and Tℓ are applied while engaged

$$T = (T_a \pm T_\ell) K [N \cdot m] \qquad (6)$$

K is a factor based on load conditions, which has been empirically found to have values like the following. The sign of T_{\ell} is positive for a clutch, since T_ℓ works in the direction that opposes driving, and negative for a brake, since it works in the direction that assists braking.

• When $T\ell$ is nearly all that is applied

$$T = T \ell \cdot K [N \cdot m] \qquad (7)$$

• When J is nearly all that is applied

$$T = T_a \cdot K [N \cdot m]$$
 (8)

· For stationary engagement

When engaging the clutch while stationary and then accelerating the load with the driver, the required torque so that the clutch does not slip when accelerating is:

$$T = \left\{ \frac{J\ell}{J_d + J\ell} \left(T_M - T\ell \right) + T\ell \right\} \quad K [N \cdot m] \quad \cdots \qquad (9)$$

Jd: Total drive-side J from clutch [kg•m²]

 $J\ell$: Total load-side J from clutch [kg•m²]

Safety factor based on load conditions: K

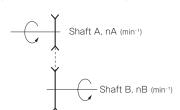
	Usage conditions	Factor K
	Low-frequency use of small inertial body	1.5
Light load	High-frequency use of relatively small inertial body Ordinary use of normal inertial body	2 ~ 2.2
	High-frequency use	2.2 ~ 2.4
	Low-frequency use of small inertial body	2 ~ 2.4
Normal load	Lload Ordinary use	2.4 ~ 2.6
	Driving large inertial body	2.7 ~ 3.2
Heavy load	Operation with shock (large load fluctuation)	3.5 ~ 4.5

■ Translation of torque to other shafts

For the torque of shaft B to be translated to shaft A:

$$T_A = T_B \bullet \frac{n_B}{n_A} [N \bullet m] \qquad (10)$$

TA: Torque of shaft A, TB: Torque of shaft B [N•m] na: Rotation speed of shaft A, nb: Rotation speed of shaft B [min-1]



Consideration of Energy

■ Engaging or braking energy (E_e, E_b)

The energy when a clutch or brake engages or brakes once is:

• For acceleration, engaging energy Ee is:

$$E_{e} = \frac{J \cdot nr^{2}}{182} \cdot \frac{T_{d}}{T_{d} - T_{\ell}} [J] \cdots (11)$$

• For deceleration, braking energy Eb is:

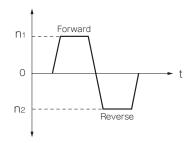
$$E_b = \frac{J \cdot nr^2}{182} \cdot \frac{T_d}{T_d + T_\ell} \quad [J] \cdots (12)$$

• Forward/reverse rotation

The engaging energy of the clutch when using the clutch to switch rotation direction is:

n₁: Forward rotation speed [min⁻¹]

n₂: Reverse rotation speed [min⁻¹]



• Energy when using slip

$$E_{e} = \frac{2 \pi}{60} \cdot \mathbf{n} \cdot \mathbf{t} \cdot \mathbf{T}_{d} [\mathbf{J}]$$
 (14)

$$E_b = \frac{2 \pi}{60} \cdot \mathbf{n} \cdot \mathbf{t} \cdot \mathbf{T}_d [J] \qquad (15)$$

t: Slip time [s]

n: Rotation speed that forces slip $[\min^{-1}]$

Td: Dynamic friction torque at n $[min^{-1}]$ [N•m]

If the clutch or brake slips as it is being used, unwanted situations such as heat generation can occur, so perform adequate checks.

• Allowable work

Allowable work $E_{ea}\,\ell$ and $E_{ba}\,\ell$ are the values under ideal conditions, so the values of E_e and E_b must be sufficiently smaller than the values of $E_{ea}\,\ell$ and $E_{ba}\,\ell$.

$$\mathsf{E}_{\mathsf{b}} \ll \mathsf{E}_{\mathsf{ba}} \, \ell$$
(17)

* For the values of $E_{ea}\ell$ and $E_{ba}\ell$, see the page on heat dissipation characteristics (P.321).

Energy rate

Since clutches and brakes turn on and off at relatively high frequencies, it is important to investigate whether accumulated heat can be dissipated.

• Engaging energy rate (Pe)

$$P_{e} = \frac{E_{e} \cdot S}{60} \ll P_{ea} \ell [W] \qquad (18)$$

• Braking energy rate (Pb)

$$P_b = \frac{E_b \cdot S}{60} \ll P_{ba} \ell \ [W] \ \cdots \ (19)$$

S: Frequency of operation [RPM]

Allowable energy rates $P_{ea} \ell$ and $P_{ba} \ell$ are the values under ideal conditions, so E_e , E_b and S must be set so these rates are sufficiently small.

* For the values of Eea & and Eba & , see the page on heat dissipation characteristics (P.321).

■ Frequency of engaging/braking (Sa)

The allowable operating frequency Sa determined by heat dissipation is:

$$S_a \ll \frac{-60 P_{ea} \ell}{E_e} [RPM] \quad \cdots \qquad (20)$$

$$S_a \ll \frac{-60P_{ba}\ell}{F_b}$$
 [RPM](21)

This allowable frequency reflects only thermal considerations; in actual use, operating time should also be considered.

Consideration of Operating Time

■ Total engagement/braking time (tte, ttb)

The time the load is engaged or braked by the clutch or brake is the sum of the operating time of the clutch or brake itself and the accelerating/deceleration time.

Total engagement time

$$tte = tid + ta + 01tae [s]$$
 (22)

tid: Initial delay time [s]

ta: Armature pull-in time [s]

tae: Actual clutch engagement time (acceleration time) [s]

Total braking time

$$t_{tb} = t_{id} + t_a + t_{ab} [s]$$
(23)

tid: Initial delay time [s]

ta: Armature pull-in time [s]

 t_{ab} : Actual braking time (deceleration time) of brake [s]

 t_{ae} and t_{ab} are found using the following equations based on operating conditions.

• When accelerating/decelerating Actual engagement time is:

$$t_{ae} = \frac{J \cdot n_r}{9.55(T_d - T_\ell)} [s] \cdot \cdots (24)$$

Actual braking time is:

• During forward/reverse rotation

The actual engagement time (acceleration time) when switching from forward to reverse with a clutch is:

$$t_{ae} = \frac{J}{9.55} \left(\frac{n^1}{T_d - T_\ell} + \frac{n^2}{T_d + T_\ell} \right) [s] \cdot \cdots \cdot (26)$$

n₁: Forward rotation speed [min⁻¹]

n₂: Reverse rotation speed [min⁻¹]

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BRAKE MOTORS

POWER SUPPLIES

■ Engaging/braking time when engaging/braking is completed during the torque rise process

In this case, it is the sum of the armature pull-in time ta and tae' or ta

• Total engagement time

$$\mathbf{t}_{te} = \mathbf{t}_{id} + \mathbf{t}_{a} + \mathbf{t}_{ae}' [s] \qquad (27)$$

$$t_{ae}' = \sqrt{\frac{J \cdot n_r}{4.77} \cdot \frac{t_{ap}}{0.8 \cdot T_d}} \ [s] \ \cdots (28)$$

· Total braking time

$$t_{tb} = t_{id} + t_a + t_{ab}' [s]$$
(29)

$$t_{ab}' = \sqrt{\frac{J \cdot n_r}{4.77} \cdot \frac{t_{ap}}{0.8 \cdot T_d}} \quad [s] \quad \cdots \qquad (30)$$

These are when $T\ell = 0$. Generally, the above equation is used only when load torque (T ℓ) is very small. When, for calculated values, $t_{ae}{}^{\prime} >$ t_{ap} and $t_{ab}' > t_{ap}$, use equations (22) to (26).

Consideration of Number of Operations

The amount of work that a clutch or brake can do before the air gap is adjusted is predetermined. When used beyond that point, the air gap must be adjusted. The number of operations that can be done before air gap adjustment is:

· For a clutch

$$L_e = \frac{E_T}{F_e}$$
 [operations](31)

ET: Total work performed until readjustment of the air gap

For brakes

$$L_b = \frac{E_T}{F_b}$$
 [operations] ······(32)

Consideration of Stopping Precision

Finding stopping precision by calculating is very difficult, since friction energy, control system fluctuations and the like are involved. Generally, it is found empirically with the following equation, and that is then used as a guide.

 \blacksquare Stopping angle (θ)

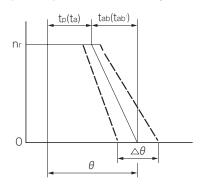
$$\theta = 6n_r(t_{id} + t_p + \frac{1}{2} t_{ab}) [^{\circ}]$$

$$Or, \theta = 6n_r(t_{id} + t_a + \frac{2}{3} t_{ab}') [^{\circ}]$$
(33)

■ Stopping precision ($\triangle \theta$)

$$\triangle \theta = \pm 0.15 \ \theta \ [^{\circ}]$$
 (35)

When there are factors that disrupt braking such as load fluctuation, use a value between 0.2 and 0.25 as the constant in Eq. (35) for safety reasons. Note that the stopping angle and stopping precision do not include divergences due to control system delays, or backlash from chains, gears, or the like.



■ Total Work Performed Until Readjustment of the Air Gap ET Electromagnetic Micro Clutches & Micro Brakes 102/112 Models

Size	Total work E⊤[J]				
02	2 × 10 ⁶				
03	3 × 10 ⁶				
04	6×10^6				
05	9 × 10 ⁶				

CYT Models

Size	Total work E _T [J]			
025	1 × 10 ⁶			
03	1.5×10^{6}			
04	2 × 10 ⁶			

Electromagnetic Clutch/Brake (Units) 101/CS/111 Models

Size	Total work E⊤[J]
06	36 × 10 ⁶
08	60 × 10 ⁶
10	130×10^{6}
12	250×10^{6}
16	470×10^{6}
20	10 × 10 ⁸
25	20 × 10 ⁸

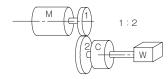
^{*} Also applies to all unit models (except models 180)

CSZ and BSZ Models

Size	Total work ET[J]
05	9×10^6
06	29 × 10 ⁶
00	60 × 106

Selection Example 1

Clutches used for intermittent transport of loads



Selection of a clutch to use to intermittently transport loads as follows, as the figure illustrates.

Usage conditions

Output of motor used	Р	0.4 kW (standard 3-phase, 4P)
Clutch operation frequency	S	20 [RPM]
Moment of inertia of load	JA	0.0208 [kg·m²]
Load torque	Tℓ	Unknown [N•m]
Clutch mounting shaft rotation speed	n	750 [min ⁻¹]
Transmission rate	η	90%

■ Consideration of Torque

We find the required torque for engagement from the above operating conditions.

First, we find the load torque. Based on Eq. (1), load torque $T\ell$ (assuming the motor was selected correctly) is:

$$T_{\ell} = \frac{9550 \times 0.4}{750} \times 0.9 = 4.58 \, [\text{N-m}]$$

Next, according to Eq. (4), the acceleration torque Ta is:

$$T_a = \frac{0.0208 \times 750}{9.55 \times 0.5} = 3.27 [\text{N} \cdot \text{m}]$$

The acceleration time is given as a condition, but in the above equation is it projected as $t_{ae} = 0.5$ [s] based on the operation frequency

Thus, the required torque (T), according to Eq. (6), is:

$$T = (4.58 + 3.27) \times 2 = 15.7 [N \cdot m]$$

Here, the sign of the load torque $T\ell$ is +. The factor K for load conditions was empirically set at 2 for general use with ordinary loads.

From the above, the clutch is size 10, which is a clutch that has torque (20 N·m) above the required torque of 15.7 [N·m].

■ Consideration of Energy

Having determined the model, we find the total load moment of inertia from the self-inertia J of that type and the load moment of inertia.

With the model as 101-10-13, the moment of inertia J of the rotor is 0.000678 [kq·m²]. Thus, the total moment of inertia $J\tau_{otal}$ ' is:

$$J_{Total}' = 0.0208 + 0.000678 = 0.02148 [kg \cdot m^2]$$

We find the engaging energy E_{e} for a single operation. From Eq. (11)

$$E_e = \frac{0.02148 \times 750^2}{182} \times \frac{20}{(20 - 4.58)} = 86.1 \text{ [J]}$$

Here, the sign of the load torque $T\ell$ is -. This engaging energy E_e is sufficiently below the allowable energy $E_{ea}\,\ell$.

$E_e \ll E_{ea} \, \ell$

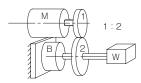
Next, we find the energy rate. From Eq. (18)

$$P_e = \frac{86.1 \times 20}{60} = 28.7 [W]$$

This value is sufficiently below the allowable energy rate $P_{ea}\ell$. Thus, this clutch is suited to the operating conditions, and model 101-10-13 is selected.

Selection Example 2

Brakes that stop momentum when motor goes off



Selection of a brake to stop the momentum of a load when a motor is turned off as follows, as the figure illustrates.

Usage conditions

_		
Output of motor used	Р	0.75kW (standard 3-phase, 4P)
Motor rotation speed	n ₁	1800 [min ⁻¹]
Moment of inertia of motor	Jм	0.00205 [kg·m ²]
Moment of inertia of V pulley (motor side)	J_1	0.00075 [kg·m²]
Moment of inertia of V pulley (brake side)	J_2	0.00243 [kg·m ²]
Moment of inertia of load	JA	0.05 [kg·m²]
Load torque	Tℓ	5.0 [N·m]
Brake mounting shaft rotation speed	n	900 [min ⁻¹]
Stopping time	t	Within 0.5 [s]

■ Consideration of Torque

From the above operating conditions, find the total moment of inertia translated to the brake shaft.

$$J_{Total} = \left(\frac{1800}{900}\right)^{2} \times (0.00205 + 0.00075) + 0.00243 + 0.05 = 0.06363 \text{ [kg·m}^{2}]$$

We find the deceleration torque. The deceleration time also includes the operating time of the brake itself, so calculate it as 1/2 of the given stopping time. From Eq. (5)

$$T_a = \frac{0.06363 \times 900}{9.55 \times 0.25} = 24.0 \, [\text{N} \cdot \text{m}]$$

The required torque from Eq. (6) is:

$T = (24.0 - 5.0) \times 2.4 = 45.6 [N \cdot m]$

Here, the sign of the load torque T_ℓ is -. The factor K for load conditions was empirically set at 2.4 for general use with ordinary loads. From the above, size 12, which has brake torque (40 N·m) equivalent to the required torque of 45.6 [N·m], was provisionally selected

■ Consideration of Energy

Having determined the model, we find the total load moment of inertia from the self-inertia J of that type and the load moment of inertia.

With the model as 111-12-11, the moment of inertia J of the armature is 0.00181 [kg·m²]. Thus, the total moment of inertia JTotal' is:

$$J_{Total}' = 0.06363 + 0.00181 = 0.06544 [kg \cdot m^2]$$

Find the braking energy Eb for a single operation. From Eq. (12)

$$E_b = \frac{0.06544 \times 900^2}{182} \times \frac{40}{(40 + 5)} = 258.9 [J]$$

Here, the sign of the load torque $T\ell$ is +. This braking energy E_b is sufficiently below the allowable energy $E_{bea}\ell$.

 $E_b \ll E_{ba\,\ell}$

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UNITS

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BRAKE MOTORS

POWER SUPPLIES

■ Consideration of Operating Time

We find the braking time. From Eq. (25)

$$t_{ab} = \frac{0.06544 \times 900}{9.55 \times (40 + 5)} = 0.137 [s]$$

Here, the sign of the load torque $T\ell$ is +.

From the specifications table, the armature pull-in time $t_{\mbox{\scriptsize a}}$ for size 12 is 0.027 [s]. If the initial delay time tid of relays and the like is 0.050 [s],

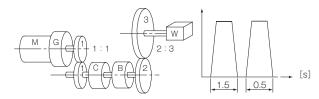
$$t_{tb} = 0.050 + 0.027 + 0.137 = 0.214 [s]$$

from Eq. (23):

This value satisfies the requirement of being at or below 0.5 [s]. Thus, this brake is suited to the operating conditions, and model 111-12-11 is selected.

Selection Example 3

Clutches and brakes that drive loads



Selection of a clutch and brake to drive the load as follows, as the figure illustrates

Usage conditions

Operation frequency	s	30 [RPM]
Required service life operations *1	L	810×10^4 (operations) or more
Moment of inertia of V pulley A	J ₁	0.00195 [kg·m²]
Moment of inertia of V pulley B	J_2	0.01668 [kg·m²]
Moment of inertia of load	JA	0.5075 [kg·m²]
Load torque	Tℓ	22.0 [N•m]
Clutch/brake mounting shaft rotation speed	n	150 [min ⁻¹]
Load shaft rotation speed	n ₂	100 [min ⁻¹]
Engagement time	t ₁	Within 0.3 [s]
Stopping time	t ₂	Within 0.3 [s]

^{*1:} Desired use is 15 hours per day without adjustment for at least 1 year $L = 30 \times 60 \text{ min} \times 15 \text{ hr} \times 300 \text{ days} = 8.1 \text{ million operations}$

Consideration of Torque

From the above operating conditions, load torque is translated to the clutch/brake shaft. From Eq. (10)

$$T_{\ell} = 22.0 \times \frac{2}{3} = 14.7 [\text{N-m}]$$

All of the moment of inertia of the rotating parts is translated to the clutch/brake shaft.

$$J_{Total} = J_{11} + (J_2 + J_A) \times \left(\frac{2}{3}\right)^2$$
$$= 0.00195 + (0.01668 + 0.5075) \times \left(\frac{2}{3}\right)^2$$

$$= 0.2349 [kg \cdot m^2]$$

The acceleration time also includes the operating time of the clutch/ brake itself, so calculate it as 1/2 of the given engagement time of 0.3 [s]. From Eq. (4):

$$T_a = \frac{0.2349 \times 150}{9.55 \times 0.15} = 24.6 \text{ [N-m]}$$

The required torque T from Eq. (6) is:

$$T = (24.5 \pm 14.7) \times K [N \cdot m]$$

If the factor K for load conditions is empirically set at 2 for general use with ordinary loads, for the clutch we get:

$$T = (24.5 + 14.7) \times 2 = 78.4 [N \cdot m]$$

And for the brake, we get:

$$T = (24.5 - 14.7) \times 2 = 19.6 [N \cdot m]$$

Based on the above, we select a size 16 clutch (torque 80N•m) and size 10 brake (torque 20N·m).

■ Consideration of Energy

Next, having determined the model, we find the total load moment of inertia from the self-inertia J of that type and the load moment of

If the clutch model is 101-16-15, the moment of inertia of the rotor is 0.0063 [kg·m²]; if the brake model is 111-10-11, the moment of inertia of the armature is 0.000663 [kg·m²].

Thus, the total moment of inertia JTotal' is:

$$J_{Total'} = 0.2349 + 0.0063 + 0.000663$$

= 0.2419 [kg·m²]

We find the engaging energy of the clutch Ee for a single operation. From Eq. (11)

$$E_e = \frac{0.2419 \times 150^2}{182} \times \frac{80}{(80 - 14.7)} = 36.6 [J]$$

We find the braking energy E_b of the brake for a single operation. From Eq. (12)

E b =
$$\frac{0.2419 \times 150^2}{182} \times \frac{20}{(20 + 14.7)} = 17.2 [J]$$

This value satisfies the allowable energy and the energy per minute of the selected model.

■ Consideration of Number of Operations

Next, we find the number of operations. From the specifications tables for the different models, the total energy of sizes 16 and 10 is, respectively, 470 \times 106 [J] and 130 \times 106 [J], so from Eqs. (31) and (32), for the clutch we get:

$$L = \frac{470 \times 10^6}{36.6} = 1284 \times 10^4 \text{ [times]}$$

And for the brake, we get:

$$L = \frac{130 \times 10^6}{17.2} = 756 \times 10^4 \text{ [times]}$$

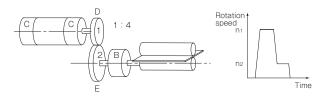
Since the requirement for number of operations in service life is roughly 8.1 million, a size 10 brake cannot satisfy the requirements. When we therefore consider the situation again with a 111-12-11 model brake, we find (leaving out intermediate calculations):

$$L = \frac{250 \times 10^6}{22.0} = 1136 \times 10^4 \text{ [times]}$$

This satisfies the requirements. Thus, we select a 101-16-15 model clutch and a 111-12-11 model brake.

Selection Example 4

Clutches and brakes used in two-step speed change/stopping mechanisms



As the figure illustrates, a selection that includes the stopping precision of the clutch and brake that drive the load is as follows.

Usage conditions

Max. input rotation speed	n ₁	1500 [min ⁻¹]
Min. input rotation speed	n ₂	200 [min ⁻¹]
Roll shaft rotation speed	n ₃	50 [min ⁻¹]
Operation frequency	S	12 [RPM]
Required service life operations *1	L	130×10^4 (operations) or more
Moment of inertia of pulley D	J_1	0.000025 [kg·m²]
Moment of inertia of pulley E	J_2	0.005375 [kg·m²]
Moment of inertia of roll	JA	0.0133 [kg·m²]
Load torque of roll	Tℓ	8.0 [N•m]
Roll diameter	R	60 [mm]

* 1: Desired use is 6 hours per day without adjustment for at least 1 year L = 12×60 min \times 6 hr \times 300 days = 1.3 million operations

■ Consideration of Brake

Consideration of energy

From the above operating conditions, we find the total moment of inertia translated to the feed roll shaft. If the moment of inertia of the rotating parts of clutch/brake unit model 121-08-10 is 0.000475 [kg•m²] and the moment of inertia of the armature of brake model 111-12-12 is 0.00181 [kg•m²],

$$J_{Total} = 0.0133 \times 2 + 0.00181 + 0.005375$$

$$+ (0.000025 + 0.000475) \times \left(\frac{4}{1}\right)^{2}$$

$$= 0.04179 \text{ [kg·m}^{2}\text{]}$$

Find the braking energy Eb for a single operation. From Eq. (12):

$$E_b = \frac{0.04179 \times 50^2}{182} \times \frac{40}{(40 + 8)} = 0.48 [J]$$

Here, the sign of the load torque $T\ell$ is +. This value satisfies the allowable energy and the energy per minute of the selected model.

• Consideration of number of operations Next, we find the number of operations. The total energy of size 12 is 250×10^6 [J], so from Eq. (32):

$$L = \frac{250 \times 10^6}{0.48} = 52083 \times 104 \text{ [times]}$$

This value adequately satisfies the requirements.

■ Consideration of Operating Time

We find the braking time.

We can use either Eq. (25) or Eq. (30), but we use Eq. (30) because the braking time is then shorter. Here, the torque increase time t_{ap} of the brake is 0.063 [s], so from Eq. (30), braking time $t_{ab'}$ is:

$$t_{ab}' = \sqrt{\frac{0.04179 \times 50}{4.77} \times \frac{0.063}{(0.8 \times 40)}}$$

= 0.0294 [S]

• Consideration of stopping precision

If the initial delay time t_{id} of relays and the like is 0.050 [s], from Eq. (34), the stopping angle is:

$$\theta = 6 \times 50 \times \left(0.050 + 0.027 + \frac{2}{3} \times 0.0294\right)$$

= 28.98 [°]

From Eq. (35), the stopping precision is:

$$\triangle \theta = \pm 0.15 \times 28.98 = \pm 4.35$$
 [°]

Converting from roll diameter to length on the circumference, we get \pm 2.3 [mm].

■ Consideration of Clutch

• Consideration of energy

From the above operating conditions, we find the total moment of inertia translated to the clutch shaft.

$$J_{Total'} = 0.000475 + 0.000025 +$$

$$(0.00181 + 0.0133 \times 2 + 0.005375 \times \left(\frac{1}{4}\right)^{2}$$

$$= 0.0026 \text{ [kg·m}^{2}\text{]}$$

Load torque translates to the clutch shaft using Eq. (10).

$$T_{\ell} = 8.0 \times \frac{1}{4} = 2.0 [\text{N} \cdot \text{m}]$$

Calculating for the clutch on the high-speed side, the engaging energy $E_{\rm e}$ for one operation, from Eq. (11), is:

$$E_e = \frac{0.0026 \times 1500^2}{182} \times \frac{10}{(10-2)} = 40.2 [J]$$

This value satisfies the allowable energy of the selected model. Next, we find the engaging energy rate P_e . From Eq. (18):

$$P_e = \frac{40.2 \times 12}{60} = 8.04 \, [W]$$

This value is sufficiently small for the allowable energy rate $P_{ea} \ell$.

Consideration of number of operations
 We find the number of operations. From Eq. (31):

$$L = \frac{60 \times 10^6}{40.2} = 149 \times 10^4 \text{ [times]}$$

Since the number of operations over one year is roughly 1.3 million, this meets the requirement.

Next, calculating for the clutch on the low-speed side, the engaging energy $E_{\rm e}$ for one operation, from Eq. (12), is:

$$E_e = \frac{0.0026 \times (1500 - 200)^2}{182} \times \frac{10}{(10 + 2)}$$
= 20.1 [J]

This clutch decelerates the load from 1500 (min $^{-1}$) to 200 (min $^{-1}$), so it does similar work to the brake. Thus, the sign of the load torque T ℓ is +. Also, since this value is smaller than the value for the clutch on the high-speed side, it clearly satisfies the requirement for number of operations during the service life.

The above shows that both clutch and brake satisfy conditions.

COUPLINGS

ETP BUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

LINEAR SHAFT DRIVE

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POST/

SERIES

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CLUTCH & BRAKE
UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

Accessories

Different models and types of clutches and brakes have different accessories. Consult these tables. Note that we may change accessories as circumstances dictate.

Micro Sizes

Maralal.	Varistor		Screw type		Disc spring washer		g washer Shim [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.
102-02- \square 1/ \square 5	NVD07SCD082 or an equivalent	1	_	-	-	-	_	_
112-02- 🗆 1/ 🗆 2	NVD07SCD082 or an equivalent	1	-	-	-	_	_	-
102/112-02- 🗌 3	NVD07SCD082 or an equivalent	1	M2 × 3	2	_	_	_	_
CYT-025-33B ø 6	NVD07SCD082 or an equivalent	1	M2.5 × 4	3	-	-	6.3 × 8.7 × 0.1t	3

Model	Varistor		Screw type Disc spring washer		Shim [mm]			
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.
102-03- \square 1/ \square 5	NVD07SCD082 or an equivalent	1	_	_	-	_	_	-
112-03- 🗆 1/ 🗆 2	NVD07SCD082 or an equivalent	1	-	-	-	-	_	-
102/112-03- 🗆 3	NVD07SCD082 or an equivalent	1	$M2.5 \times 4$	3	-	_	_	_
CYT-03-33 □ φ 6	NVD07SCD082 or an equivalent	1	M2.5 × 4	3	-	-	$6.3 \times 8.7 \times 0.1t$	3
CYT-03-33 □ ф 8	NVD07SCD082 or an equivalent	1	M2.5 × 4	3	_	_	8.3 × 11.7 × 0.1t	3

Madal	Varistor		Screw type		Disc sprin	g washer	Shim [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.
102-04- \square 1/ \square 5	NVD07SCD082 or an equivalent	1	_	_	-	-	_	_
112-04- 🗆 1/ 🗆 2	NVD07SCD082 or an equivalent	1	-	-	-	-	_	-
102/112-04- 🗆 3	NVD07SCD082 or an equivalent	1	M3 × 6	3	_	_	_	_
CYT-04-33 🗆 🏚 8	NVD07SCD082 or an equivalent	1	M3 × 6	3	-	_	8.3 × 11.7 × 0.1t	3
CYT-04-33 🗆 🏚 10	NVD07SCD082 or an equivalent	1	M3 × 6	3	-	_	$10.3 \times 13.7 \times 0.1t$	3

M. J.I	Varistor		Screw type Disc spring washer				Shim [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.
102-05- \square 1/ \square 5	NVD07SCD082 or an equivalent	1	_	-	_	_	-	-
112-05- 🗆 1/ 🗆 2	NVD07SCD082 or an equivalent	1	-	-	_	_	_	-
102/112-05- 🗆 3	NVD07SCD082 or an equivalent	1	M3 × 6	3	M3	3	_	-
CSZ/BSZ-05- □	NVD07SCD082 or an equivalent	1	-	-	-	-	_	-

^{*} Only the screws supplied with 102/112-05- \(\Boxed{1} \) 3 are hex-socket low-head bolts. All others are Phillips pan-head machine screws.

Standard Sizes

Model	Varistor		Low head	bolt	Disc spring v		Shim 1 [mm]				Collar [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.
101/CS-06- 🗆 1	NVD07SCD082 or an equivalent	1	-	_	-	_	_	-	_	_	_	_
101/CS-06- □ 3 ø 12	NVD07SCD082 or an equivalent	1	$M3 \times 6$	3	M3	3	$12.3\times15.7\times0.1t$	3	-	-	-	_
101-06-13 ф 15	NVD07SCD082 or an equivalent	1	$M3 \times 6$	3	M3	3	$15.3\times20.7\times0.1t$	3	_	_	_	_
101/CS-06- □ 5 ¢ 12	NVD07SCD082 or an equivalent	1	-	-	_	-	$12.3\times15.7\times0.1t$	5	$12.3\times15.7\times0.5t$	1	$12.2\times18\times5.5$	1
111-06-11 ¢ 12/ ¢ 15	NVD07SCD082 or an equivalent	1	-	-	_	-	_	-	_	-	_	_
111-06-12 ф 12	NVD07SCD082 or an equivalent	1	-	-	-	-	$12.3\times15.7\times0.1t$	3	-	-	-	_
111-06-12 ф 15	NVD07SCD082 or an equivalent	1	-	_	_	_	$15.3\times20.7\times0.1t$	3	_	-	_	_
111-06-13	NVD07SCD082 or an equivalent	1	-	-	_	-	_	-	-	-	-	_
CSZ/BSZ-06- □	NVD07SCD082 or an equivalent	1	$M3 \times 6$	3	M3	3	-	_	_	_	_	_

Model	Varistor		Low head	bolt	Disc spring v	vasher	Shim 1 [mm]		Shim 2 [mm]		Collar [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.
101/CS-08- 🗆 1	NVD07SCD082 or an equivalent	1	-	_	_	-	_	_	_	-	_	-
101/CS-08- □ 3 ¢ 15	NVD07SCD082 or an equivalent	1	$M4 \times 8$	3	M4	3	$15.3\times20.7\times0.1t$	3	_	-	_	-
101-08-13 ф 20	NVD07SCD082 or an equivalent	1	$M4 \times 8$	3	M4	3	$20.3\times27.7\times0.1t$	3	_	_	_	-
101/CS-08- □ 5 ¢ 15	NVD07SCD082 or an equivalent	1	-	-	-	-	$15.3\times20.7\times0.1t$	5	$15.3\times20.7\times0.5t$	1	15.2 × 22 × 5.5	1
111-08-11 ф 15/ ф 20	NVD07SCD082 or an equivalent	1	-	-	_	-	$15.3\times20.7\times0.5t$	1	_	-	_	_
111-08-12 ф 15	NVD07SCD082 or an equivalent	1	-	-	_	-	_	-	_	-	_	-
111-08-12 ф 20	NVD07SCD082 or an equivalent	1	-	_	_	-	$15.3\times20.7\times0.1t$	3	_	_	_	-
111-08-13	NVD07SCD082 or an equivalent	1	$M4 \times 8$	3	M4	3	$20.3\times27.7\times0.1t$	3	-	-	-	-
CSZ/BSZ-08- □	NVD07SCD082 or an equivalent	1	_	_	_	_	_	_	_	_	_	_

Standard Sizes

Model	Varistor		Low head	bolt	Disc spring						Collar [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.
101/CS-10- 🗆 1	NVD07SCD082 or an equivalent	1	-	-	-	-	_	-	_	-	-	-
101/CS-10- □ 3 ¢ 20	NVD07SCD082 or an equivalent	1	$M5 \times 10$	3	M5	3	$20.3\times27.7\times0.1t$	3	_	-	_	-
101-10-13 ф 25	NVD07SCD082 or an equivalent	1	$M5 \times 10$	3	M5	3	$25.3\times34.7\times0.1t$	3	_	-	_	-
101/CS-10- ☐ 5 ¢ 20	NVD07SCD082 or an equivalent	1	-	-	-	-	$20.3\times27.7\times0.1t$	5	$20.3\times27.7\times0.5t$	2	$20.2\times28\times5.9$	1
111-10-11 ф 20/ ф 25	NVD07SCD082 or an equivalent	1	-	-	-	-	-	-	-	-	-	-
111-10-12 ф 20	NVD07SCD082 or an equivalent	1	-	-	-	_	$20.3\times27.7\times0.1t$	3	-	-	_	_
111-10-12 ф 25	NVD07SCD082 or an equivalent	1	_	_	_	_	$25.3\times34.7\times0.1t$	3	_	-	_	_
111-10-13	NVD07SCD082 or an equivalent	1	$M5 \times 10$	3	M5	3	-	-	-	-	-	-

Model	Varistor		Low head	bolt	Disc spring	washer	Shim 1 [mm]		Shim 2 [mm]		Collar [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.
101/CS-12- 🗌 1	NVD07SCD082 or an equivalent	1	-	_	-	_	_	-	_	_	_	-
101-12-13 ф 25	NVD07SCD082 or an equivalent	1	$M6 \times 10$	3	M6	3	$25.3\times34.7\times0.1t$	3	_	_	_	-
101-12-13 ф 30	NVD07SCD082 or an equivalent	1	M6 × 10	3	M6	3	$30.3 \times 39.7 \times 0.1t$	3	_	-	_	-
CS-12-33 ф 25	NVD07SCD082 or an equivalent	1	$M6 \times 10$	3	M6	3	$25.3\times31.7\times0.1t$	3	-	-	-	-
101/CS-12- ☐ 5 ¢ 25	NVD07SCD082 or an equivalent	1	_	_	_	_	$25.3\times31.7\times0.1t$	5	$25.3\times31.7\times0.5t$	2	$25.2\times32\times7.5$	1
111-12-11 \$\phi\$ 25/ \$\phi\$ 30	NVD07SCD082 or an equivalent	1	-	-	-	_	_	-	-	-	_	-
111-12-12 ф 25	NVD07SCD082 or an equivalent	1	_	-	_	_	$25.3\times31.7\times0.1t$	3	_	-	_	-
111-12-12 ф 30	NVD07SCD082 or an equivalent	1	-	-	-	_	$30.3\times39.7\times0.1t$	3	_	-	_	-
111-12-13	NVD07SCD082 or an equivalent	1	M6 × 10	3	M6	3	_	-	_	-	_	_

Model	Varistor		Low head	bolt	Disc spring	washer	Shim 1 [mm]			Shim 2 [mm]		
Wodei	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.
101/CS-16- ☐ 1	NVD07SCD082 or an equivalent	1	-	-	-	-	_	-	_	-	_	-
101-16-13 ф 30	NVD07SCD082 or an equivalent	1	M8 × 15	3	M8	3	$30.3\times41.7\times0.1t$	3	-	-	-	-
101-16-13 ф 40	NVD07SCD082 or an equivalent	1	$M8 \times 15$	3	M8	3	$40.3\times51.7\times0.1t$	3	-	-	_	-
CS-16-33 ø 30	NVD07SCD082 or an equivalent	1	$M8 \times 15$	3	M8	3	$30.3\times39.7\times0.1t$	3	-	-	-	-
101/CS-16- ☐ 5 ф 30	NVD07SCD082 or an equivalent	1	-	-	-	_	$30.3\times39.7\times0.1t$	5	$30.3\times39.7\times0.5t$	2	$30.2\times40\times11.2$	1
111-16-11 \$\phi\$ 30/ \$\phi\$ 40	NVD07SCD082 or an equivalent	1	-	-	-	-	-	-	-	-	-	-
111-16-12 ф 30	NVD07SCD082 or an equivalent	1	-	-	-	_	$30.3\times39.7\times0.1t$	3	-	-	_	-
111-16-12 ф 40	NVD07SCD082 or an equivalent	1	-	-	-	_	$40.3\times51.7\times0.1t$	3	-	-	-	-
111-16-13	NVD07SCD082 or an equivalent	1	$M8 \times 15$	3	M8	3	-	-	-	-	_	-

Madal	Varistor		Low head b		olt Disc spring washer				Shim 2 [mm]		Collar [mm]	
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.
101-20-11	NVD07SCD082 or an equivalent	1	_	_	_	_	_	-	_	-	_	-
101-20-13 ф 40	NVD07SCD082 or an equivalent	1	$M10 \times 18$	3	M10	3	$40.3\times51.7\times0.1t$	3	-	-	_	-
101-20-13 ф 50	NVD07SCD082 or an equivalent	1	$\rm M10\times18$	3	M10	3	$50.3\times67.7\times0.1t$	3	_	-	_	_
CS-20-33 ф 40	NVD07SCD082 or an equivalent	1	$M10 \times 18$	3	M10	3	$40.3\times51.7\times0.1t$	5	-	-	_	-
101-20-15 ф 40	NVD07SCD082 or an equivalent	1	-	-	-	_	$40.3\times51.7\times0.1t$	5	$40.3\times51.7\times0.5t$	2	40.2 × 50 × 11.7	1
111-20-11 \$\phi\$ 40/ \$\phi\$ 50	NVD07SCD082 or an equivalent	1	-	-	-	_	-	-	-	-	-	-
111-20-12 ф 40	NVD07SCD082 or an equivalent	1	-	-	_	-	$40.3\times51.7\times0.1t$	3	_	-	_	-
111-20-12 ø 50	NVD07SCD082 or an equivalent	1	-	-	-	-	$50.3\times67.7\times0.1t$	3	-	-	-	-
111-20-13	NVD07SCD082 or an equivalent	1	M10 × 18	3	M10	3	_	_	_	_	_	_

Model	Varistor		Low head	bolt	Disc spring	washer	Shim 1 [mm]	Shim 1 [mm]		Shim 2 [mm]		
Model	Model	Qty.	Standards	Qty.	Standards	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.	Internal dia. × External dia. × Thickness	Qty.
101-25-11	NVD07SCD082 or an equivalent	1	-	-	-	-	_	-	_	-	_	-
101-25-13 ф 50	NVD07SCD082 or an equivalent	1	M12 × 22	4	M12	4	$50.3\times67.7\times0.1t$	3	-	-	-	-
101-25-13 ф 60	NVD07SCD082 or an equivalent	1	$\rm M12 \times 22$	4	M12	4	$60.3\times84.7\times0.1t$	3	_	-	_	-
CS-25-33 ø 50	NVD07SCD082 or an equivalent	1	M12 × 22	4	M12	4	$50.3\times67.7\times0.1t$	5	-	-	-	-
101-25-15 ф 50	NVD07SCD082 or an equivalent	1	_	-	_	-	$50.3\times67.7\times0.1t$	5	$50.3\times67.7\times0.5t$	2	$50.2\times60\times12.2$	1
111-25-11 \$\phi\$ 50/ \$\phi\$ 60	NVD07SCD082 or an equivalent	1	-	-	-	-	-	-	-	-	-	-
111-25-12 ф 50	NVD07SCD082 or an equivalent	1	_	-	_	-	$50.3\times67.7\times0.1t$	3	_	-	_	-
111-25-12 ф 60	NVD07SCD082 or an equivalent	1	-	-	-	-	$60.3\times84.7\times0.1t$	3	-	-	-	-
111-25-13	NVD07SCD082 or an equivalent	1	$M12 \times 22$	4	M12	4	-	-	_	-	-	-

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SPEED CHANGERS & REDUCERS

SERIES

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UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

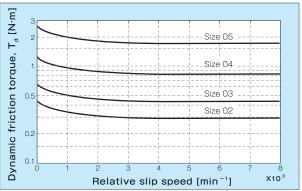
POWER SUPPLIES

Torque Characteristics

Static and Dynamic Friction Torque Characteristics

Clutches and brakes transmit torque as they slip at certain relative speeds in the engaging/braking process. Then, the relative speed gradually decreases until the clutch is fully engaged. The torque that can be transmitted when this engaging/braking is complete is called the dynamic friction torque at that relative speed.

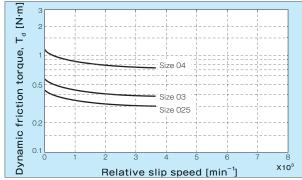
Static friction torque is a nearly predetermined value, while dynamic friction torque varies somewhat with relative speed.



Dynamic friction torque characteristics (micro size models 102 and 112)

Dynamic Friction Torque Characteristics

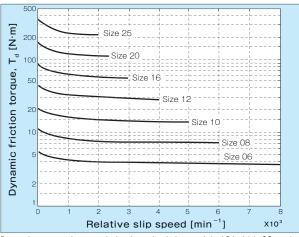
The figure at right shows the relationship between relative slip speed and dynamic friction torque. As the figure shows, the difference between static friction torque and dynamic friction torque is small, so the effects in actual use are diminished. Note that the specifications present the values when the relative slip speed is 100 min⁻¹.



Dynamic friction torque characteristics (micro size CYT models)

Initial Torque Characteristics

The frictional surfaces of clutches and brakes that use friction will not be fully broken during initial use, so they may not always reach rated torque. This is referred to as the initial torque state. The initial torque value will be 60 to 70% of indicated torque; after a little breaking in, the indicated value will be reached. Check these values if you require the indicated torque right from the initial use. Breaking in may take longer when the equipment is used with light loads or at low speeds. Residual torque (torque remaining after current is shut off) also exists. Due to the action of the disc spring, residual torque persists for a very short time, so special circuits for reverse excitation or the like are not necessary in normal use.



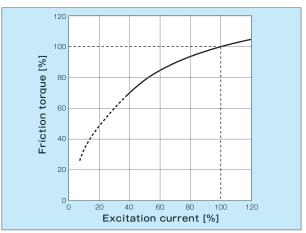
Dynamic torque characteristics (standard size models 101, 111, CS etc.)

Torque-Current Characteristics

The size of the friction torque, when the friction coefficient is μ , the average radius of the frictional surface is r, and the pull-in force is P, is given by:

$T = \mu \times r \times P$

Here, μ and r are predetermined, but pull-in force P varies with the size of the current supplied. Since current is proportional to voltage, friction torque changes when the voltage applied to the coil changes. The figure at right shows the relationship between friction torque and excitation current. Near the rated current value, torque increases and decreases nearly proportionally to current. As current is increased beyond the rated value, magnetic flux in the magnetic circuit reaches saturation. Further increases do not increase torque but merely increase the amount of heat generated. Conversely, as current is decreased, torque decreases. However, as the minimum current required to attract the armature is neared, torque becomes unstable; when decreased further, the armature can no longer be attracted, and torque is extinguished. (To generate torque below the armature pull-in current value, appropriate measures must be taken.) Note that this characteristics chart is at the prescribed air gap; if the air gap value changes, the characteristics curve will also change.



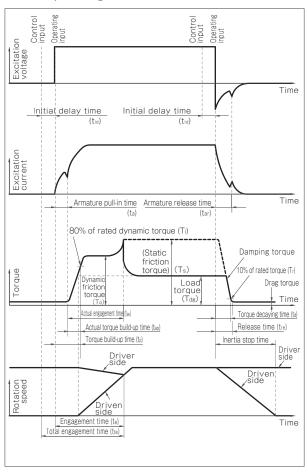
Torque-current characteristics

Operating Characteristics

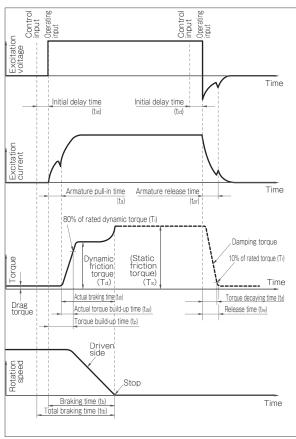
Transient Characteristics When Clutch/ **Brake Are Actuated**

The figure below illustrates transient phenomena of current and torque when clutches and brakes engage (brake) and release. These are generally called dynamic characteristics. When a voltage is applied to the clutch/brake, current increases according to a time constant determined by the coil. Once current has increased to a certain value, the armature is pulled in and the generation of friction torque begins. Thereafter, as current increases, friction torque also increases to reach the rated value. At the time of release, current decreases in the same way as when engaging (braking), the armature starts its withdrawal with the release action of the disc spring, and torque is extinguished.

Clutch operating characteristics



Brake operating characteristics



ta: Armature pull-in time

(The time from when current flow first starts until the armature is pulled in and torque begins to be generated)

tap: Actual torque build-up time

(The time from when torque first begins to be generated until it reaches 80% of rated torque)

t_p: Torque build-up time

(The time from when current flow first starts until torque reaches 80% of rated torque)

td: Torque decaying time

(The time from when current flow is shut off until torque decreases to 10% of rated torque)

tid: Initial delay time

(The time from the arrival of operational input at the clutch and brake until the actuation input or release input arrives at the clutch or brake body)

tae: Actual engagement time

(The time from when the clutch begins generating torque until engagement is complete)

tab: Actual braking time

(The time from when the brakes begins generating torque until braking is complete)

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES ELECTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES** FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

Operating Characteristics

Control Circuit System and Operation Times

The standard voltage is DC 24 V. If there is no DC power supply, the direct current obtained by stepping down and rectifying (full-wave rectification) the AC power supply is used. (See page on power supplies.) The clutch or brake is normally turned on or off on the DC side. The operation times in that case are shown in the table below. Performing these command operations on the DC side provides fast response, but a very large surge current is generated when the current is shut off. This surge current can burn contacts within the control circuit or damage the coil insulation. For this reason, circuit protectors are used to absorb surges.

When switching is performed on the AC side, the torque decaying time lengthens. When the torque decaying time lengthens, one clutch or brake operation may interfere with the next. Accordingly, a time lag should be designed in. The torque build-up time is the same as when the command operation is performed on the DC side.

The electromagnetic clutch/brake operation times below are values using transformer stepdown/single-phase full-wave rectification.

■ Micro sizes Clutch operation time

Clutch size		Operatin	g time [s]	
Ciutcii size	ta	t ap	t _p	t d
102-02	0.009	0.010	0.019	0.017
102-03	0.009	0.013	0.022	0.020
102-04	0.011	0.017	0.028	0.030
102-05	0.012	0.019	0.031	0.040
CYT-025	0.014	0.014	0.028	0.030
CYT-03	0.015	0.015	0.030	0.040
CYT-04	0.030	0.010	0.040	0.040

Brake operating time

Brake size		Operatin	g time [s]	
DI ake Size	ta	tap	t _p	t d
112-02	0.004	0.006	0.010	0.010
112-03	0.005	0.007	0.012	0.008
112-04	0.007	0.009	0.016	0.010
112-05	0.010	0.013	0.023	0.012

Standard sizes

Clutch operation time

Clutch size		Operatin	g time [s]	
Ciutcii size	ta	tap	t _p	td
101-06	0.020	0.021	0.041	0.020
101-08	0.023	0.028	0.051	0.030
101-10	0.025	0.038	0.063	0.050
101-12	0.040	0.075	0.115	0.065
101-16	0.050	0.110	0.160	0.085
101-20	0.090	0.160	0.250	0.130
101-25	0.115	0.220	0.335	0.210

 $^{^{*}}$ The above values are suitable for CS and CSZ models as well as for the various clutch/brake unit models

Brake operating time

Brake size		Operatin	g time [s]	
DI ake Size	ta	t ap	t _p	td
111-06	0.015	0.018	0.033	0.015
111-08	0.016	0.026	0.042	0.025
111-10	0.018	0.038	0.056	0.030
111-12	0.027	0.063	0.090	0.050
111-16	0.035	0.092	0.127	0.055
111-20	0.065	0.135	0.200	0.070
111-25	0.085	0.190	0.275	0.125

^{*} The above values are suitable for BSZ models as well as for the various clutch/brake unit models

To Shorten the Engagement/Braking Time

Current obeys a predetermined time constant, but when a particularly fast build-up time is required, the operation characteristics can be changed by using an excitation method, such as overexcitation. The overexcitation method applies an overvoltage to the coil to speed up the rise. Operation times in the case of overexcitation are shown in the

For details, refer to the section on power supplies.

Operation times for overexcitation of clutch (using a BEH power supply)

Clutch size		Operatin		
Ciutcii size	ta	tap	t _p	td
101-06	0.008	0.005	0.013	0.005
101-08	0.009	0.008	0.017	0.008
101-10	0.010	0.010	0.020	0.011
101-12	0.013	0.012	0.025	0.018
101-16	0.018	0.016	0.034	0.023
101-20	0.027	0.020	0.047	0.037
101-25	0.045	0.026	0.071	0.045

^{*} The above values are suitable for CS and CSZ models as well as for the various clutch/brake unit models.

Operation times for overexcitation of brake (using a BEH power supply)

Brake size		Operatin		
DI ake Size	ta	tap	t _p	td
111-06	0.005	0.007	0.012	0.004
111-08	0.005	0.007	0.012	0.005
111-10	0.007	0.008	0.015	0.007
111-12	0.009	0.009	0.018	0.007
111-16	0.014	0.010	0.024	0.011
111-20	0.015	0.025	0.040	0.020
111-25	0.021	0.034	0.055	0.038

^{*} The above values are suitable for BSZ models as well as for the various clutch/brake unit models.

- ta Armature pull-in time: The time from when current flow first starts until the armature is pulled in and torque begins to be generated.
- tap Actual torque build-up time: The time from when torque first begins to be generated until it reaches 80% of rated torque.
- Torque build-up time: The time from when current flow first starts until torque reaches 80% of rated torque.
- Torque decaying time: The time from when current flow is shut off until torque decreases to 10% of rated torque.

Limit on Number of Operations

There are some limits for command operations that turn clutches and brakes on and off per unit time. Due to their size, micro sizes are particularly prone to being unable to externally dissipate heat at some energization frequencies, and may malfunction or be damaged. That limit is expressed as an energization rate. For that limit, being energized for 0.5 seconds over a one second period is treated as 50%. Operations must be designed so that the energization rate does not exceed the following rates shown for each model. These limits may not apply, however, if the clutch or brake is effectively cooled.

Models	Energization rate
102 Models	80%
CYT Models	50%
112 Models	80%
101/CS Models	100%
CSZ Models	100%
111 Models	100%
BSZ Models	100%

Furthermore, in the case of overexcitation intended to speed up the build-up by applying overvoltage to the coil, a voltage higher than the normal excitation voltage is applied, so care is required even with standard sizes. Ascertain your operating conditions and the like and then check these issues for your particular situation.

Heat Radiation Characteristics

I Allowable Energy (Eeaℓ or Ebaℓ)

When loads are accelerated or decelerated by a clutch/brake, heat will be generated by sliding friction. This is because frictional energy is converted to heat, so the amount of heat will vary with the conditions of use.

Clutches and brakes dissipate this heat externally as they work, but if they cannot dissipate all the heat, they accumulate it internally and the temperatures of the components rise. If temperatures exceed allowable values, malfunctions and damage result.

The limit for friction work undergone due to this heat is called allowable energy. The allowable energy is predetermined for each size. Heat dissipation is affected by the mounting situation, rotation speed, atmosphere, and the like.

When large loads are accelerated or decelerated, violent slipping occurs, and the frictional surface generates larges amounts of heat. The frictional material and armature can be damaged by even a single engagement.

The table at right shows the allowable energy (allowable friction energy) for each size of micro clutches and micro brakes. Even if frequency is low, use the device at a value that is sufficiently smaller than the table value if you have a single engagement whose amount of energy is high.

Use standard sizes below the limit lines of the figure below.

Allowable energy of micro clutches and micro brakes

Model size	Allowable (engagement/braking) energy $(E_{ea}\ell\ or\ E_{ba}\ell\)\ [J]$
102/112-02	1500
102/112-03	2300
102/112-04	4500
102/112-05	9000
CYT-025	800
CYT-03	900
CYT-04	1900

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BRAKE MOTORS

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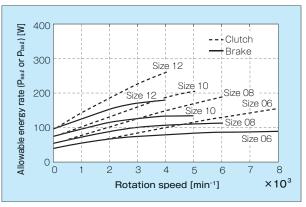
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Heat Radiation Characteristics

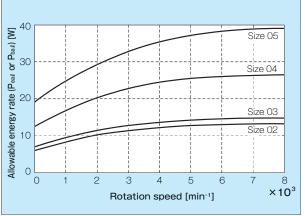
I Allowable Energy Rate (Peaℓ or Pbaℓ)

High frequency of engagement and/or braking must take heat dissipation fully into account. The maximum energy amount per unit time is called the allowable energy rate. It is predetermined for each size as shown in the figure. In actual use, use a value that is sufficiently smaller than the allowable value to allow for changes in conditions and the like.

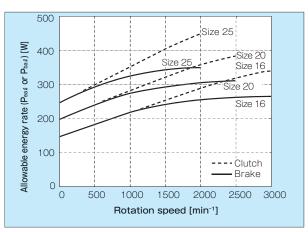
The figure shows values for wall-mounted devices. For devices mounted on shafts such as bearing-mounted models, use 80% of the allowable values in the figures.



Standard sizes



Micro sizes (excludes CYT models)



Standard sizes

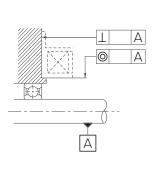
Items Checked for Design Purposes

What is the best way to ensure that the design allows clutches and brakes used in machinery and equipment to perform and function adequately? We describe here approaches to design that we feel are useful in improving machinery reliability.

Mounting Stators and Rotors

■ Flange-mounted stators (models □ - □ -1 □)

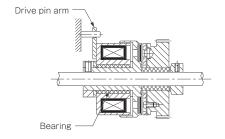
These stators must be correctly positioned with respect to the rotation shaft before mounting. The inner and outer circumferences of the stators have grades for fit. The surface on which the stator is mounted should be positioned relative to the rotation shaft and the allowable values for concentricity and perpendicularity of the diameter should not be exceeded.



		Unit [mm]
Size	Concentricity (T.I.R.)	Perpendicularity (T.I.R.)
02	0.05	0.03
03	0.05	0.04
04	0.06	0.04
05	0.06	0.05
06	0.08	0.05
08	0.08	0.05
10	0.1	0.05
12	0.1	0.07
16	0.12	0.08
20	0.12	0.13
25	0.14	0.13

■ Bearing-mounted stators (models \square - \square -3 \square)

This stator is subject to a slight amount of rotation force from the builtin bearing or the slide bearing. The drive pin arm should therefore be held to the machinery's stationary parts to prevent drag turning.



■ Magnetic shield of stator

Installing clutches and brakes in combination can lead to instability of clutch/brake operation due to their magnetic effects on each other. Also, if there are instruments or machinery in the vicinity of the clutch or brake, adverse effects such as noise or malfunction may result. In such cases, measures to block magnetism are advised. The method generally used is to adopt non-magnetic materials for the surface on

■ Lead wire protection

which the stator is mounted and for the shaft.

Damage to the covering of the leads can cause shorts, breaks or other problems. Keep protection of these coverings in mind from the design

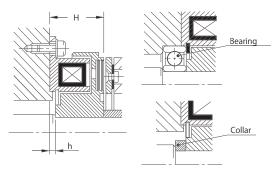
■ Rotor mounting

The rotor is part of the magnetic circuit. Machining other than bore drilling can lower performance, so it should be avoided.

Consult Miki Pulley if you are creating a rotor bore with a non-standard diameter not shown in the dimensions table.

■ Relationship between rotor and stator (models □ - □ -1 □)

In flange-mounted clutches, the positional relationship between rotor and stator is important. If the dimension H in the figure below is too small, the rotor and stator will touch; if H is too large, the pull-in force will decline. The table below lists allowable values for each size. Design your setup so that these values are not exceeded. The allowable value for h should conform to the normal JIS allowable value.



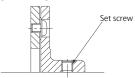
Unit [mm]

Clutch size	H	1	h
Clutch size	Reference value	Tolerance	Reference value
102-02	18.0	± 0.2	1.6
102-03	22.2	± 0.2	2.0
102-04	25.4	± 0.2	2.0
102-05	28.1	± 0.2	2.0
101-06	24.0	± 0.2	2.0
101-08	26.5	± 0.2	2.5
101-10	30.0	± 0.3	3.0
101-12	33.5	± 0.3	3.5
101-16	37.5	± 0.3	3.5
101-20	44.0	± 0.4	4.0
101-25	51.0	± 0.4	4.0

Armature Mounting Methods

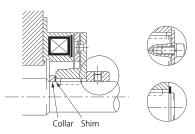
■ Mounting armature type-1

Securely fasten the armature with the provided hex-socket-head set screw. If you are concerned that it might be loosened by vibration or high-frequency operations, apply adhesive to the threads, which is effective in stopping loosening.



■ Mounting armature type-2

Since the boss is hidden on the inside of the stator, secure it firmly using a C-shaped snap ring, collar, or the like, as shown in the figure below.



■ Mounting armature type-5

For size 05 and smaller micro sizes, insert the armature directly onto the shaft. As when assembling armature type-2, firmly press the end face of the armature with a C-shaped snap ring, collar or the like.

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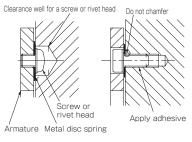
■ Armature type-3 mounting

Machine in the screw bores and clearance well for screw and/or rivet heads in the mounting surface. Mount the armature using the supplied special hex-socket-head bolts and disc spring washers, applying a small amount of adhesive to the threads to prevent loosening. (Note that any excess adhesive will seep into the disc spring, impeding operation.)

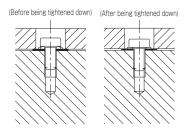
The mounting screw bores should not be beveled; simply removing burr is sufficient. The hex-socket-head bolts supplied are special lowhead bolts. For sizes 04 and smaller, Phillips-head round head screws that meet JIS standards are supplied. Use disc spring washers like that depicted in the figure below. Their fastening effect is diminished if used facing backwards.

Assemble armature type-3 correctly so that the concentricity and perpendicularity relative to the rotation shaft do not exceed the

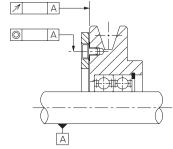
		Offic [illing
Size	Concentricity (T.I.R.)	Perpendicularity (T.I.R.)
02	0.1	0.02
03	0.1	0.03
04	0.1	0.04
05	0.1	0.04
06	0.16	0.04
08	0.16	0.05
10	0.16	0.05
12	0.16	0.06
16	0.16	0.07
20	0.24	0.11
25	0.24	0.11



Armature type-3 mounting

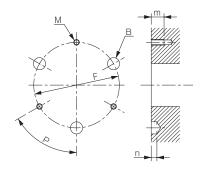


How to use washers



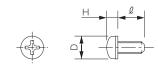
Mounting precision

Armature type-3 mounting dimensions

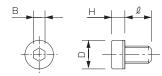


Clutch/	Mounting pi	tch diameter	Mountii	ng angle	Mou	ınting screw	Clearance well for screw/rivet head		
brake size	F (P.C.D.)	Tolerance	P [°]	Tolerance [']	No. of bores-M (nominal)	Pitch	Effective thread depth m (MIN)	No. of bores- Bore diameter B	Spot facing depth n (MIN)
02	19.5	± 0.05	90	± 5	2-M2	0.4	4	2-5	2.5
03	23	± 0.05	60	± 5	3-M2.5	0.45	5	3-6	3
04	30	± 0.05	60	± 5	3-M3	0.5	7	3-6	3.5
05	38	± 0.05	60	± 5	3-M3	0.5	7	3-7	3.5
06	46	± 0.05	60	± 5	3-M3	0.5	7	3-7	3.5
08	60	± 0.05	60	± 5	3-M4	0.7	9	3-8.5	3.5
10	76	± 0.05	60	± 5	3-M5	0.8	11	3-10.5	4
12	95	± 0.05	60	± 5	3-M6	1.0	11	3-12.5	4
16	120	± 0.05	60	±5	3-M8	1.25	16	3-15.5	4.5
20	158	± 0.05	60	± 5	3-M10	1.5	18	3-19	5.5
25	210	± 0.1	45	± 5	4-M12	1.75	22	4-22	6

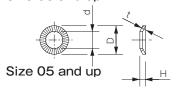
Armature type-3 mounting components



Size 02 to 04



Size 05 and up



Clutch/	Special hex-socket-l	nead bolt (*	Phillips-he	ead screw)	Disc spring washer				
brake size	${\sf Nominal} \times {\sf pitch}$	φ D	Н	В	l	φ D	φ d	Н	t
02	$*$ M2 \times 0.4	3.5	1.3	_	3	_	-	-	_
03	* $M2.5 \times 0.45$	4.5	1.7	_	4	_	_	-	_
04	* $M3 \times 0.5$	5.5	2.0	_	6	_	-	-	_
05	$M3 \times 0.5$	5.5	2.0	2.0	6	6	3.2	0.55	0.36
06	$M3 \times 0.5$	5.5	2.0	2.0	6	6	3.2	0.55	0.36
08	$M4 \times 0.7$	7	2.8	2.5	8	7	4.25	0.7	0.5
10	$M5 \times 0.8$	8.5	3.5	3.0	10	8.5	5.25	0.85	0.6
12	M6 × 1.0	10	4.0	4.0	10	10	6.4	1.0	0.7
16	$M8 \times 1.25$	13	5.0	5.0	15	13	8.4	1.2	0.8
20	M10 × 1.5	16	6.0	6.0	18	16	10.6	1.9	1.5
25	$M12 \times 1.75$	18	7.0	8.0	22	18	12.6	2.2	1.8

^{*} Sizes 02, 03, and 04 do not use disc spring washers.

Air Gap Design and Adjustment

Set the air gap "a" (below figure) between the frictional surfaces so that when released the gap becomes the control value. Handling will be easier if the device is designed to facilitate this adjustment.

We recommend designs with both collars and shims as shown below to accomplish this. (We always have shims available; please contact Miki Pulley for details.)

■ Setting air gap "a"

Prepare a collar that is slightly shorter than the length $\,\ell\,$ needed to maintain air gap "a", and then adjust the remaining gap with shims to achieve the control value for "a". The collar length at this time is roughly the value given by the following equation.

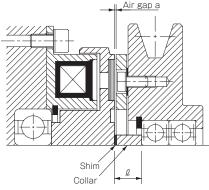
$L = \ell - 2a [mm]$

Here, L: Collar length.

- ℓ : Length required to maintain air gap "a"
- a: Control air gap value

Based on the value of L found with this equation, prepare a collar of a length that is easy to machine. Using a design like this that employs shims will enable you to adjust the air gap after long periods of use by simply removing the necessary number of shims.

Air gap setting



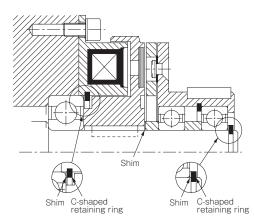
* Use the section on technical documentation to check the shim dimensions.

■ Eliminating axial play

If there is any axial play between the clutch or brake and the components used in combination with it after assembly, the performance of the clutch or brake could be impaired. Design to keep play extremely small. Many types of shims are available for keeping the axial play to a very slight amount. They match the shaft diameters and bearing outer diameters dimensions used most.

If C-shaped retaining rings are also used, a secure lock can be achieved while preserving the spring effect of the retaining ring.

How to use shims

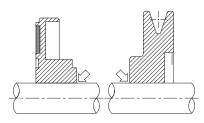


Fitting Tolerances

Clutches and brakes must be able to do large amounts of work instantly while also performing precise control. That means that the precision of all components must be appropriately unified so they do not cause wear or generate vibration. Fitting tolerances (grades) must also be determined so that they match the conditions of use.

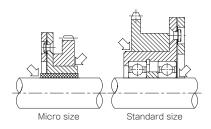
■ Fitting tolerance for rotor, armatures type-1 and type-2, V pulley, and shaft

The reference bore tolerance is H7 class. CYT models, however, have a special bore diameter tolerance (shown in the dimensions table). The table below shows dimensional tolerances for the shaft to be used.



Load conditions	Shaft to	lerance	Remark					
Shaft with Ø10 or below	h6	h7	h5 if accuracy is required					
Light/normal	h	6	For motor shaft, h6 or j6					
loads and fluctuating loads	js6	js7	For clutch/brake					
	j6	j7	unit shafts, j6					
Heavy loads and shock loads	k6	k7						
	n	16						

■ Fitting tolerances for armature type-5 and sprockets, or the like, and for armature type-5 and shafts



Clutch/brake	Armatur	re type-5	Bore tolerance for sprockets,	Shaft		
size	Boss tolerance	Bore tolerance	etc.	tolerance		
02 ~ 05	h7	H7	H7	h7 h8		
06 or over	j6	As given in table below	H7	As given in table above		

■ Tolerances for fitting ball bearing to housings

		J	o carring to ricacing.	
Load co	nditions	Bore tolerance	Remark	
	Heavy loads	N7		
Rotating outer ring load	Normal load and fluctuating loads	M7	,	
	Heavy shock loads			
Directionally unstable loads Rotating inner ring load	Heavy loads and normal loads	K7		
	Normal loads and light loads	J7		
	Shock loads			
	Ordinary loads	H7	When clutch/brake is not subject to shock	

^{*} Applicable to steel or iron housings. For light alloy housings, the fit must be stiffer.

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BRAKE MOTORS

POWER SUPPLIES

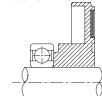
ELECTROMAGNETIC-ACTUATED CLUTCHES AND BRAKES

■ Tolerances for fitting ball bearings to shafts

Load co	nditions	Bore toler	ance	Remark
Rotating ou	ter ring load	h6		When precision is required, h5
D: : !!	Light loads, normal	ø18 or below	h5	711111111111111111111111111111111111111
Dimensionally unstable loads	and fluctuating loads	ø100 or below	j6	
and rotating inner ring loads	Heavy loads and	ø18 or below	j5	J
	shock loads	ø100 or below	k5	

■ Fitting tolerances for bearings and other components

If bearings are mounted on the same part of the shaft as rotors, V pulleys or other components, give priority to the bearing when determining the grade of the shaft by using the tolerance for fitting ball bearings to shafts.



Bore Diameters and Keyways

■ Bore diameters

Standard bore diameters are determined for each size (shown in the dimensions table) and available for selection. If you wish to use a nonstandard bore diameter, pilot bores are provided on 101 and 111 type rotors and armatures type-1 and type-2. Adhere to the drilling ranges and cautions noted below. The ranges of bore diameters that can be drilled are shown in the table below.

- Make the fitting tolerance of the bore H7 class.
- Pay sufficient attention to concentricity and perpendicularity when drilling bores.
- The outer circumference of the rotor can become misshapen if force is applied, so do not chuck it.
- Completely remove all cutting oil, cleaning oil, and the like from the bore and dry it before mounting the piece on machinery.

Keys and keyways

Keyways of rotors and armatures are made to Miki Pulley standards, which are based on JIS standards. (See the page on standard bore drilling standards for clutches and brakes.) CYT models, however, use special keyway tolerances (shown in the dimensions table).

Use JIS standard keys and keyways on the shafts to be used. (Refer to the pages on technical documentation extracted from JIS B 1301-1996) Follow this standard also for rotor and armature hub.

Bore dia	ore diameter processing ranges for rotors, armature type-1, and armature type-2.																							
C	lutch/brake	Bore diameter																						
	size	5	6	8	(8.5)	10	12	(12.5)	15	17	(18.5)	20	(24)	25	28	30	32	35	40	48	50	60	70	75
02	Rotor (R)	•																						
UZ	Armature (A)	•																						
03	Rotor (R)		•																					
US	Armature (A)		•																					
04	Rotor (R)			•		•																		
04	Armature (A)			•		•																		
05	Rotor (R)					•			•															
05	Armature (A)					•			•															
0.4	Rotor (R)						•		•															
06	Armature (A)						•		•															
08	Rotor (R)								•			•												
00	Armature (A)											•												
10	Rotor (R)											•		•										
10	Armature (A)											•		•										
12	Rotor (R)													•		•								
12	Armature (A)													•		•								
16	Rotor (R)															•			•					
10	Armature (A)															•			•					
20	Rotor (R)																		•		•			
20	Armature (A)																		•		•			
25	Rotor (R)																				•	•		
23	Armature (A)																				•	•		

^{*} The ● mark indicates a standard bore diameter. is the range of bore diameters that can be drilled in products with pilot bores.

^{*} If a bore diameter is given in parentheses, the bore is a pilot bore. (The final bore has not been drilled.) * The above table does not apply to CYT, CS, CSZ, and BSZ models.

I Environment for Mounting Parts

Take the environment where the clutch or brake will be used into account in your design.

■ Temperature

Clutches and brakes are heat resistance class B. Their operating temperature range is -10 to 40°C. If used at higher temperatures, heat generated by actual engagement and braking work cannot be dissipated and the coil and/or frictional parts may be damaged. The devices may be used at temperatures below -10°C if the heat generated by the clutch or brake keeps the devices at -10°C or above. However, moisture may adhere through condensation if stationary for longer periods of time or if used at low frequency, potentially leading to decreased performance. Use in extreme environments of -20°C and below may lead to problems. Consult Miki Pulley for details.

Humidity and dripping

As with temperature, water droplets adhering to the frictional surfaces will temporarily decrease frictional force until the surface dries, so place a cover on the equipment or otherwise protect it. The adherence of moisture can cause rust.

■ Infiltration of dust, oils, and other foreign matter

The infiltration of foreign matter into the frictional surface is undesirable. Infiltration of oils markedly degrades frictional force. Dust, especially if it contains metal particles, can cause problems by damaging the frictional surface and rotating parts. Chemical infiltration can cause corrosion, in addition to the rust described above.

In such environments, consider the use of a protective cover.

Since clutches and brakes convert frictional energy into heat and dissipate it externally, it is preferable to install them in well ventilated locations. Forced air cooling (with a fan or the like) can be used effectively to increase the allowable energy. If you are using the equipment in a poorly ventilated location, consider temperatures carefully.

Max. Rotation Speed

The max. rotation speeds of clutches and brakes are shown in the specifications table. This value is determined by the circumferential speed of the frictional surface, so when used beyond the max. rotation speed, not only will the indicated torque not be generated, abnormal wear, heat damage, and the like may occur.

Ball Bearings

Ball bearings are widely used in combination with clutches and brakes, with deep groove ball bearings the most widely used among them. Since it is undesirable to get oils on the frictional surfaces of dry-style clutches and brakes, use double-sealed bearings that do not require the addition of oil. Non-contact style double-sealed bearings that use rubber seals not only do not require the addition of oil, they are also excellent at keeping out dust. Metal double-sealed bearings can also be used for compact bearings and some hard-to-obtain bearings.

Mechanical Strength of Components

Clutches and brakes have excellent operational characteristics, so they are able to instantly engage or brake loads. For that reason, machinery components may experience impact forces. Be sure to build sufficient strength into your design. (Note that an overly safe design may increase load torque or affect the precision of engagement/braking.)

Vibration and Rattle

The structural components of clutches and brakes are adequately balanced so vibration does not occur. Mounting rattle can occur, however, after repeated shocks, and that can produce vibration noise. Use a design without rattle.

Corrosion Prevention

Clutches and brakes are treated to prevent corrosion, but rust may occur if storage conditions are poor or if the device is used in certain environments. Moderate rust does not present a problem for use, but we advise that you care for the equipment so that it does not rust.

Sparking

Sparks may be produced during clutch or brake use. This is because of friction between the armature and the magnetic part of the frictional surface. Adequate checks are required when using this equipment in volatile atmospheres.

Designing for Maintenance

Clutches and brakes require virtually nothing in the way of maintenance over the long term.

However, you can get even longer use out of them by proper maintenance of the air gap of the frictional parts and the ball bearings used. We recommend that you design structures so they can be easily disassembled and reassembled.

For details, refer to the operating manual.

Use of Micro Clutches

When using bearing-mounted micro clutches (in which the bearings are oil-impregnated metal), energization rate, temperature and the like may sometimes be restricted. Consult Miki Pulley for details.

Overhang Load of Unit

The table below shows the allowable values for radial load that can be applied to the shaft of the unit. Allowable values will vary somewhat on through-shaft model units due to the directions in which input and output loads act. (The values shown are for the most demanding conditions. The load point is the center point of the shaft.)

Size	125- □ -12 126- □ -4B	121-	121-□-10G 122-□-20G	
	W	W ₁ (W ₂)	W ₁ W ₃ W ₂	W ₃
05	250	-	-	_
06	320	300 (320)	140	140
08	480	450 (500)	250	250
10	700	700 (800)	450	450
12	900	900 (1000)	700	700

1000

1800

2600

1000

1800

2600

1400 (1600)

2000 (2500)

2900 (3600)

1300

1800

16

20

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES FI FCTROMAGNETIC ACTUATED **CLUTCHES & BRAKES**

> FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

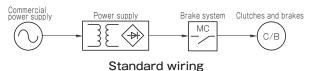
^{*} Numbers in parentheses are for loads in the same direction.

ELECTROMAGNETIC-ACTUATED CLUTCHES AND BRAKES

Control Circuits

Basic Structure of Electrical Circuits

When designing the electrical circuitry that controls clutches and brakes, the selection of the control method and control equipment is very important. The correct selection of these and designing the circuit both stabilize the operating characteristics of clutches and brakes and increase the reliability of machinery. A DC 24 V (standard specification) power supply is needed to operate clutches and brakes. For this, either a DC power supply can be used, or an AC power supply can be stepped down and rectified. We have a variety of power supply devices dedicated for clutches and brakes available. For details, refer to the page on power supplies.



Selecting Components for Power Supplies

■ Transformers

Match the primary side to the supply voltage. On the secondary side, use something with sufficient capacity to be able to apply the rated voltage to the clutch (brake) coil.

As a guideline, select a transformer that has a capacity 1.25 times the rated capacity of the clutch (brake) at 20° C. Note that the secondaryside output voltage must be set according to the rectifier's voltage drop or the transformer's impedance drop. These can be found in simplified terms, from Eqs. (1) and (2) below.

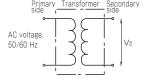
$$V_2 = \frac{V + 1.4}{0.9} [V]$$
(1)

Eq. (1) is from the single-phase full-wave rectification system.

$P \ge W_{CB} \times 1.25 \text{ [VA]}$

V2: Transformer secondary voltage [V] V: DC voltage [V]

P: Transformer capacity [VA] WcB: Clutch (brake) capacity [VA]



(2)

Rectifiers

There are several different rectification systems. Miki Pulley uses singlephase full-wave rectification (the bridge system). For a system to be selected, the maximum rated value of the rectifier must not be exceeded. The rated maximum can be found in simplified terms using the following Eq. (3).

• Determining withstand voltage VRM in the reverse direction

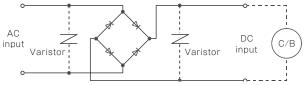
$$V_{RM} = V_{L^{\bullet}} \sqrt{2} \cdot K$$
 (3)

VL: AC input voltage [V]

K: Safety factor (make the factor between 2 and 3)

Note that if a surge voltage at or above the withstand voltage may find its way in from outside, the rectifier must be protected.

• Determining the average rectification current Select a rectifier that has an average rectification current value of 1.5 or more times the rated current of the clutch (or brake) used. Note that when large currents flow, temperature rise becomes a problem. Take measures to give the device a heat dissipation effect and to suppress extreme temperature rises.



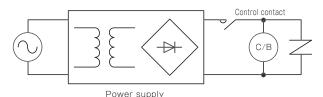
Single-phase full-wave rectified

■ Relays (control contacts)

Since electromagnetic clutches and brakes have internal electromagnetic coils, they must be used under the conditions of the DC inductive load of the relay you will use.

This is because contacts are heavily worn by surge voltage generated during electromagnetic clutch or brake control.

If relay service life, operational frequency, and the like are problems in use, the design must be contactless. For details, see the page on controlling electromagnetic clutches and brakes using power supplies.



DC switching

■ Points to note on control circuit structure

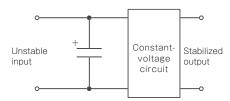
· Control of clutches and brakes

When controlling the clutch or brake on the AC side, armature release time lengthens and high-frequency operation becomes impossible. Install control contacts on the DC side.

· Voltage supplied to the clutch or brake When designing a power supply circuit, keep fluctuation of the excitation voltage to within \pm 10% of the rated voltage of the clutch or brake.

· Smoothing of excitation voltage

Normally, the power supply for the clutch or brake is a single-phase full-wave rectifier. When high precision is required, however, better results are obtained by smoothing.



Stabilized power supply circuit

Protection of control contacts

If a protective circuit is placed in the clutch/brake, the control contacts will be protected, but the protective effect will be greater if CR absorbers are used between contacts, as shown in the figure. C (capacitor) and R (resistor) are roughly as follows.

Capacitor C [u F]: Ratio to contact current is:

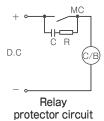
$$\frac{\mathsf{C}[\;\mu\;\mathsf{F}]}{\mathsf{I}[\mathsf{A}]} = \frac{0.5\,\mathsf{to}\,\mathsf{1}}{\mathsf{1}}$$

Withstand voltage: 600 [V]

Resistance R[Ω]: Ratio to contact voltage is:

$$\frac{R[\Omega]}{E[V]} \pm 1$$

Capacity = 1 [W]



■ Discharge circuits

When a DC excitation current flows in an electromagnetic clutch or brake, energy accumulates in the coil. If current is then shut off, a surge voltage is generated between the coil terminals by the accumulated energy. This surge voltage may reach 1000 V or more depending on the shutoff speed, shutoff current, and other factors, so it can cause damage to the coil insulation, burn the contacts in switches, and more. Appropriate discharge circuits must therefore be installed to prevent such problems.

Different types of discharge circuits have differing armature discharge times and effectiveness in suppressing surge voltages. The table below shows the characteristics of some discharge circuits.

While different discharge circuits have many advantages and disadvantages, the type we recommend are varistors.

ELECTROMAGNETIC

CLUTCHES & BRAKES

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC-ACTUATED

CLUTCHES & BRAKES ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

Very effective in keeping surge voltage small without and delay to the armature release time. Can lower power consumption in the power supply par reduce resistor capacity. The armature release time become somewhat longer, so care is required in high frequency use delayed, so clutch and brake are more prone to interfere each other, making diodes unsuitable for high frequency use the power supply par reduce resistor capacity. The armature release time become what longer, so care is required in high frequency use the power supply particles. Have a short armature release time, but require capacitors.		Circuit diagram	Current decay	Characteristics
Can lower power consumption in the power supply par reduce resistor capacity. The armature release time becomewhat longer, so care is required in high frequency use Diodes Good at suppressing surge voltage, but armature release time delayed, so clutch and brake are more prone to interfere each other, making diodes unsuitable for high frequency use Have a short armature release time, but require capacitors	Varistor	+ 0 MC		Very effective in keeping surge voltage small without adding delay to the armature release time.
Good at suppressing surge voltage, but armature reledelayed, so clutch and brake are more prone to interfere each other, making diodes unsuitable for high frequency under the suppression of the suppressi	Resistors + diodes	+ O R C/B		Can lower power consumption in the power supply part and reduce resistor capacity. The armature release time becomes somewhat longer, so care is required in high frequency use.
Have a short armature release time, but require canacitor	Diodes	+		Good at suppressing surge voltage, but armature release is delayed, so clutch and brake are more prone to interfere with each other, making diodes unsuitable for high frequency use.
Resistors + capacitors high pressure resistance.	Resistors + capacitors	+0		Have a short armature release time, but require capacitors with high pressure resistance.

Commercial Power Supply Specifications

Model	Rectification method	Frequency [Hz]	AC input voltage AC [V]	DC output voltage DC [V]	Wattage [W]	Applicable clutch/ brake size
BES-20-05	Single-phase, full-wave	50/60	200	24	50	02 ~ 05
BES-20-10	Single-phase, full-wave	50/60	200	24	50	06 ~ 10
BES-20-16	Single-phase, full-wave	50/60	200	24	50	12 ~ 16
BES-20-20	Single-phase, full-wave	50/60	200	24	50	20
BES-40-25	Single-phase, full-wave	50/60	200	24	100	25
BES-20-05-1	Single-phase, full-wave	50/60	100	24	50	02 ~ 05
BES-20-10-1	Single-phase, full-wave	50/60	100	24	50	06 ~ 10
BES-20-16-1	Single-phase, full-wave	50/60	100	24	50	12 ~ 16
BES-20-20-1	Single-phase, full-wave	50/60	100	24	50	20
BES-40-25-1	Single-phase, full-wave	50/60	100	24	100	25

SPRING-ACTUATED BRAKES



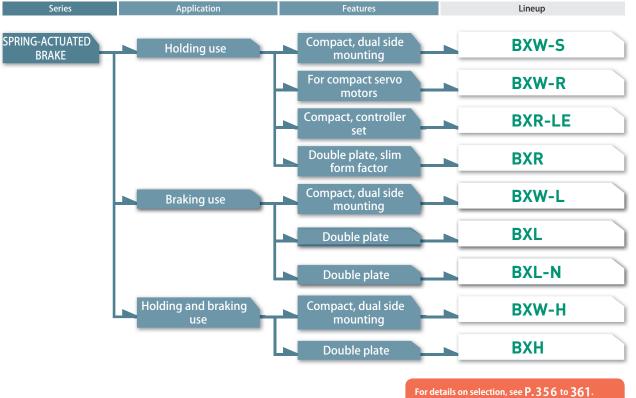
Motors, articulated robots, actuators, machine tools, forklifts, aerial vehicles, hoists, electric carts, electric shutters, medical equipment, wind turbing energators.

Provides Excellent Performance in Emergency Braking When Power Goes Out and in Long-term Holding

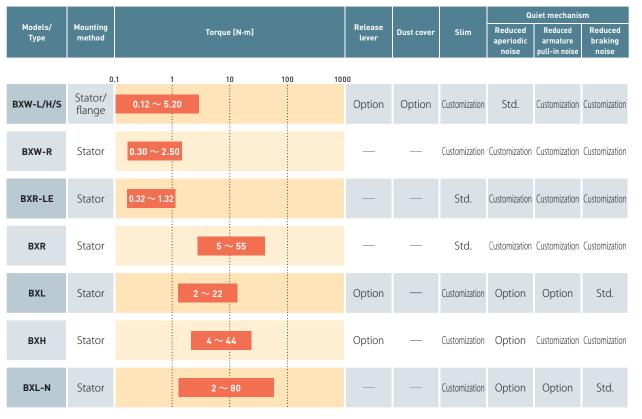
These are electromagnetic brakes actuated by the force of springs when not energized. These standard brakes boast a variety of advantages, including quiet operation, long service life, slim form factors, high torque in a compact package, stable braking force, and the ability to release manually. We can create custom designs for you based on these standard products.



Available Models



Model Selection



ELECTROMAGNETIC **CLUTCHES & BRAKES** SERIES ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** FI FCTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS SPRING-ACTUATED BRAKE ELECTROMAGNETIC

TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BXW BXR

BXL BXH

MODELS

BXL-N

Product Lineup

BXW-L/H/S













I Three types for various applications

The line-up includes three types: the S type for holding, the L type for braking, and the H type for both holding and braking.

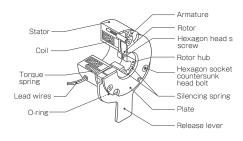
2-way mounting

The stator (a heat source) can be mounted facing either inwards or outwards.

Brake type		BXW-□-□L	BXW-□-□H	BXW-□-□S
Brake torque	[N·m]	$0.12 \sim 2.00$	$0.24 \sim 4.00$	$0.36 \sim 5.20$
Operating temperature	[℃]	−10 ~+40	−10 ~+40	−10 ~+40
Backlash		Extremely small size	Extremely small size	Extremely small size

Structure

Has release lever



BXW-R











Dedicated design for small servo motors

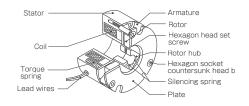
These have dedicated designs matched for specifications and dimensions for \square 40, \square 60, and \square 80 small servo motors.

Low-inertia rotor

We succeeded in dramatically reducing both mass and drag wear while ensuring adequate strength.

	-	
Brake torque	[N·m]	0.30 ~ 2.50
Operating temperature	[℃]	−10 ~+40
Backlash		Extremely small size

Structure



BXR-LE









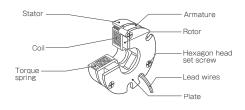


Ultra compact

Use with a built-in dedicated controller provides a range of benefits, including an ultra-thin profile, reduced energy consumption, lower heat emissions, higher torque and a longer service life.

Brake torque	[N·m]	0.32 ~ 1.32
Operating temperature	[℃]	- 10 ∼+ 40
Backlash		Extremely small size

Structure



BXR















This ultra-slim design is two-thirds the thickness of our previous design.

Low-inertia rotor

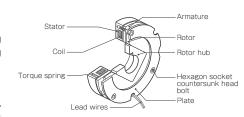
We succeeded in dramatically reducing both mass and drag wear while ensuring adequate strength.

Extremely small backlash

The backlash of the spline hub type is 0.2° to 0.5°.

Brake torque	[N·m]	5~55
Operating temperature	[℃]	− 10 ~+ 40
Backlash		Extremely small size

Structure

















Low noise

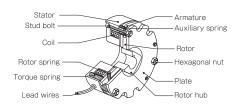
These reduce annoying high-frequency friction noise during braking. Products that reduce aperiodic noise or armature pull-in noise are also available.

Stable braking

With low torque fluctuation, these brake loads instantly even when malfunctions

Brake torque	[N·m]	2~22
Operating temperature	[℃]	−10 ~+40
Backlash		Extremely small size

Structure



ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

	ELECTROMAGNETIC-
	ACTUATED MICRO
	CLUTCHES & BRAKES
	ELECTROMAGNETIC-
	ACTUATED
	CLUTCHES & BRAKES
	ELECTROMAGNETIC
	CLUTCH & BRAKE
	UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BXH













I For both holding and braking

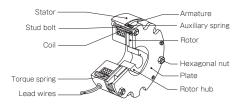
These brakes ensure sufficient torque for holding applications while also being usable as emergency brakes.

High torque

Provide twice the torque with the same dimensions as BXL models.

Brake torque	[N·m]	4~44
Operating temperature	[℃]	−10 ~+40
Backlash		Extremely small size

Structure



BXL-N













Low noise

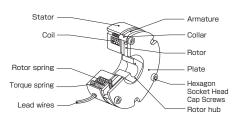
These reduce annoying high-frequency friction noise during braking. Products that reduce aperiodic noise or armature pull-in noise are also available.

Variety of torques

Two to three different kinds of braking torque for the same outer diameter are available to permit the most suitable design for the application at hand.

Brake torque	[N·m]	2∼80
Operating temperature	[℃]	0~+40
Backlash		Extremely small size

Structure



MODEL	S									
BXW										
BXR		 	 •	•	•	•	•	•		
BXL		 						•		
вхн		 				•		•		•
BXL-N		 • •		•	٠	•				

Customization Examples

■ BXW Large Type

This is a large version of the BXW with static friction torque of 300 N·m. Backlash is kept extremely small by locking the rotor hub to the rotor via a disc spring.



■ BXW Slim Type

Ultra-slim types 15 mm thick or less are available to fit the space in your device. Power consumption can also be kept to one-third the level of our standard products by using our dedicated controllers.



■ Types with Integrated Flanges

Mounting flanges and brake stators can be integrated. This helps reduce the number of components and saves space.



■ Special Release Levers

Release levers can also be designed for specific units to match the device construction.



Visit the MIKI PULLEY website for details.

FAQ

I don't see anything with the torque and response I need in your standard products. Can you customize something for me?

Me can customize units in many ways: outfitting them for overexcitation power supplies or use of inrush current at motor startup, changing the frictional material, boosting torque, increasing response, extending the total energy (service life), suppressing heat generation, and more. Consult Miki Pulley for details.



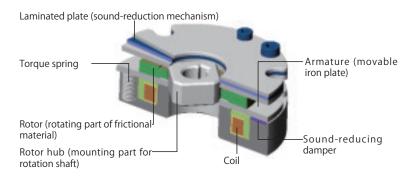
Q 2 Can you handle cases in which standard products cannot be installed due to dimensional constraints?

A Yes, we can. For example, we have a long track record creating slimmer units that deliver the same torque. These units can provide the same torque while being only about half as thick as the standard product, although this will vary with your conditions. Consult Miki Pulley for details.

Q3 What do you have for dealing with noise issues?

A Spring-actuated brakes have a number of types of noises, such as (1) rattling generated by microvibrations during rotating, (2) armature pull-in and release noise, (3) friction noise (chirping) during braking, and (4) grinding noise under drive (when the brake is released). We have ways of reducing all of these. The figure below shows an example.

To reduce pull-in/release noise: Special plate specification



To reduce grinding noise: Single-side braking specification



ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES

FI FCTROMAGNETIC ACTUATED **CLUTCHES & BRAKES**

FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BXW

BXR

BXL

BXH

BXL-N

BXW Models

Specifications

I BXW- □ - □ L (Braking use)

		Static friction		Coil (at	20°C)		res	Max.	Rotating part	Allowable braking	Total braking	Armature	Armature	
Model	Size	torque Ts [N·m]	Voltage [V]	Coil (at Wattage [W]	Current [A]	Resistance [Ω]	Heat istance class	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	energy rate Pba ℓ [W]	energy ET[J]	pull-in time ta [s]	release time t _{ar} [s]	Mass [kg]
			12	5.0	0.417	28.8	F							
			24	5.0	0.208	115	F							
BXW-01-10L	01	0.12	45	5.0	0.111	405	F	5000	0.6×10^{-6}	2.5	1.5×10^{6}	0.008	0.015	0.2
			90	5.0	0.056	1622	F							
			180	5.0	0.028	6486	F							
			12	6.6	0.550	21.8	F							
BXW-02-10L BXW-02-12L			24	6.6	0.275	87.3	F							
	02	0.25	45	6.6	0.147	307	F	5000	1.9×10^{-6}	5.0	3.0×10^{6}	0.008	0.015	0.3
			90	6.6	0.073	1228	F							
			180	6.6	0.037	4912	F							
		0.50	12	9.0	0.750	16.0	F							
BXW-03-10L			24	9.0	0.375	64.0	F	5000						
BXW-03-12L	03		45	8.2	0.182	247	F		3.8 × 10 ⁻⁶	10.0	4.5 × 10 ⁶	0.025	0.025	0.4
			90	8.2	0.091	988	F							
			180	8.2	0.046	3954	F							
			12	11.5	0.958	12.5	F							
BXW-04-10L			24	11.5	0.479	50.1	F							
BXW-04-12L	04	1.00	45	10.0	0.222	203	F	5000	12.0×10^{-6}	20.0	7.0×10^{6}	0.030	0.030	0.6
			90	10.0	0.111	810	F							
			180	10.0	0.056	3241	F							
			12	13.0	1.083	11.1	F							
BXW-05-10L	0.5	2.00	24	13.0	0.542	44.3	F	5000	22.0 \(\) 10-6	30.0	120 × 106	0.035	0.035	0.0
BXW-05-12L	05	2.00	45	13.0	0.289	156	F	5000	23.0×10^{-6}	30.0	12.0×10^{6}	0.035	0.035	8.0
			90	13.0	0.144	623	F							
			180	13.0	0.072	2492	F							

I BXW- □ - □ H (Holding and braking use)

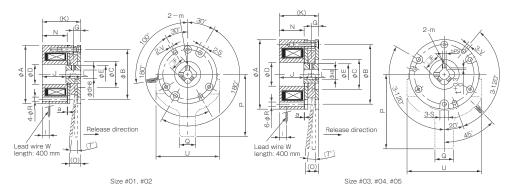
Size		tic friction		Coil (at	20°C)		æ	Max	Rotating part	Allowable braking	Total braking	Armature	Armature	
. 6	!	torque Ts [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance $[\Omega]$	Heat sistance class	Max. rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	energy rate Pba & [W]	energy ET[J]	pull-in time ta [s]	release time t _{ar} [s]	Mass [kg]
			12	5.0	0.417	28.8	F							
			24	5.0	0.208	115	F							
- 10H 01	1	0.24	45	5.0	0.111	405	F	5000	0.6×10^{-6}	0.5	0.2×10^{6}	0.010	0.010	0.2
			90	5.0	0.056	1622	F							
			180	5.0	0.028	6486	F							
			12	6.6	0.550	21.8	F							
1011			24	6.6	0.275	87.3	F							
	2	0.50		6.6	0.147	307	-	5000	1.9×10^{-6}	1.0	0.3×10^{6}	0.010	0.010	0.3
				6.6	0.073	1228								
-10H														
-12H 03	3	1.00						5000	3.8×10^{-6}	2.0	0.5×10^{6}	0.035	0.020	0.4
-10H														
-12H ⁰⁴	1	2.00					-	5000	12.0×10^{-6}	4.0	1.0 × 10 ⁶	0.040	0.025	0.6
-10H or	_	4.00						5000	22.0 × 10-6		2011106	0.045	0.030	0.0
-12H ^{US})	4.00						5000	23.0 × 10 ⁻⁶	6.0	2.0 × 10°	0.045	0.030	0.8
BXW-05-12H														
-10H 04 -12H 04	3	0.50 1.00 2.00		6.6 6.6	0.275 0.147	87.3 307		5000 5000 5000	1.9×10^{-6} 3.8×10^{-6} 12.0×10^{-6} 23.0×10^{-6}	1.0 2.0 4.0	0.3×10^{6} 0.5×10^{6} 1.0×10^{6} 2.0×10^{6}	0.010 0.035 0.040		0.010 0.020 0.025

■ BXW- □ - □ S (Holding use)

		Static friction	Coil (at 20°C)					Max.	Rotating part	Allowable braking	Total braking	Armature	Armature	Mass
Model	Size	torque Ts [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance $[\Omega]$	Heat esistance class	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	energy rate Pba & [W]	energy Eτ[J]	pull-in time ta [s]	release time t _{ar} [s]	Mass [kg]
BXW-01-10S	01	0.36	24	5.0	0.208	115	F	5000	0.6×10^{-6}	_	_	0.025	0.010	0.2
BXW-02-10S BXW-02-12S	02	0.75	24	6.6	0.275	87.3	F	5000	1.9 × 10 ⁻⁶	-	-	0.030	0.010	0.3
BXW-03-10S BXW-03-12S	03	1.50	24	9.0	0.375	64.0	F	5000	3.8×10^{-6}	-	-	0.035	0.020	0.4
BXW-04-10S BXW-04-12S	04	2.60	24	11.5	0.479	50.1	F	5000	12.0×10^{-6}	-	-	0.040	0.025	0.6
BXW-05-10S BXW-05-12S	05	5.20	24	13.0	0.542	44.3	F	5000	23.0×10^{-6}	-	-	0.045	0.030	0.8

 $[\]ensuremath{^{*}}$ The armature pull-in time and armature release time are taken during DC switching.

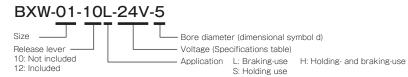
Dimensions



							3126 #0	1, #02								3/26 #05. #04. #05							Unit [mm]			
Size							Radial	direct	ion din	nensions							Axi	al direc	tion d	imenti	ons		Bore dimensions			
ze	Α	В	С	D	E	S	V	R	F	W	m	0	Р	Q	U	G	-1	J	K	L	N	а	d	b	t	
01	37	32	18	13.5	12.0	6	3	3	10	AWG26	М3	-	-	-	-	4.5	5.0	22.5	32	9	22.5	0.10	5 6	-	-	
02	47	40	21	16.0	14.5	7	3.4	3.4	12	AWG26	М3	9	50	13	51	6.0	5.5	19.2	32	12	20.0	0.10	6 7	-	-	
03	56	48	24	19.0	17.0	7	3.4	3.4	14	AWG26	M3	11	60	15	60	6.0	6.0	19.9	32	12	20.0	0.15	8	-	_	
04	65	58	35	24.0	22.0	7	3.4	3.4	18	AWG22	M4	12	70	15	70	7.0	7.0	19.9	34	14	21.0	0.15	10	3	1.2	
05	75	66	36	28.0	26.5	9	4.5	4.5	22	AWG22	M4	14	80	20	80	7.0	7.0	22.1	36	14	21.5	0.15	12	4	1.5	

^{*} There is no release lever option for size #01.

How to Place an Order



* Models equipped with the release lever and models with 12-V and 180-V voltage specifications are made to order.

* Contact Miki Pulley for assistance with bore diameters, d, not listed in the Dimensions tales and voltages not listed in the Specifications table.

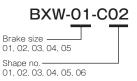
Options: Dust Cover

Dust covers are available as options. These enable use in challenging environments by keeping out foreign matter.

Dust covers come in two types: full covers that have no hole for the shaft, and shaft-hole covers, which can be used on brakes mounted with the shaft passing through. You can also choose the locations of the lead exit holes for brakes mounted on plates or mounted on stators.



How to Place an Order

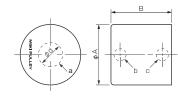


Specifications

Material	Ethylene propylene diene monomer (EPDM) rubber
Temperature range	-40°C to 140°C
Exterior color	Black
Applicable brake models	L type, H type, S type BXW models
Applicable brake sizes	#01, #02, #03, #04, #05
Applicable specification voltages	12 V DC, 24 V DC, 45 V DC, 90 V DC, 180 V DC

- * This temperature range is for dust cover materials. The operating temperature for BXW models is -10°C to 40°C.
- Cannot be mounted on BXW models with release levers or R-type BXW models.

Dimensions



Shape No.	а	b	c
01	×	×	×
02	×	×	0
03	×	0	×
04	0	×	×
05	0	×	0
06	0	0	×

			Unit [mm]
Model	φ A	В	φ d
BXW-01-C	41	33	16
BXW-02-C □	51	33	21
BXW-03-C □	60	33.5	24
BXW-04-C □	69	35.5	30
BXW-05-C □	79	37.5	30

 * Symbol a indicates a hole made for brakes with shafts passing through; symbol b indicates a hole made for lead exit when mounted on a plate; symbol c indicates a hole made for lead exit when mounted on a stator.

C017

 $\mbox{\ast}$ Shapes #01 and #04 require that a hole be made separately for leads to exit.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNET	ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
	ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BXW BXR

MODELS

BXL BXH BXL-N

BXW Models

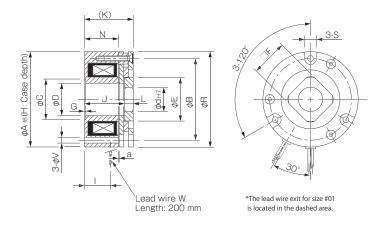
Specifications (BXW- \square - \square R)

(For servo motors)

			Static	Coil (at 20°C)				Max.		Rotating part	Allowable	Total	Armature	Armature		
Me	odel	Size	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat istance class	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	braking energy rate Eba & [J]	braking energy Et [J]	pull-in time t _a [s]	release time t _{ar} [s]	Mass [kg]	
BXW-	01-10R	01	0.3	24	6.1	0.254	94.4	F	6000	1.36×10^{-7}	15	3000	0.035	0.020	0.1	
BXW-	03-10R	03	1.3	24	7.2	0.300	80.0	F	6000	1.17×10^{-6}	87	17000	0.050	0.020	0.3	
BXW-	05-10R	05	2.5	24	8.0	0.333	72.0	F	6000	3.68×10^{-6}	200	40000	0.060	0.020	0.5	

 $^{^{\}ast}$ The armature pull-in time and armature release time are taken during DC switching.

Dimensions



Unit [mm]

Size				Radia	al direction	on dimen	sions				Axial direction dimentions							Bore dimensions		
ze	Α	В	С	D	E	S	V	R	F	w	G	Н	-1	J	K	L	N	a	d	d max
01	33	26.5	16	9	14	7	3.4	32.5	12	AWG26	0.2	4	19	26	30	4	22.8	0.1	8.5	8.5
03	48	42	26	14	23	8	3.4	47.5	19	AWG22	0.2	4	18	26	30	4	22.6	0.1	11	15
05	64	56	28	22	31	8	4.5	63.5	25	AWG22	0.2	4	16	25.5	30	4.5	21.3	0.1	16	20

^{*} Bore diameters other than the standard bore diameters given above are also possible. d max indicates the maximum bore diameter with a round shaft.

To download CAD data or product catalogs:

How to Place an Order



 * Contact Miki Pulley for assistance with bore diameters, d, not listed in the Dimensions tales and voltages not listed in the Specifications table.

^{*} In addition to round bores, key processing can also be handled. Consult Miki Pulley for details. * Dimensions, mounting and the like are not interchangeable with other BXW models.

Items Checked for Design Purposes

Precautions for Handling

■ Brakes

Most electromagnetic braking systems are made using flexible materials. Be careful when handling such parts and materials as striking or dropping them or applying excessive force could cause them to become damaged or deformed.

Lead Wires

Be careful not to pull excessively on the brake lead wires, bend them at sharp angles, or allow them to hang too low.

■ Frictional Surface

Since these are dry brakes, they must be used with the frictional surface dry. Keep water and oil off of the frictional surfaces when handling the brakes.

Precautions for Use

Environment

These brake units are dry braking systems, meaning that the torque will drop if oil residue, moisture, or other liquids get onto friction surfaces. Attach the protective cover when working in areas with oil, moisture, dust, and other particles that could affect the braking system.

■ Operating Temperature

The operating temperature range is -10° C to 40° C. If you will use the product at other temperatures, consult Miki Pulley.

■ Power Supplies

BXW models use commercial AC 100 V or 200 V single phase, full-wave rectified or half-wave rectified. Select as appropriate for your application. See the table below, "Recommended power supplies and circuit protectors," for the power supply devices we recommend.

■ Power Supply Voltage Fluctuations

Full braking performance may not be guaranteed with extreme changes in power supply voltage. Make sure to keep power supply voltage to within $\pm\,10\%$ of the rated voltage value.

Air Gap Adjustment

BXW models do not require air gap adjustment. The brake air gap is adjusted when the braking system is shipped from the factory.

Circuit Protectors

If using a power supply that is not equipped with a circuit protector for DC switching, make sure to connect the recommended circuit protector device in parallel with the brake.

Recommended Power Supplies and Circuit Protectors Recommended power supplies

Input AC power	Brake voltage	Rectification method	Recommended power supply model
AC100V 50/60Hz	DC24V	Single-phase, full-wave	BES-20-71-1
AC100V 50/60Hz	DC45V	Single-phase, half-wave	BEW-1R
AC100V 50/60Hz	DC90V	Single-phase, full-wave	BEW-1R
AC200V 50/60Hz	DC24V	Single-phase, full-wave	BES-20-71
AC200V 50/60Hz	DC90V	Single-phase, half-wave	BEW-2R
AC200V 50/60Hz	DC180V	Single-phase, full-wave	BEW-2R
AC400V 50/60Hz	DC180V	Single-phase, half-wave	BEW-4R

^{*} A DC power supply such as a battery can also be used to supply the 24 V DC required for the brake voltage

Recommended circuit protectors

ı	Input voltage	Brake voltage	Rectification method	Recommended circuit protector (varistor)
	DC24V	DC24V		NVD07SCD082 or an equivalent
	AC100V 50/60Hz	DC45V	Single-phase, half-wave	NVD07SCD220 or an equivalent
	AC100V 50/60Hz	DC90V	Single-phase, full-wave	NVD07SCD220 or an equivalent
	AC200V 50/60Hz	DC90V	Single-phase, half-wave	NVD07SCD470 or an equivalent
	AC200V 50/60Hz	DC180V	iuii-wave	NVD07SCD470 or an equivalent
	AC400V 50/60Hz	DC180V	Cincola orbana	NVD14SCD820 or an equivalent

^{*} NVD

SCD

parts are manufactured by KOA Corporation.

Precautions for Mounting

■ Mounting Orientation

BXW models can be mounted with the stator facing inwards (stator mounted) or outwards (plate mounted). Select your mounting orientation as the application dictates. Be aware, however, that the BXW-R type is only compatible with stator centering-mark mounting. Your understanding is appreciated.

Affixing the Rotor Hub

Affix the rotor hub to the shaft with hex-socket-head set screws such that the rotor hub does not touch the armature or stator. If you are applying adhesive to the hex-socket-head set screws, be careful that the adhesive does not come out onto the rotor hub surface. Note also that since the BXW-R type is constructed so that the rotor hub does not go through the stator, affix it by press-fitting it onto the shaft at a position that does not touch the armature (see dimension J) when they are assembled.

Bolts and Screws

Implement screw-locking measures such as use of an adhesive threadlocking compound to bolts and screws used to install brakes.

Shafts

The shaft tolerance should be h7 class (JIS B 0401). Be aware that the harder the material used for the shaft, the lower the effect of the hexsocket-head set screws.

■ Accuracy of Brake Attachment Surfaces

Make sure that concentricity (X) and perpendicularity (Y) do not exceed the allowable values of the table below.

Allowable concentricity and perpendicularity values for the BXW

		•
Size	Concentricity (X)	Perpendicularity (Y)
Size	T.I.R. [mm]	T.I.R. [mm]
01	0.05	0.02
02	0.05	0.02
03	0.10	0.02
04	0.10	0.02
05	0.10	0.02

Stator mounted

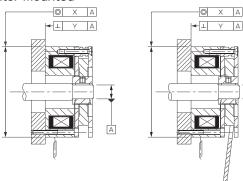
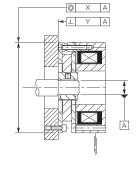
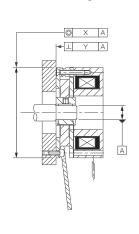


Plate mounted





ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

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ELECTROMAGNETIC
CLUTCH & BRAKE
LINITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BXW BXR BXL **BXH** BXL-N

DC24V indicates a product recommended with a stepdown transformer or the like.

^{*} BXW models do not come with circuit protectors.

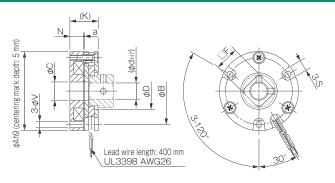
BXR-LE Models For holding

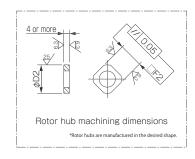
Brake unit

Specifications

		Static	Coil (at 20°C)					res	Max.	Rotating part	Allowable	Total	Armature	Armature	
Model	Size	friction torque T _s [N·m]	Output	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	Heat resistance class	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	braking energy rate Eba & [J]	braking energy E _T [J]	pull-in time (24 V DC) ta [s]	release time (7 V DC) tar [s]	Mass [kg]
BXR-01-10LE	01	0.32	Overexcitation Constant excitation		22.0 1.9	0.92 0.27	26.2	F	6000	2.5 × 10 ⁻¹⁰	15	3000	0.035	0.020	0.08
BXR-02-10LE	02	0.62	Overexcitation Constant excitation		22.0 1.9	0.92 0.27	26.2	F	6000	3.8 × 10 ⁻¹⁰	87	17000	0.050	0.020	0.12
BXR-03-10LE	03	1.32	Overexcitation Constant excitation		26.0 2.2	1.08 0.32	22.2	F	6000	4.0 × 10 ⁻¹⁰	87	17000	0.060	0.020	0.16

Dimensions





Unit [mm]

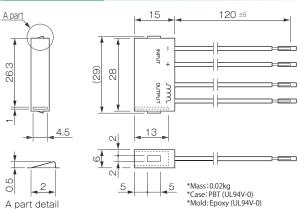
Model	Si		Radial direction dimensions								rection dim	entions	Rotor hub machining dimensions		
Model	ize	φΑ	φΒ	φC	φD	φ d:Max.	□F	S	φV	K	N	a	φ D2	□ F2	
BXR-01-10LE	01	39	33	9	18	8	12	5.5	3.0	14	7.0	0.1	14 _ 0.1	$12_{-0.07}^{0}$	
BXR-02-10LE	02	48	42	15	28	14	19	5.5	3.0	14	7.0	0.1	23 _0.1	19_007	
BXR-03-10LE	03	56	50	15	27	14	19	6.5	3.4	14.5	7.4	0.1	23 0,	19 007	

Controller

Specifications

Мо	del	BEM-24ES7-12	ON					
Input v	oltage	24V DC ± 10% smoothing	power supp	oly				
Output	voltage	Initial: 24 V DC (0.2 sec.) Constant: 7 V DC (\pm 10%), PWM control						
Max. outp	ut current	1.0 A DC (ambient temp.: 20 $^{\circ}$ C), 0.8 A DC (ambient temp.: 60 $^{\circ}$ C)						
Time rating		Continuous						
Insulating resistance		500 V DC, 100 M Ω with Megger (input/output - between terminal and case)						
Dielectric stre	ength voltage	1000 V AC, 50/60 Hz, 1 min. (input/output - between terminal and case)						
Ambient er	nvironment	-20 to 60° C, 5 to 95% RH, no co	ndensation/	freezing				
Lead wire	Function	Description	Specifi	cation				
Red	Input (+)	Connects the 24 V DC smoothing power supply (+)	UL3398	AWG22				
Black	Input (-)	Connects the 24 V DC smoothing power supply (-)	UL3398	AWG22				
Yellow	Output	Connects the spring-actuated brake (either pole)	UI 3398	AWG22				

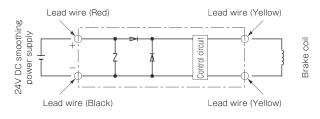
Dimensions



Structure

Output

Yellow

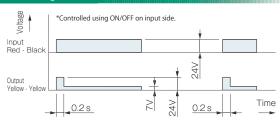






UL3398 AWG22

Timing Chart



Items Checked for Design Purposes

I Precautions for Handling

■ Brakes

Electromagnetic brakes use many soft materials. Care should be taken during handling as accidentally striking, dropping or applying excessive force to the brake could cause denting or deformation.

■ Lead wires

Be careful not to pull excessively on the brake lead wires, bend them at sharp angles or allow them to hang too low.

■ Friction Surfaces

Since these are dry brakes, they must be used with the friction surfaces dry. Keep water and oil away from the friction surfaces when handling the brakes

I Precautions for Mounting

■ Affixing the Rotor Hub

The BXR LE models are specifically designed to be as compact as possible and the rotor hub can be freely designed for a particular purpose. In the design, the rotor hub should be installed such that it does not touch the armature or stator. Also, with the normal installation method of using hexagon-socket set screws coated with adhesive, take care not to trap adhesive between the screws and the rotor hub surface.

■ Bolts and Screws

Implement screw-locking measures such as use of an adhesive thread locking compound to bolts and screws used to install brakes.

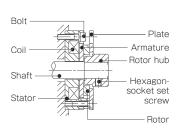
■ Shafts

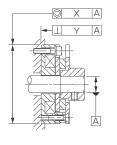
The shaft tolerance should be h7 class (JIS B 0401).

■ Accuracy of Brake Attachment Surfaces

Make sure that the centering mark and shaft concentricity (X) and the shaft perpendicularity (Y) relative to the brake mounting surface do not exceed the allowable values in the table below.

Model	Size	Concentricity (X)	Perpendicularity (Y)
Model	Size	T.I.R. [mm]	T.I.R. [mm]
BXR-01-10LE	01	0.05	0.02
BXR-02-10LE	02	0.05	0.02
BXR-03-10LE	03	0.10	0.02





Precautions for Use

■ Environment

These brake units are dry braking systems, meaning that the torque will drop if oil residue, moisture, or other liquids get onto friction surfaces. Attach the protective cover when working in areas with oil, moisture, dust or other particles that could affect the braking system.

■ Operating Temperature

The operating temperature range is -10 $^{\circ}$ C to 40 $^{\circ}$ C for brakes and -20 $^{\circ}$ C to 60 $^{\circ}$ C for dedicated controllers. If you will use the product at other temperatures, consult Miki Pulley.

■ Power Supply Voltage Fluctuations

Full braking performance may not be guaranteed with extreme fluctuations in power supply voltage. Keep the power supply voltage to within \pm 10% of the rated voltage.

■ Air Gap Adjustment

BXR LE models do not require air gap adjustment. The brake air gap is adjusted at shipment from the factory.

■ Circuit Protectors

Circuit protectors should not be connected as they are built into the dedicated controllers.

■ Controller Operation

The control function is operated by the ON/OFF switch on the input side, so switching should be carried out by the input side of the dedicated controller.

COUPLINGS

ETP BUSHINGS

ELECTROMAGNETIC CLUTCHES & BRAKES

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INVERTERS

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ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
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ELECTROMAGNETIC
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UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BXW

BXL

вхн

BXL-N

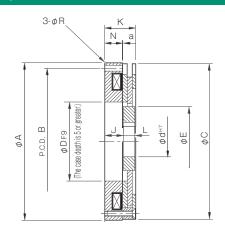
BXR Models Square Hub Type

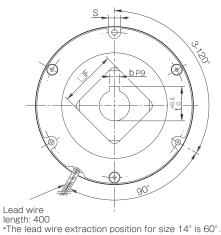
Specifications (BXR- \square -10)

		Static		Coil (at	20°C)		Heat	Max.	Rotating part	Allowable braking	Total	Armature	Armature		
Model	Size	friction torque Ts [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	resistance	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	energy rate Eba & [J]	braking energy E _T [J]	pull-in time ta [s]	release time t _{ar} [s]	Backlash [°]	Mass [kg]
BXR-06-10-005	06	5	24	17.6	0.73	32.7	F	5000	2.35×10^{-5}	500	2.0×10^5	0.050	0.020	1.2	0.9
BXR-08-10-012	08	12	24	19.4	0.81	29.7	F	5000	3.45×10^{-5}	800	2.0×10^{5}	0.080	0.020	1.2	1.2
BXR-10-10-016	10	16	24	21.5	0.90	26.8	F	5000	1.12×10^{-4}	1500	2.2×10^6	0.110	0.050	0.9	1.3
BXR-12-10-030	12	30	24	23.7	0.99	24.3	F	5000	1.88×10^{-4}	1500	2.5×10^6	0.120	0.030	0.8	2.3
BXR-14-10-038	14	38	24	31.0	1.29	18.6	F	3600	4.22×10^{-4}	1800	3.0×10^6	0.120	0.030	0.5	3.0
BXR-16-10-055	16	55	24	19.0	0.79	30.3	F	3600	7.10×10^{-4}	2000	3.0×10^6	0.220	0.100	0.5	3.6

^{*} The armature pull-in time and armature release time are taken during DC switching.

Dimension (BXR- □ -10)





Unit [mm]

Size			Rad	ial direction	on dimens	ions			Axial direction dimentions				Bore diameter				
Size	Α	В	C	D	E	F	R	S	J	L	N	K	a	d	b	t	d max
06	83.5	76	82	47	42	35	4.5	9	17.0	7	14.7	25.0	0.10	20	6	22.5	25
08	93.5	85	92	49	42	35	4.5	10	19.0	7	15.7	27.0	0.10	20	6	22.5	25
10	123.5	115	122	62	55	45	4.5	9.5	14.6	9	13.7	24.3	0.10	24	8	27	28
12	137.5	130	136	65	62	50	4.5	12	15.4	9	12.5	25.0	0.15	24	8	27	30
14	167.5	158	166	80	74	60	5.5	12	16.0	9	12.0	25.0	0.15	28	8	31	38
16	185	175	184	100	86	65	5.5	12.5	21.3	11.5	19.4	32.8	0.20	28	8	31	45

How to Place an Order

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BXR-14-10-038-24V-28DIN Size -Bore diameter (dimensional symbol d) Voltage Static friction torque [N·m] (Refer to the Specifications table for details on the three-digit code.) Shape fitting 10: Square

^{*} Backlash is the value between the rotor and rotor hub.

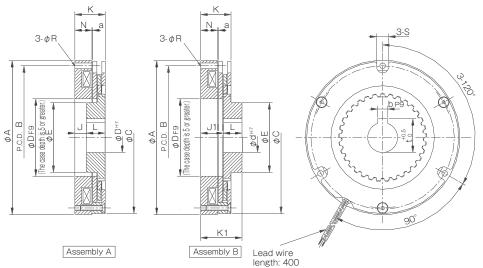
BXR Models Spline Hub Type

Specifications (BXR- \square -20)

	Sta So frict			Coil (at	:20℃)		Heat	Max.	Rotating part	Allowable braking	Total	Armature	Armature		
Model	Size	friction torque Ts [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	resistance	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	energy rate Eba & [J]	braking energy E _T [J]	pull-in time t _a [s]	release time tar [s]	Backlash [°]	Mass [kg]
BXR-06-20-005	06	5	24	17.6	0.73	32.7	F	5000	3.43×10^{-5}	500	2.0×10^5	0.050	0.020	0.5	1.0
BXR-08-20-012	08	12	24	19.4	0.81	29.7	F	5000	6.75 × 10 ⁻⁵	800	2.0×10^{5}	0.080	0.020	0.4	1.3
BXR-10-20-016	10	16	24	21.5	0.90	26.8	F	5000	2.32×10^{-4}	1500	2.2×10^6	0.110	0.050	0.3	1.5
BXR-12-20-030	12	30	24	23.7	0.99	24.3	F	5000	3.02×10^{-4}	1500	2.5×10^{6}	0.120	0.030	0.3	2.5
BXR-14-20-038	14	38	24	31.0	1.29	18.6	F	3600	9.41 × 10 ⁻⁴	1800	3.0×10^6	0.120	0.030	0.2	3.4
BXR-16-20-055	16	55	24	19.0	0.79	30.3	F	3600	15.2 × 10 ⁻⁴	2000	3.0×10^{6}	0.220	0.100	0.2	4.0

^{*} The armature pull-in time and armature release time are taken during DC switching

Dimension (BXR- □ -20)



*The lead wire extraction position for size 14° is 60°.

Unit [mm] Axial direction dimentions Radial direction dimensions Size Α В F R S J1 K1 d max 06 83.5 76 47 36 35 4.5 10.5 18 12.5 14.7 25.0 30.5 0.10 20 22.5 25 08 93.5 85 92 49 42 35 4.5 10 11.5 20 13.5 15.7 27.0 33.5 0.10 20 22.5 30 10 123.5 115 62 45 4.5 9.5 18.2 13.7 24.3 0.10 24 40 12 130 65 61 50 4.5 12 8.8 17.8 12.5 25.0 32.8 0.15 24 45 14 167.5 158 166 75 60 5.5 12 17.2 16 12.0 25.0 33.2 0.15 28 55 175 100 82 65 5.5 12.5 13.6 24.6 18 32.7 42.6 0.20 28 8 65

How to Place an Order



COUPLINGS

EED DUGUUNG

ELECTROMAGNETIC
CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

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POSTA

SERIES

ELECTROMAGN	ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
IETIC-ACTUATED CLUT	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
CHES AND BRAKES	ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BXW

BXR

BXL

BXH

BXL-N

C018

^{*} Backlash is the value between the rotor and rotor hub.

BXR Models

Items Checked for Design Purposes

Precautions for Handling

Brakes

Most electromagnetic braking systems are made using flexible materials. Be careful when handling such parts and materials as striking or dropping them or applying excessive force could cause them to become damaged or deformed.

■ Lead Wires

Be careful not to pull excessively on the brake lead wires, bend them at sharp angles, or allow them to hang too low.

■ Frictional Surface

Since these are dry brakes, they must be used with the frictional surface dry. Keep water and oil off of the frictional surfaces when handling the brakes.

Precautions for Use

■ Environment

These brake units are dry braking systems, meaning that the torque will drop if oil residue, moisture, or other liquids get onto friction surfaces. Attach the protective cover when working in areas with oil, moisture, dust, and other particles that could affect the braking system.

■ Operating Temperature

The operating temperature range is -10 $^{\circ}$ C to 40 $^{\circ}$ C. If you will use the product at other temperatures, consult Miki Pulley.

■ Power Supplies

BXR models use commercial AC 100 V or 200 V single phase, full-wave rectified. Select as appropriate for your application. See the table, "Recommended power supplies and circuit protectors," for the power supply devices we recommend.

■ Power Supply Voltage Fluctuations

Full braking performance may not be guaranteed with extreme changes in power supply voltage. Make sure to keep power supply voltage to within \pm 10% of the rated voltage value.

■ Air Gap Adjustment

BXR models do not require air gap adjustment. The brake air gap is adjusted when the braking system is shipped from the factory.

■ Circuit Protectors

If using a power supply that is not equipped with a circuit protector for DC switching, make sure to connect the recommended circuit protector device in parallel with the brake.

Precautions for Mounting

■ Affixing the Rotor Hub

Affix the rotor hub to the shaft with bolts, snap rings, or the like such that the rotor hub does not touch the armature or stator. Leave at least dimension J on spline hub types, since the rotor hub may contact the armature.

■ Bolts and Screws

Implement screw-locking measures such as use of an adhesive threadlocking compound to bolts and screws used to install brakes.

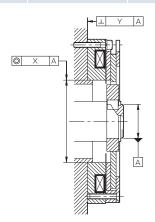
Shafts

The shaft tolerance should be h7 class (JIS B 0401).

■ Accuracy of Brake Attachment Surfaces

Ensure that the concentricity (X) of the centering mark and shaft and the perpendicularity (Y) of the brake mounting surface and shaft do not exceed allowable values.

Size	Concentricity (X)	Perpendicularity (Y)
Size	T.I.R. [mm]	T.I.R. [mm]
06	0.3	0.04
08	0.3	0.05
10	0.4	0.05
12	0.4	0.06
14	0.6	0.06
16	0.6	0.07



Recommended Power Supplies and **Circuit Protectors**

Recommended power supplies

Input AC power	Brake voltage	Rectification method	Brake size	Recommended power supply model
AC100V 50/60Hz	DC24V	Single-phase, full-wave	06,08,10	BES-20-71-1
AC100V 50/60Hz	DC24V	Single-phase, full-wave	12,14,16	BES-20-72-1
AC200V 50/60Hz	DC24V	Single-phase, full-wave	06,08,10	BES-20-71
AC200V 50/60Hz	DC24V	Single-phase, full-wave	12,14,16	BES-20-72

^{*} A DC power supply such as a battery can also be used to supply the 24 V DC required for the brake

Circuit protector

Brake voltage	Included varistors
DC24V	NVD07SCD082 or an equivalent

* NVD \square SCD \square parts are manufactured by KOA Corporation.

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNET	ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
IC-ACTUATED CLUT	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
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SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BXW

BXR BXL

вхн

BXL-N

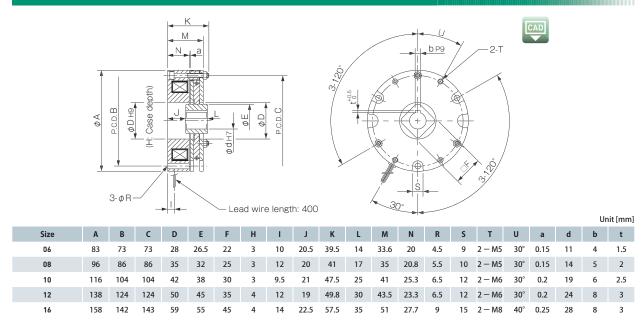
BXL Models

Specifications

		Static		Coil (at	: 20°C)		Heat	Max.	Rotating part	Allowable	Total	Armature	Armature	
Model	Size	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	resistance	rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	braking energy rate Pba ℓ [W]	braking energy Et [J]	pull-in time t _a [s]	release time t _{ar} [s]	Mass [kg]
			DC24	15	0.63	38.4	F							
BXL-06-10	06	2	DC45	12	0.27	169	F	5000	3.75×10^{-5}	58.3	2.0×10^7	0.035	0.020	0.9
			DC90	12	0.13	677	F							
			DC24	23	0.94	25.6	F							
BXL-08-10	08	4	DC45	18	0.41	110	F	5000	6.25×10^{-5}	91.7	3.5×10^{7}	0.040	0.020	1.3
			DC90	18	0.21	440	F							
			DC24	27	1.14	21.1	F							
BXL-10-10	10	8	DC45	25	0.54	83.0	F	4000	13.75×10^{-5}	108.3	6.2×10^{7}	0.050	0.025	2.3
			DC90	25	0.27	331	F							
BXL-12-10	12	16	DC24	35	1.46	16.2	F	3600	33.75 × 10 ⁻⁵	133.3	9.0 × 10 ⁷	0.070	0.030	3.4
DAL-12-10	12	10	DC90	30	0.33	271	F	3000	33.73 × 10 -	133.3	5.0 × 10	0.070	0.030	3.4
BXL-16-10	16	22	DC24	39	1.64	14.6	F	3000	7.35 × 10 ⁻⁴	183.3	11.4 × 10 ⁷	0.100	0.035	5.4
DVF-10-10	10	22	DC90	39	0.43	207	F	3000	7.55 × 10	103.3	11.4 \ 10	0.100	0.033	J. 4

^{*} The armature pull-in time and armature release time are taken during DC switching

Dimensions



How to Place an Order



 $^{^*}$ Contact Miki Pulley for assistance with bore diameters, d, not listed in the Dimensions tales and voltages not listed in the Specifications table.

^{*} See the operating characteristics page for the armature pull-in time and release time during AC-side switching (half-wave rectified).

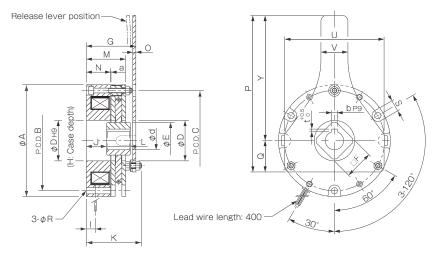
Option

Made to Order

Release Lever

Option No.: 12

In addition to the manual release tap of the standard product, we also offer an optional manual release lever. See the dimensions table below for the dimensions of brakes with release levers. Other specifications are the same as the standard specifications.



																									Uni	t [mm]
Model	Α	В	C	D	E	F	G	Н	1	J	K	L	М	N	0	Р	Q	R	Υ	U	٧	S	a	d	b	t
BXL-06-12	83	73	73	28	26.5	22	42.8	3	10	20.5	49.5	14	33.7	20	2.6	88	24	4.5	64	73	16	9	0.15	11	4	1.5
BXL-08-12	96	86	86	35	32	25	44.4	3	12	20	51	17	35	20.8	2.9	122	27	5.5	95	85	20	10	0.15	14	5	2
BXL-10-12	116	104	104	42	38	30	51.5	3	9.5	21	57.5	25	41	25.3	3.2	162.5	32.5	6.5	130	103	28	12	0.2	19	6	2.5
BXL-12-12	138	124	124	50	45	35	55.7	4	12	19	64.8	30	43.5	23.3	5	200	40	6.5	160	121	36	12	0.2	24	8	3
BXL-16-12	158	142	143	59	55	45	64.2	4	14	22.5	72.5	35	51	27.7	6	230	44	9	186	140	36	15	0.25	28	8	3

Quiet Mechanism (Silencing Spring)

Option No.: S1

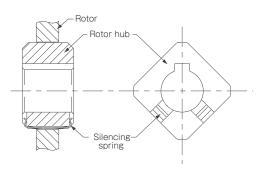
There is a extremely small structural backlash (see figure on the right) between the rotor and the rotor hub. In applications that are prone to microvibrations of the drive shaft such as single-phase motors, this backlash may produce rattling (banging). The silencing spring for the rotor hub reduces this rattling.

Quiet Mechanism (Pull-in Noise Reduction Mechanism)

When the brake is energized, a magnetic circuit is formed, and the armature is pulled to the stator by that magnetic force. At that time, the armature touches the magnetic pole of the stator and a noise is produced. This sound (pull-in noise) is reduced by putting shock absorbing material in the stator's magnetic pole part.

In option S2, in addition to the pull-in noise reduction mechanism, the silencing spring (option S1) is also supplemented.

To download CAD data or product catalogs:



List of Option Numbers

Description of options	No quiet mechanism	Silencing spring	Silencing spring + Pull-in noise reduction mechanism
No release lever	10	10S1	10S2
Has release lever	12	1251	1252

^{*} Option 10 uses standard specifications.

BXL-06-12S1G 24V 11DIN -Option no.

Web code

C019

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

듄	ELECTROMAGNETIC-
ROM	ACTUATED MICRO
AGNET	CLUTCHES & BRAKES
E C	ELECTROMAGNETIC-
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SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BXL вхн BXL-N

MODELS

BXW

BXR

BXL Models

Items Checked for Design Purposes

Precautions for Handling

■ Brakes

Most electromagnetic braking systems are made using flexible materials. Be careful when handling such parts and materials as striking or dropping them or applying excessive force could cause them to become damaged or deformed.

■ Lead Wires

Be careful not to pull excessively on the brake lead wires, bend them at sharp angles, or allow them to hang too low.

I Precautions for Mounting

■ Affixing the Rotor Hub

Affix the rotor hub to the shaft with bolts, snap rings, or the like such that the rotor hub does not touch the armature or stator.

■ Bolts and Screws

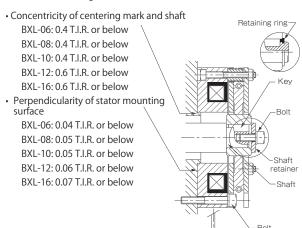
Implement screw-locking measures such as use of an adhesive thread-locking compound to bolts and screws used to install brakes.

■ Shafts

The shaft tolerance should be h6 or js6 class (JIS B 0401).

■ Accuracy of Brake Attachment Surfaces

Ensure that the concentricity of the centering mark and shaft and the perpendicularity of the brake mounting surface and shaft do not exceed the following allowable values.



Precautions for Use

■ Environment

These brake units are dry braking systems, meaning that the torque will drop if oil residue, moisture, or other liquids get onto friction surfaces. Attach the protective cover when working in areas with oil, moisture, dust, and other particles that could affect the braking system.

■ Power Supply Voltage Fluctuations

Full braking performance may not be guaranteed with extreme changes in power supply voltage. Make sure to keep power supply voltage to within \pm 10% of the rated voltage value.

■ Operating Temperature

The operating temperature is -10° C to 40° C (no freezing or condensation). If you will use the product at other temperatures, consult Miki Pulley.

■ Manual Release

BXL models can be released manually.

Alternately tighten screws in two or three of the tap holes on the plate to press the armature.

The screw tips will push against the armature and release it with about a 90° rotation. Do not force the screws in more than that.

■ Air Gap Adjustment

BXL models do not require air gap adjustment. The brake air gap is adjusted when the braking system is shipped from the factory. When first used, no gap adjustment is needed, so do not rotate the nut.

■ Initial Torque

The torque may be lower than the indicated value at initial use. In such cases, run it to break in the frictional surface before use.

■ Circuit Protectors

If using a power supply that is not equipped with a circuit protector for DC switching, make sure to connect the recommended circuit protector device in parallel with the brake.

Recommended Power Supplies and Circuit **Protectors**

Recommended power supplies

Input AC power	Brake voltage	Rectification method	Brake size	Recommended power supply model
AC100V 50/60Hz	DC24V	Single-phase, full-wave	06,08,10	BES-20-71-1
AC100V 50/60Hz	DC24V	Single-phase, full-wave	12,16	BES-20-72-1
AC100V 50/60Hz	DC45V	Single-phase, half-wave	06,08,10	BEW-1R
AC100V 50/60Hz	DC90V	Single-phase, full-wave	06,08,10,12,16	BEW-1R
AC200V 50/60Hz	DC24V	Single-phase, full-wave	06,08,10	BES-20-71
AC200V 50/60Hz	DC24V	Single-phase, full-wave	12,16	BES-20-72
AC200V 50/60Hz	DC90V	Single-phase, half-wave	06,08,10,12,16	BEW-2R
AC200V 50/60Hz	DC90V	Single-phase, half-wave	06,08,10,12,16	BEW-2R

^{*} A DC power supply such as a battery can also be used to supply the 24 V DC required for the brake

Recommended circuit protectors

Input voltage	Brake voltage	Rectification method	Recommended circuit protector (varistor)
DC24V	DC24V	-	NVD07SCD082 or an equivalent
AC100V 50/60Hz	DC45V	Single-phase, half-wave	NVD07SCD220 or an equivalent
AC100V 50/60Hz	DC90V	Single-phase, full-wave	NVD07SCD220 or an equivalent
AC200V 50/60Hz	DC90V	Single-phase, half-wave	NVD07SCD470 or an equivalent

- * NVD \square SCD \square parts are manufactured by KOA Corporation.
- * DC24V indicates a product recommended with a stepdown transformer or the like.

Included varistors

Brake voltage	Included varistors
DC24V	NVD07SCD082 or an equivalent
DC45V	No varistor provided
DC90V	No varistor provided

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

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ELECTROMAGNETIC-
ACTUATED MICRO
CLUTCHES & BRAKES
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ACTUATED
CLUTCHES & BRAKES
ELECTROMAGNETIC
CLUTCH & BRAKE
UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BXW BXR BXL вхн

MODELS

BXL-N

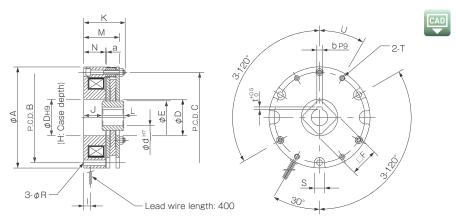
BXH Models

Specifications

		Static		Coil (a	t 20℃)		Heat	Max.	Rotating part	Allowable	Total	Armature	Armature	
Model	Size	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]		rotation speed [min ⁻¹]	moment of inertia J [kg·m²]	braking energy rate Ebaℓ[J]	braking energy Et [J]	pull-in time ta [s]	release time t _{ar} [s]	Mass [kg]
			DC24	15	0.63	38.4	F							
BXH-06-10	06	4	DC45	12	0.27	169	F	5000	3.25×10^{-5}	700	2.0×10^6	0.040	0.020	0.9
			DC90	12	0.13	677	F							
			DC24	23	0.94	25.6	F							
BXH-08-10	08	8	DC45	18	0.41	110	F	F 5000	5.75×10^{-5}	1100	3.5×10^{6}	0.045	0.020	1.3
			DC90	18	0.21	440	F							
			DC24	27	1.14	21.1	F							
BXH-10-10	10	16	DC45	25	0.54	83	F	4000	1.30×10^{-4}	1300	6.2×10^{6}	0.070	0.025	2.3
			DC90	25	0.27	331	F							
BXH-12-10	12	32	DC24	35	1.46	16.2	F	3600	3.20 × 10 ⁻⁴	1600	9.0 × 10 ⁶	0.090	0.025	3.4
BAH-12-10	12	32	DC90	30	0.33	271	F	3000	3.20 × 10	1000	3.0 × 10°	0.090	0.023	J. 4
BXH-16-10	16	44	DC24	39	1.64	14.6	F	3000	6.93 × 10 ⁻⁴	2200	11.4 × 10 ⁶	0.125	0.030	5.4
DATT-10-10	10	44	DC90	39	0.43	207	F	3000	0.93 × 10	2200	11.4 × 10°	0.125	0.030	5.4

^{*} The armature pull-in time and armature release time are taken during DC switching

Dimensions



																				Ur	nit [mm]
Size	Α	В	С	D	E	F	Н	-1	J	K	L	M	N	R	S	T	U	a	d	b	t
06	83	73	73	28	26.5	22	3	10	20.5	39.5	14	33.6	20	4.5	9	2 — M5	30°	0.15	11	4	1.5
08	96	86	86	35	32	25	3	12	20	41	17	35	20.8	5.5	10	2 — M5	30°	0.15	14	5	2
10	116	104	104	42	38	30	3	9.5	21	47.5	25	41	25.3	6.5	12	2 - M6	30°	0.2	19	6	2.5
12	138	124	124	50	45	35	4	2	19	49.8	30	43.5	23.3	6.5	12	2 — M6	30°	0.2	24	8	3
16	158	142	143	59	55	45	4	14	22.5	57.5	35	51	27.7	9	15	2 — M8	40°	0.25	28	8	3

How to Place an Order

BXH-06-10G 24V 11DIN

Size _____ Bore diameter (dimensional symbol d)
Option number _____ Voltage (Specifications table)
10: Standard

*Contact Miki Pulley for assistance with bore diameters, d, not listed in the Dimensions tales and voltages not listed in the Specifications table.

^{*} See the operating characteristics page for the armature pull-in time and release time during AC-side switching (half-wave rectified).

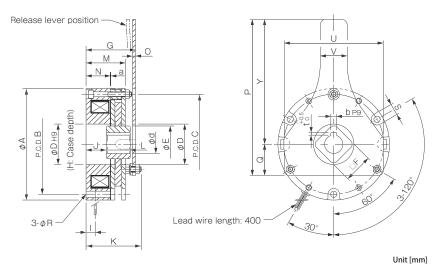
Option

Made to Order

Release Lever

Option No.: 12

In addition to the manual release tap of the standard product, we also offer an optional manual release lever. See the dimensions table below for the dimensions of brakes with release levers. Other specifications are the same as the standard specifications.

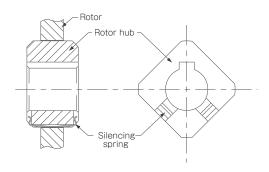


Model	Α	В	C	D	E	F	G	Н	-1	J	K	L	М	N	0	Р	Q	R	Υ	U	٧	S	а	d	b	t
BXH-06-12	83	73	73	28	26.5	22	42.8	3	10	20.5	49.5	14	33.7	20	2.6	88	24	4.5	64	73	16	9	0.15	11	4	1.5
BXH-08-12	96	86	86	35	32	25	45.4	3	12	20	56	17	35.3	20.8	4	122	27	5.5	95	85	20	10	0.2	14	5	2
BXH-10-12	116	104	104	42	38	30	53.9	3	9.5	21	62.5	25	42.2	25.3	4.5	162.5	32.5	6.5	130	103	28	12	0.25	19	6	2.5
BXH-12-12	138	124	124	50	45	35	58.3	4	12	19	69.8	30	45.4	23.3	5	200	40	6.5	160	121	36	12	0.25	24	8	3
BXH-16-12	158	142	143	59	55	45	66.5	4	14	22.5	75.5	35	53.3	27.7	6	230	44	9	186	140	36	15	0.25	28	8	3

Quiet Mechanism (Silencing Spring)

Option No.: S1

There is a extremely small structural backlash (see figure on the right) between the rotor and the rotor hub. In applications that are prone to microvibrations of the drive shaft such as single-phase motors, this backlash may produce rattling (banging). The silencing spring for the rotor hub reduces this rattling.



List of Option Numbers

Description of options	No quiet mechanism	With silencing spring
No release lever	10	10S1
Has release lever	12	1251

^{*} Option 10 uses standard specifications.

BXH-06-12S1G 24V 11DIN

—Option no.

COUPLINGS

ETD BUSHINGS

ELECTROMAGNETIC CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

LINEAD SHAET DDIVE

TOPOLIE I IMITEDS

ROSTA

SERIES

層	ELECTROMAGNETIC-
종	ACTUATED MICRO
AGNET	CLUTCHES & BRAKES
CAC	ELECTROMAGNETIC-
됾	ACTUATED
	CLUTCHES & BRAKES
黑黑	ELECTROMAGNETIC
NO B	CLUTCH & BRAKE
桑	UNITS

SPRING-ACTUATED
BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS							
BXW							
BXR							
BXL							
вхн							
BXL-N							

BXH Models

Items Checked for Design Purposes

Precautions for Handling

■ Brakes

Most electromagnetic braking systems are made using flexible materials. Be careful when handling such parts and materials as striking or dropping them or applying excessive force could cause them to become damaged or deformed.

■ Lead Wires

Be careful not to pull excessively on the brake lead wires, bend them at sharp angles, or allow them to hang too low.

Precautions for Mounting

■ Affixing the Rotor Hub

Affix the rotor hub to the shaft with bolts, snap rings, or the like such that the rotor hub does not touch the armature or stator.

■ Bolts and Screws

Implement screw-locking measures such as use of an adhesive threadlocking compound to bolts and screws used to install brakes.

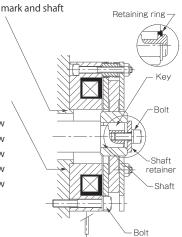
The shaft tolerance should be h6 or js6 class (JIS B 0401).

■ Accuracy of Brake Attachment Surfaces

Ensure that the concentricity of the centering mark and shaft and the perpendicularity of the brake mounting surface and shaft do not exceed the following allowable values.

· Concentricity of centering mark and shaft BXH-06: 0.4 T.I.R. or below BXH-08: 0.4 T.I.R. or below BXH-10: 0.4 T.I.R. or below BXH-12: 0.6 T.I.R. or below BXH-16: 0.6 T.I.R. or below

• Perpendicularity of stator mounting surface BXH-06: 0.04 T.I.R. or below BXH-08: 0.05 T.I.R. or below BXH-10: 0.05 T.I.R. or below BXH-12: 0.06 T.I.R. or below BXH-16: 0.07 T.I.R. or below



Precautions for Use

■ Dedicated for Holding

These brakes are dedicated holding brakes. Do not use them for ordinary braking, except for emergency braking in the event of a power outage or the like.

■ Environment

These brake units are dry braking systems, meaning that the torque will drop if oil residue, moisture, or other liquids get onto friction surfaces. Attach the protective cover when working in areas with oil, moisture, dust, and other particles that could affect the braking system.

■ Power Supply Voltage Fluctuations

Full braking performance may not be guaranteed with extreme changes in power supply voltage. Make sure to keep power supply voltage to within \pm 10% of the rated voltage value.

Operating Temperature

The operating temperature is -10°C to 40°C (no freezing or condensation). If you will use the product at other temperatures, consult Miki Pulley.

■ Manual Release

BXH models can be released manually.

Alternately tighten screws in two or three of the tap holes on the plate to press the armature.

The screw tips will push against the armature and release it with about a 90° rotation. Do not force the screws in more than that.

■ Air Gap Adjustment

BXH models do not require air gap adjustment. The brake air gap is adjusted when the braking system is shipped from the factory. When first used, no gap adjustment is needed, so do not rotate the nut.

■ Circuit Protectors

If using a power supply that is not equipped with a circuit protector for DC switching, make sure to connect the recommended circuit protector device in parallel with the brake.

Recommended Power Supplies and Circuit **Protectors**

Recommended power supplies

Input AC power	Brake voltage	Rectification method	Brake size	Recommended power supply model
AC100V 50/60Hz	DC24V	Single-phase, full-wave	06,08,10	BES-20-71-1
AC100V 50/60Hz	DC24V	Single-phase, full-wave	12,16	BES-20-72-1
AC100V 50/60Hz	DC45V	Single-phase, half-wave	06,08,10	BEW-1R
AC100V 50/60Hz	DC90V	Single-phase, full-wave	06,08,10,12,16	BEW-1R
AC200V 50/60Hz	DC24V	Single-phase, full-wave	06,08,10	BES-20-71
AC200V 50/60Hz	DC24V	Single-phase, full-wave	12,16	BES-20-72
AC200V 50/60Hz	DC90V	Single-phase, half-wave	06,08,10,12,16	BEW-2R
AC200V 50/60Hz	DC90V	Single-phase, half-wave	06,08,10,12,16	BEW-2R

^{*} A DC power supply such as a battery can also be used to supply the 24 V DC required for the brake

Recommended circuit protectors

Input voltage	Brake voltage	Rectification method	Recommended circuit protector (varistor)
DC24V	DC24V	_	NVD07SCD082 or an equivalent
AC100V 50/60Hz	DC45V	Single-phase, half-wave	NVD07SCD220 or an equivalent
AC100V 50/60Hz	DC90V	Single-phase, full-wave	NVD07SCD220 or an equivalent
AC200V 50/60Hz	DC90V	Single-phase, half-wave	NVD07SCD470 or an equivalent

^{*} NVD \square SCD \square parts are manufactured by KOA Corporation.

Included varistors

Brake voltage	Included varistors
DC24V	NVD07SCD082 or an equivalent
DC45V	No varistor provided
DC90V	No varistor provided

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNET	ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
IC-ACTUATED CLUT	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
CHES AND BRAKES	ELECTROMAGNETIC CLUTCH & BRAKE UNITS

BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BXW	
BXR	
BXL	
вхн	

MODELS

BXL-N

^{*} DC24V indicates a product recommended with a stepdown transformer or the like

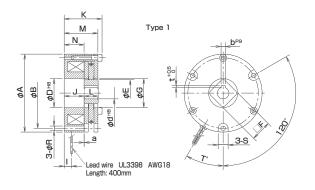
BXL-N Models

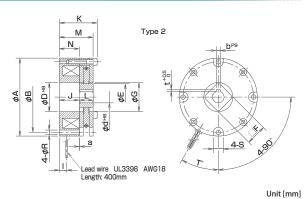
Specifications

		Static		Coil (a	t 20°C)		Heat	Max.	Rotating part	Allowable	Total	Armature	Armature	Applicable	
Model	Size	friction torque T _s [N·m]	Voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]		rotation moment of b speed inertia [min ⁻¹] J [kg • m ²]		braking energy rate Pbal [W]	braking energy Et [J]	pull-in time ta [s]	release time t _{ar} [s]	motor output (Reference) Four poles [kW]	Mass [kg]
			24	19.0	0.793	30.3	F								
BXL-08-10N-002	80	2	99	19.0	0.192	515.8	F	3600	6.3×10^{-5}	60.0	5.0×10^7	0.030	0.050	0.1/0.2	1.4
			171 24	19.0	0.111	1539 30.3	F F								
BXL-08-10N-004	08	4	99	19.0 19.0	0.793	515.8	F	3600	6.3 × 10 ⁻⁵	60.0	5.0×10^{7}	0.040	0.040	0.4	1.4
DAL-00-TOR-004	00	7	171	19.0	0.111	1539	F	3000	0.5 × 10	00.0	3.0 × 10	0.040	0.040	0.4	1.4
			24	28.0	1.166	20.6	F								
BXL-10-10N-008	10	8	99	28.0	0.283	350.0	F	3600	13.8 × 10 ⁻⁵	70.0	8.0×10^{7}	0.050	0.050	0.75	2.7
			171	28.0	0.164	1044	F								
			24	28.0	1.166	20.6	F								
BXL-10-10N-015	10	15	99	28.0	0.283	350.0	F	3600	13.8 × 10 ⁻⁵	70.0	8.0×10^{7}	0.070	0.030	1.5	2.7
			171	28.0	0.164	1044	F								
BXL-12-10N-022	12	22	24 99	35.0 35.0	1.460 0.353	16.4 280.1	F F	3600	33.8 × 10 ⁻⁵	90.0	12.0 × 10 ⁷	0.080	0.060	2.2	4.7
BAL-12-10N-022	12	22	99 171	35.0	0.205	835.5	F	3600	33.8 × 10 °	90.0	12.0 × 10	0.080	0.060	2.2	4.7
			24	35.0	1.460	16.4	F								
BXL-12-10N-030	12	30	99	35.0	0.353	280.1	F	3600	33.8 × 10 ⁻⁵	90.0	12.0 × 10 ⁷	0.100	0.030	3.0	4.7
			171	35.0	0.205	835.5	F								
			24	42.0	1.753	13.7	F								
BXL-16-10N-040	16	40	99	42.0	0.424	233.3	F	1800	73.5×10^{-5}	120.0	16.0×10^{7}	0.100	0.070	3.7	6.3
			171	42.0	0.246	696.1	F								
			24	55.0	2.294	10.5	F								
BXL-16-10N-060	16	60	99 171	55.0 55.0	0.556	178.1 531.6	F F	1800	74.6 × 10 ⁻⁵	150.0	16.0×10^7	0.100	0.050	5.5	6.7
			24	55.0	2.294	10.5	F								
BXL-16-10N-080	16	80	99	55.0	0.556	178.1	F	1800	74.6 × 10 ⁻⁵	150.0	16.0×10^{7}	0.100	0.030	7.5	6.7
			171	55.0	0.322	531.6	F								

^{*}The armature pull-in time and armature release time are taken during DC switching.

Dimensions





Model	Type	Α	В	D	E	F	G	-1	J	K	L	M	N	R	S	T	а	d	b	t
BXL-08-10N-002	1	94	85	35	32	25	35	9	24	45.7	17	40.7	24	5.5	12	30	0.3	11	4	1.5
BXL-08-10N-004	1	94	85	35	32	25	35	9	24	45.7	17	40.7	24	5.5	12	30	0.3	14	5	2
BXL-10-10N-008	1	124	110	40	38	30	42	10	22	48.7	25	42.7	26	6.5	12	30	0.3	18	6	2.5
BXL-10-10N-015	1	124	110	40	38	30	42	10	22	48.7	25	42.7	26	6.5	12	30	0.3	20	6	2.5
BXL-12-10N-022	1	150	130	49	45	35	50	18	25	57.1	30	51.1	29	6.5	14	30	0.3	24	8	3
BXL-12-10N-030	1	150	130	49	45	35	50	18	25	57.1	30	51.1	29	6.5	14	30	0.3	24	8	3
BXL-16-10N-040	1	165	150	62	55	45	62	18	24	63.1	35	55.1	28	9	15	30	0.3	28	8	3
BXL-16-10N-060	2	165	150	64	61	50	64	20	29	68.1	35	60.1	33	9	15	15	0.3	37	10	3.5
BXL-16-10N-080	2	165	150	64	61	50	64	20	29	68.1	35	60.1	33	9	15	15	0.3	37	10	3.5

How to Place an Order

BXL-08-10N-004-24V-11
Size Bore diameter (dimensional symbol d)
Static torque (refer to the specifications table)

^{*} Contact Miki Pulley for assistance with bore diameters, d, not listed in the Dimensions tales and voltages not listed in the Specifications table,

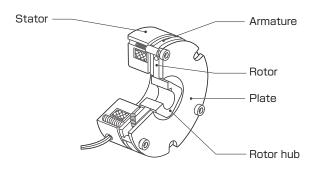
Option

Plate Installation

Standard installation is performed using stator installation, but a plate installation specification is also available as an option. Please contact Miki Pulley for assistance if desiring to use plate installation.

Quiet Mechanism

There is a slight backlash between the rotor and the rotor hub. The armature may also strike the surface of the magnetic poles on the stator when electricity flows, generating a noise. There is a quiet mechanism available that works to suppress such clattering noises as well as operating noise. Please contact Miki Pulley for details.



ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

Items Checked for Design Purposes

Precautions for Handling

■ Brakes

Most electromagnetic braking systems are made using flexible materials. Be careful when handling such parts and materials as striking or dropping them or applying excessive force could cause them to become damaged or deformed.

■ Lead Wires

Be careful not to pull excessively on the brake lead wires, bend them at sharp angles, or allow them to hang too low.

■ Frictional Surface

Since these are dry brakes, they must be used with the frictional surface dry. Keep water and oil off of the frictional surfaces when handling the brakes.

Precautions for Use

Environment

These brake units are dry braking systems, meaning that the torque will drop if oil residue, moisture, or other liquids get onto friction surfaces. Attach the protective cover when working in areas with oil, moisture, dust, and other particles that could affect the braking system.

Operating Temperature

The operating temperature is from 0°C to 40°C (no freezing or condensation). If you will use the product at other temperatures, consult Miki Pulley.

Power Supplies

BXL-N models use commercial AC 220 V or 380 V single phase, half-wave rectified. Select as appropriate for your application.

■ Power Supply Voltage Fluctuations

Full braking performance may not be guaranteed with extreme changes in power supply voltage. Make sure to keep power supply voltage to within \pm 10% of the rated voltage value.

■ Air Gap Adjustment

BXL-N models do not require air gap adjustment. The brake air gap is adjusted when the braking system is shipped from the factory.

■ Circuit Protectors

If using a power supply for separate DC switching, make sure to connect the recommended circuit protector device in parallel with

I Precautions for Mounting

■ Precautions for Mounting

Use a bolt or snap ring to lock the rotor hub onto the shaft.

Shaft

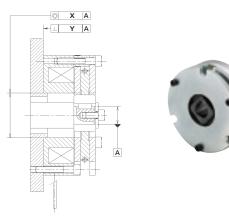
The shaft tolerance should be h7 class (JIS B 0401).

Bolts and Screws

Implement screw-locking measures such as use of an adhesive thread-locking compound to bolts and screws used to install

Accuracy of Brake Attachment Surfaces

Ensure that the concentricity (X) of the centering mark and shaft and the perpendicularity (Y) of the brake mounting surface and shaft do not exceed allowable values.



Allowable concentricity and perpendicularity values for the **BXL-N Models**

Size	Concentricity (X)	Perpendicularity (Y)				
Size	T.I.R. [mm]	T.I.R. [mm]				
08	0.4	0.05				
10	0.4	0.05				
12	0.6	0.05				
16	0.6	0.05				

SERIES

ELECTROMAGNETI	ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
IC-ACTUATED CLUT	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
CHES AND BRAKES	ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

Size	Concentricity (X)	Perpendicularity (Y)						
Size	T.I.R. [mm]	T.I.R. [mm]						
08	0.4	0.05						
10	0.4	0.05						
12	0.6	0.05						
16	0.6	0.05						

Recommended Power Supplies and Circuit **Protectors**

Model	Rectification method	Frequency [Hz]	Input AC voltage [V]	DC output voltage *1 [V]	Recommended circuit protectors *2 (Varistor)
BEM-2T	Single-phase, half-wave	50/60	AC220	DC99	NVD07SCD220 or an equivalent
BEM-4T	Single-phase, half-wave	50/60	AC380	DC171	NVD14SCD820 or an equivalent

^{*1} The values given are for when there is electricity flowing to the brake coil.

MODELS

BXH

BXL-N

^{*2} NVD SCD parts are manufactured by KOA Corporation

Selection Procedure for Brakes for Braking

Consideration of Required Torque to Brake Loads

To select the appropriate brake size, you must find the torque required for braking T, and then select a size of brake that delivers a greater torque than T.

Consideration of cases when load conditions are not clearly known

When load conditions are unclear, assuming that the motor has been selected correctly for the load, the approximate torque can be obtained from the motor output using the following equation.

 Consideration when load conditions can be clearly ascertained

When load conditions can be clearly ascertained, the torque T required for braking can be found using the following equation.

$$T_{M} = \frac{9550 \times P}{n_{r}} \times \eta \quad [N \cdot m] \quad P: \text{ Motor output [kW]} \\ n_{r} \text{ Brake shaft rotation speed [min}^{-1}] \\ \eta : \text{ Transmission efficiency from motor to b}$$

P: Motor output [kW]

 η : Transmission efficiency from motor to brake

J: Total moment of inertia of load side [kg·m²] $T = \left(\frac{J \times n}{9.55 \times t_{ab}} \pm T_{\ell}\right) \times K [N \cdot m]$

n: Rotation speed [min⁻¹] tab: Actual braking time [s]

Tℓ: Load torque [N·m]

Safety factor (see table below)

The sign of load torque $T\ell$ is minus when the load works in the direction that assists braking and plus when it works in the direction that hinders braking. The actual braking time tab is the time required from the start of braking torque generation until braking is complete. When this is not clearly known at the selection stage, a guideline value is used that factors in service life and the like.

Load state	Factor
Low-inertia/low-frequency constant load	1.5
Ordinary use with normal inertia	2
High-inertia/high-frequency load fluctuation	3

Provisional Size Selection

Select a brake of a size for which the torque T found in the equation of step 1 satisfies the following equation.

A brake of a size for which torque T found from the equations above satisfies the following equation must be selected.

Tb > T (or Tm) [N•m] Tb: Brake torque [N•m] * For brake torque, treat Ts as equaling Tb. (Ts: Static friction torque from specifications table)

Consideration of Energy

When the load required for braking is sufficiently small, the size can be selected considering only torque T as described above. Given the effects of heat generated by braking, however, the following equation must be used to confirm that the operation frequency per unit time and the total number of operations (service life) meet the required specifications.

Use the following equation to find the energy Eb required for a single braking operation. $E_b = \frac{J \times n^2}{182} \times \frac{T_b}{T_b \pm T_\ell} \quad [J]$

$$E_b = \frac{J \times n^2}{182} \times \frac{T_b}{T_b \pm T_\ell} \quad [J]$$

The sign of load torque T ℓ is plus when the load works in the direction that assists braking and minus when it works in the direction that hinders braking.

 Confirm the frequency S of operations that can be performed per minute

Find the frequency of operations that can be performed per minute using the equation at right to confirm that the desired operation frequency is sufficiently smaller than the value found.

 $S = \frac{60 \times P_{ba} \ell}{E_b} [times/min]$

 $P_{ba}\ell$: Allowable braking energy rate [W] Eb : Energy required for one braking

Confirm the total number of operations (service life)

Find the total number of operations (service life) using the equation at right, and then check that it meets the desired service life

 $L = \frac{E_T}{F_b} \text{ [times]} \quad \text{Et: Total braking energy [J]}$

Consideration of Braking Time

When there are limits on the time required to decelerate or stop the load, use the equation at right to confirm that the total braking time ttb satisfies requirements.

Here, actual braking time tab is the time from the start of braking torque generation to the completion of braking. Find it with the following equation.

$$t_{tb} = t_{id} + t_{ar} + t_{ab} \qquad \text{tar: Armature release time [s]} \\ t_{id: Initial delay time [s]}$$

$$t_{ab} = \frac{J \times n}{9.55 \times (T_b \pm T_\ell)} [s]$$

The sign of load torque T ℓ is plus when the load works in the direction that assists braking and minus when it works in the direction that hinders braking.

Consideration of Stopping Precision

To confirm stopping precision, find the stopping angle (rotation) using the following equation.

The variation in stopping precision--i.e., stopping precision $\Delta \theta$ --can be found empirically with the following equation and used as a guide.

$$\theta = 6 \times n \times \left(t_{id} + t_{ar} + \frac{1}{2} t_{ab}\right) [\circ]$$
 tar: All tars All

tar: Armature release time [s] tid: Initial delay time [s]

 $\Delta\theta = \pm 0.15 \times \theta$ [°]

Selection Procedure for Brakes for Holding

Consideration of Required Torque to Hold Loads

Use the following equation to find the torque T required to hold a load while stationary.

T=T ℓ max \times K [N•m] T ℓ max: Max. load torque [N·m] K: Safety factor (see table at right)	Load state	Factor
	Low inertia/small load fluctuations	1.5
	Ordinary use with normal inertia	2
	High inertia/large load fluctuations	3

Provisional Selection of Size

A brake of a size for which torque T found from the equations above satisfies the following equation must be selected.

 $T_s > T [N \cdot m]$ Ts: Static friction torque of brake [N•m]

Consideration of Energy

When considering a brake with the objective of holding loads, braking is limited to emergency braking.

Use the following equation to find the braking energy Eb for a single operation required for emergency braking. You must confirm that this result is sufficiently smaller than the allowable braking energy $\mathsf{Eba}\,\ell$ of the selected brake.

$$E_b = \frac{J \times n^2}{182} \times \frac{T_b}{T_b \pm T\ell} \quad [J] \quad \begin{array}{l} \text{J:} \qquad \text{Total moment of inertia on load side [kg·m²]} \\ \text{n:} \qquad \text{Rotation speed [min⁻¹]} \\ \text{Brake torque [N·m]} \\ \text{T}_\ell \quad \text{max.} \quad \text{Max. load torque [N·m]} \end{array}$$

The sign of maximum load torque $T\ell$ max is plus when the load works in the direction that assists braking and minus when it works in the direction that hinders braking.

$$E_b \ll E_{ba} \, \ell \ [J]$$

When using brakes for both holding and braking and the specification is indicated by allowable braking energy rate $P_{ba}\ell$, check under the following conditions.

 $E_b \ll 60 \times P_{ba} \ell$ [J]

Consideration of Number of Operations

The total number of braking operations (service life) when performing emergency braking L must be found using the following equation to confirm that required specifications are satisfied.

$$L = \frac{E_T}{E_b} \text{ [times]} \quad \text{Et: Total braking energy [J]}$$

Note that the frequency of emergency braking will also vary with operating environment; however, it should be about once per minute or better. When the braking energy of a single operation \acute{E}_b is 70% or more of the allowable braking energy $E_{ba} \ell$, however, allow the brake to cool sufficiently after emergency braking before resuming use.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** FI FCTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BXW BXR BXL

BXL-N

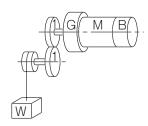
BXH

MODELS

BXW/BXR/BXL/BXH Models

Selection Example 1

Braking Brakes Used in Raising Loads



Selection of a brake to brake the load is as follows, as the above figure illustrates.

Motor (brake shaft) rotation speed	n	1800 [min ⁻¹]
Load shaft rotation speed	n1	60 [min ⁻¹]
Moment of inertia of motor-side gear	J ₁	$1.5 \times 10^{-2} [kg \cdot m^2]$
Moment of inertia of load-side gear	J_2	$1.5 \times 10^{-2} [kg \cdot m^2]$
Moment of inertia of load-side drum	J ₃	4.30 [kg·m²]
Moment of inertia of motor with speed reducer	Jm	$6 \times 10^{-3} [kg \cdot m^2]$
Moment of inertia of load	JA	15.67 [kg·m²]
Load-side torque	T	62.5 [N•m]
Number of braking operations of brake	L	53,000 cycles or more
Brake operating frequency	S	0.1 [cycles/min]

 $^{^{}st}$ The number of braking operations and operation frequency treat one ascending operation and one descending operation together as one cycle

■ Consideration of Torque

The torque required for braking is calculated from the above specifications, compared to the dynamic friction torque in the catalog, and the appropriate brake size is selected.

• Calculating the inertial moment converted to brake shaft inertial moment J_B

We use the following equation to calculate the moment of inertia converted to the brake shaft (motor shaft) moment of inertia JB[kg·m²]. Here, R represents the ratio of the motor rotation speed to the load shaft rotation speed.

$$\begin{split} J_B = &J_M + (J_1 + J_2 + J_3 + J_A) &\times R^2 \ [kg \cdot m^2] \\ J_B = &6 \times 10^{-3} + (1.5 \times 10^{-2} + 1.5 \times 10^{-2} + 4.30 + 15.67) \\ &\times (60/1800)^2 \\ &\stackrel{.}{\Rightarrow} 2.8 \times 10^{-2} [kg \cdot m^2] \end{split}$$

ullet Calculating the load torque converted to brake shaft load torque $T\ell$ We use the following equation to calculate the load torque converted to the brake shaft (motor shaft) load torque T_{\ell} [N•m]. However, η indicates the transmission efficiency, which is 0.85 in this selection.

$T_{\ell}=R\times T/\eta [N\cdot m]$ $T_{\ell} = 60/1800 \times 62.5/0.85 = 2.45 \text{ [N·m]}$

· Calculating the torque required for braking T Use the following equation to calculate the torque required for braking T [N·m].

Here, the conditions are set as follows.

- * The guideline for actual braking time t_{ab} is 2.0 [s].
- * The sign of load torque TR is minus when ascending because the load works in the direction that assists braking and plus when descending because the load works in the direction that hinders
- braking.

 * Select a safety factor K of 3.0, based on operating conditions.

Ascending

$$\begin{split} & T_{\text{up}} = \left(\frac{J_{\text{B}} \times n}{9.55 \times t_{\text{ab}}} - T_{\ell}\right) \times \text{K} \\ & T_{\text{up}} = \left(\frac{2.8 \times 10^{-2} \times 1800}{9.55 \times 2.0} - 2.45\right) \times 3.0 & \stackrel{.}{=} 0.57 \left[\text{N} \cdot \text{m}\right] \end{split}$$

Descendina

$$\begin{split} T_{\text{DOWN}} &= \left(\frac{J_{\text{B}} \times n}{9.55 \times t_{\text{ab}}} + T_{\ell}\right) \times K \\ T_{\text{DOWN}} &= \left(\frac{2.8 \times 10^{-2} \times 1800}{9.55 \times 2.0} + 2.45\right) \times 3.0 \\ &\stackrel{\Leftarrow}{=} 15.3 \left[\text{N} \cdot \text{m}\right] \end{split}$$

Since the result of the above shows that required torque is 15.3 [N·m], check the specifications in the catalog and select size 12 (dynamic friction torque of 16.0 [N•m]) of the BXL models of brakes for braking.

^{*} The number of braking operations of the brake is treated as 6 (operations/h) $\, imes\,$ 8 (h/day) $\, imes\,$ 365 $(days/year) \times 3 (years).$

■ Consideration of Energy

Confirm that the brake selected based on required torque satisfies the required specifications for number of braking operations and braking frequency.

 \bullet Calculating the total moment of inertia ${\sf J}$

Adding the inertial moment converted to brake shaft inertial moment J_B that was just calculated to the inertial moment of the rotating parts of the provisionally selected BXL-12 (catalog value of 33.75×10^{-5}), we arrive at the total moment of inertia.

$$J = 2.8 \times 10^{-2} + 33.75 \times 10^{-5}$$

$$= 2.83 \times 10^{-2} [\text{kg} \cdot \text{m}^2]$$

• Calculating the amount of energy required for one braking operation Eb The calculated total moment of inertia is used to calculate the energy required by a single braking operation. Here, the sign of load torque $T\ell$ is plus when ascending because the load works in the direction that assists braking and minus when descending because the load works in the direction that hinders braking.

Ascending

Descending

$$\begin{split} E_{\text{bDOWN}} &= \frac{J \times n^2}{182} \times \frac{T_b}{T_b - T_{\ell}} \\ E_{\text{bDOWN}} &= \frac{2.83 \times 10^{-2} \times 1800^2}{182} \times \frac{16.0}{16.0 - 2.45} \\ &\doteq 595 \text{ [J]} \end{split}$$

 Confirm the frequency S of operations that can be performed per minute

Substitute the energy required for a single braking E_b calculated above and the allowable braking energy rate $P_{ba\,\ell}$ for the BXL-12 (catalog value 133.3 W) into the following equation and calculate the frequency S of operations that can be performed per minute.

Ascending

$$\begin{split} S_{up} &= \frac{60 \times P_{ba} \, \ell}{E_{bup}} \\ S_{up} &= \frac{60 \times 133.3}{437} \\ &\doteq 18.3 \, [times/min.] \end{split}$$

Descending

$$S_{DOWN} = \frac{60 \times P_{ba} \ell}{E_{bDOWN}}$$

$$S_{DOWN} = \frac{60 \times 133.3}{595}$$

$$= 13.4 \text{ [times/min.]}$$

The desired operation frequency is sufficiently smaller than the calculated operation frequency, so the specification is satisfied. Note that the braking energy rate (catalog value) used in the calculation is the value under ideal conditions, so the desired operation frequency needs to be sufficiently small.

13.4 [times/min.] ≫ 0.1 [times/min.]

• Calculating the total number of operations (service life) Substituting in the just-calculated energy required for a single braking Eb and the BXL-12 total frictional energy ET (catalog value of 9.0×10^7 [J]), we arrive at the total number of operations L.

If the energy of a single cycle of ascending and descending Eb is:

$$E_b = E_{bup} + E_{bDOWN}$$

$$E_b = 1032 [J]$$

The total number of operations L is:

$$L = \frac{E_T}{E_b}$$

$$L = \frac{9.0 \times 10^7}{1032}$$

$$\rightleftharpoons 87209 \text{ [cycles]}$$

The desired total number of operations is fewer than the calculated total number of operations (service life), so the specification is satisfied.

87,209 [cycles] > 53,000 [cycles]

■ Consideration of Braking Time

Total braking time t_{tb} is calculated as the sum of actual braking time t_{ab} , armature release time t_{ar} , and the initial delay time from start of command input to start of operating input t_{id} .

Here, the actual braking time is expected to be greater in the descending direction, so only the case of descending is considered. The sign of the load torque $T\ell$ is minus, since it is in the direction that impedes braking.

$$\begin{split} t_{ab} &= \frac{J \times n}{9.55 \times (T_b - T_\ell)} \\ t_{ab} &= \frac{2.83 \times 10^{-2} \times 1800}{9.55 \times (16.0 - 2.45)} \\ & = 0.39[s] \end{split}$$

Here, the armature release time t_{ar} of the BXL-12 from the catalog is 0.03 [s]. The initial delay time t_{td} is the delay of the operation of relays and the like, so we use 0.025 [s], the typical relay operation time. Thus, the total braking time t_{tb} is:

$$t_{tb}=0.025+0.030+0.39$$

 $\approx 0.445 [s]$

■ Consideration of Stopping Precision

When stopping precision (stopping distance) is restricted, calculate stopping precision using the following equations.

$$\theta = 6 \times n \times (t_{id} + t_{ar} + 1/2 \times t_{ab})$$
$$= 2700[^{\circ}]$$

The variation in stopping precision--i.e., stopping precision $\Delta \theta$ --can be found empirically with the following equation and used as a quide.

$$\triangle \theta = \pm 0.15 \times \theta$$

= ± 405 [°]

This angle is the angle at the brake shaft, so when the stopping precision θ max is 2700 + 405 = 3105 [°] and the drum diameter Dd is 0.5 [m], the braking distance Bd of load W is:

$$B_d = \theta \max/360 \times R \times \pi \times D_d$$

= (3105/360) × (60/1800) × π × 0.5
=0.45[m]

If there is no problem with the braking time and stopping precision, BXL-12 can be selected.

COLIDI INGS

ETP BUSHINGS

ELECTROMAGNETIC CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

LINEAR SHAFT DRIVES

TOROLIE LIMITERS

ROSTA

SERIES

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ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BXL-N

BXW

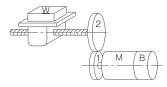
BXR

BXL

BXW/BXR/BXL/BXH Models

Selection Example 2

I Holding Brakes Used in Ball Screw Drive of Loads



Selection of a brake to brake the load is as follows, as the above figure illustrates.

Motor (brake shaft) rotation speed	n	1800 [min ⁻¹]
Load shaft rotation speed	nı	900 [min ⁻¹]
Moment of inertia of motor	JM	0.001 [kg·m²]
Mass of load	М	500 [kg]
Lead of feed screw	Р	0.01 [m]
Shaft diameter of feed screw	D	0.05 [m]
Length of feed screw	1	1 [m]
Friction coefficient of feed screw	μ	0.2

■ Consideration of Torque

The torque required for holding is calculated from the specifications at left, compared to the static friction torque in the catalog, and the appropriate brake size is selected.

• Calculating load torque converted to brake shaft load torque $T\ell$ Use the following equation to calculate the load torque $T\ell$ [N•m]. Here, there is no external force F [N•m], gravitational acceleration g $[m/s^2]$ is 9.8 $[m/s^2]$, R is the ratio of motor rotation speed to load shaft rotation speed, and η is transmission efficiency, which in this selection is 0.85.

 $T_{\ell} = R \times 1/2\pi \times P \times (F + \mu M_g)/\eta [N \cdot m]$ $T_{\ell} = (900/1800) \times 1/2\pi \times 0.01 \times (0 + 0.2 \times 500 \times 9.8)/0.85$ ≒0.92[N·m]

• Calculating the required holding torque T Use the following equation to calculate the required holding torque T. Here, safety factor K is 2.

 $T=T_{\ell}\times K[N\cdot m]$ $T=0.92\times2$

≒1.84[N·m]

Since the result of the above shows that required torque is 1.84 [N•m], check the specifications in the catalog and select size 06 (static friction torque of 4.0 [N·m]) of the BXH models of brakes for holding.

■ Consideration of Energy During Emergency Braking

Brakes selected based on required holding torque are designed primarily for holding, so their braking operations are limited to emergency braking and the like. It is therefore necessary to check that the braking energy per braking operation Eb during emergency braking does not exceed the allowable braking energy $\mathsf{Eba}\,\ell$.

· Calculating the moment of inertia of feed screws Given a feed screw whose shaft has a length of 1 [m], diameter of 0.05 [m], and specific gravity of 7.8, the feed screw moment of inertia Ja [kg•m²] is:

$$J_{A} = \frac{1}{8} \times M \times D^{2}$$

$$= \frac{1}{8} \times (0.025^{2} \times \pi \times 1 \times 7.8 \times 1000) \times 0.05^{2}$$

· Calculating the moment of inertia of a linearly moving object Use the following equation to calculate the moment of inertia Jx [kg·m²] of a linearly moving object.

$$J_{X}=J_{A}+\frac{M \cdot P^{2}}{4 \pi^{2}}$$

$$=0.0048+\frac{500 \times 0.01^{2}}{4 \times \pi^{2}}$$

$$=6.1 \times 10^{-3} [kg \cdot m^{2}]$$

· Calculating the total inertial moment converted to brake shaft inertial moment

The moment of inertia Jx [kg·m²] of a linearly moving object found above is added to the moment of inertia of the rotating parts of the provisionally selected BXH-06 (catalog value of 3.25 imes 10 $^{-5}$ kg•m²) and the motor's moment of inertia Jм [kg•m²] to calculate the total moment of inertia. Here, R represents the ratio of the motor rotation speed to the load shaft rotation speed.

$$\begin{split} J &= J_x \times R^2 + J_M + J_B [kg \cdot m^2] \\ &= 6.1 \times 10^{-3} \times \ \left(\frac{1}{2}\right)^2 + 0.001 + 3.25 \times 10^{-5} \\ &= 2.56 \times 10^{-3} [kg \cdot m^2] \end{split}$$

· Consideration of energy

We calculate the braking energy per braking Eb required for emergency braking using the following equation. Here, the brake torque Tb [N•m] is the catalog value of 4.0 [N•m] and the sign of the load torque $T\ell$ is plus, since it works in the direction that assists

$$\begin{split} E_{b} &= \frac{J \cdot n^{2}}{182} \times \frac{T_{b}}{T_{b} + T_{\ell}} \\ E_{b} &= \frac{2.56 \times 10^{-3} \times 1800^{2}}{182} + \frac{4.0}{4.0 + 0.92} \\ &= 37.1[J] \end{split}$$

Since the calculated braking energy Eb does not exceed the BXH-06's allowable braking energy Ebal (catalog value of 700 [J]), the specification is satisfied.

37.1 [J] < 700 [J]

■ Consideration of Number of Operations

The total number of braking operations (service life) L when doing emergency braking can be found using the following equation. Here, the BXH-06's total braking energy E_{T} is the catalog value of 2.0 \times 10⁶ [J].

$$L = \frac{E_T}{E_b}$$

$$L = \frac{2.0 \times 10^6}{37.1}$$

≒ 53908 [times]

With these specifications, BXH-06 can be selected.

Note that the frequency of emergency braking has a major impact on service life, so it should be about once per minute or better.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

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ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BXW

BXR BXL

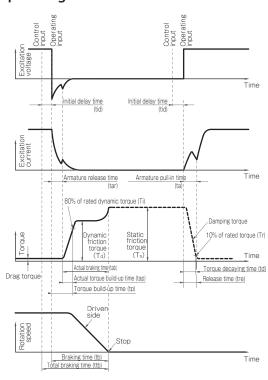
RXH

BXL-N

BXW/BXR/BXL/BXH Models

Operating Characteristics

Operating Time



tar: Armature release time

The time from when current shuts off until the armature returns to its position prior to being pulled in and torque begins to be generated

tap: Actual torque build-up time

The time from when torque first begins to be generated until it reaches 80% of rated torque

tp: Torque build-up time

The time from when current flow is shut off until torque reaches 80% of rated torque

ta: Armature pull-in time

The time from when current flow first starts until the armature is pulled in and torque disappears

tid: Initial delay time

The time from start of command input to actuation input or release input to the main brake body

BXW Models

Unit [s]

Туре	Voltage	Size	Switching	tar	ta
	12V	01		0.015	0.008
	24V	02		0.015	0.008
L type (Braking use)	45V	03	DC side	0.025	0.025
(Di akilig use)	90V	04		0.030	0.030
	180V	05		0.035	0.035
	12V	01		0.010	0.010
H type	24V	02	DC side	0.010	0.010
(Holding and	45V	03		0.020	0.035
braking use)	90V	04		0.025	0.040
	180V	05		0.030	0.045
		01		0.010	0.025
٠.		02		0.010	0.030
S type (Holding use)	24V	03	DC side	0.020	0.035
(Hotaling use)		04		0.025	0.040
		05		0.030	0.045
R type		01		0.020	0.035
(For servo	24V	03		0.020	0.050
motors)		05		0.020	0.060

BXR LE Models (Holding use)

- 1	In	iŧ	ſσ

Voltage	Size	Switching	tar	ta
	01		0.020	0.035
24V	02	DC side	0.020	0.050
	03		0.020	0.060

BXR Models (Holding use)

Unit [s]

Voltage	Size	Switching	tar	t _a
	06	06 08 10 12 14	0.02	0.05
	08		0.02	0.08
24V	10		0.05	0.11
244	12		0.03	0.12
	14		0.03	0.12
	16	0.10	0.22	

BXL Models (Braking use)

Unit [s]

Voltage	Size	Switching	t ar	tap	t _p	ta
	06		0.020	0.015	0.035	0.035
24V	08		0.020	0.015	0.035	0.040
45V	10	DC side	0.025	0.020	0.045	0.050
90V	12		0.030	0.025	0.055	0.070
	16		0.035	0.030	0.065	0.100
	06		0.110	0.035	0.145	0.035
(5)(08		0.110	0.040	0.150	0.040
45V 90V	10	AC side	0.150	0.060	0.210	0.050
701	12		0.180	0.095	0.275	0.070
	16		0.180	0.100	0.280	0.100

BXH Models (Holding use)

Unit [s]

Voltage	Size	Switching	tar	ta
	06		0.020	0.040
24V	08		0.020	0.045
45V	10	DC side	0.025	0.070
90V	12		0.025	0.090
	16		0.030	0.125
	06		0.070	0.040
(5)(08		0.080	0.045
45V 90V	10	AC side	0.090	0.070
701	12		0.120	0.090
	16		0.140	0.125

BXL-N Models (Braking use)

Unit [s]

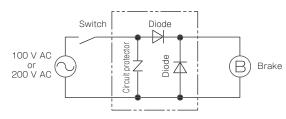
				[-]
Voltage	Size	Switching	tar	t a
	08-10N-002		0.050	0.030
	08-10N-004		0.040	0.040
	10-10N-008 10-10N-015		0.050	0.050
24V			0.030	0.070
99V	12-10N-022	DC side	0.060	0.080
171V	12-10N-030		0.030	0.100
	16-10N-040		0.070	0.100
	16-10N-060		0.050	0.100
	16-10N-080		0.030	0.100

Control Circuits

45 V, 90 V, and 96 V Specifications for BXW, BXR, BXL, and BXH Models (Single-phase Half-wave Rectified)

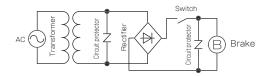
■ AC-side Switching

This is the usual switching method. Connection is simple.



1 12 V and 24 V Specifications for BXW, BXR, BXL, and BXH Models (Single-phase Full-wave Rectified)

■ DC-side Switching



■ Circuit Protectors

If using a power supply that is not equipped with a circuit protector for DC switching, make sure to connect the recommended circuit protector device in parallel with the brake. However, with some circuit protectors, operation times may lengthen. In such cases, we recommend use of varistors.

Select varistors from the following table based on brake size and AC voltage before rectification.

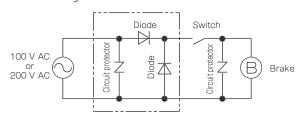
Note that the 24 V specifications of BXL and BXH as well as all BXR models are supplied with varistors. See Included varistors for each model.

Pre-rectification voltage [V]	Recommended varistor model
AC 30 or below	NVD07SCD082 or an equivalent
Over AC 30 to AC 110 or below	NVD07SCD220 or an equivalent
Over AC 110 to AC 220 or below	NVD07SCD470 or an equivalent
Over AC 220 to AC 460 or below	NVD14SCD820 or an equivalent
AC 30 or below	NVD14SCD082 or an equivalent
Over AC 30 to AC 110 or below	NVD14SCD220 or an equivalent
Over AC 110 to AC 220 or below	NVD14SCD470 or an equivalent
Over AC 220 to AC 460 or below	NVD14SCD820 or an equivalent
	[V] AC 30 or below Over AC 30 to AC 110 or below Over AC 110 to AC 220 or below Over AC 220 to AC 460 or below AC 30 or below Over AC 30 to AC 110 or below Over AC 30 to AC 220 or below

^{*} NVD \square SCD \square parts are manufactured by KOA Corporation.

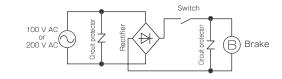
■ DC-side Switching

This method achieves even faster operational characteristics than AC-side switching.



90 V, 96 V, 180 V, and 190 V Specifications for BXW Models (Single-phase Full-wave Rectified)

■ DC-side Switching



COUPLINGS

ETD BLISHING

ELECTROMAGNETIC CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

LINEAR SHAFT DRIVES

TOPOLIE LIMITERS

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SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

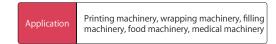
BRAKE MOTORS

POWER SUPPLIES

MODELS

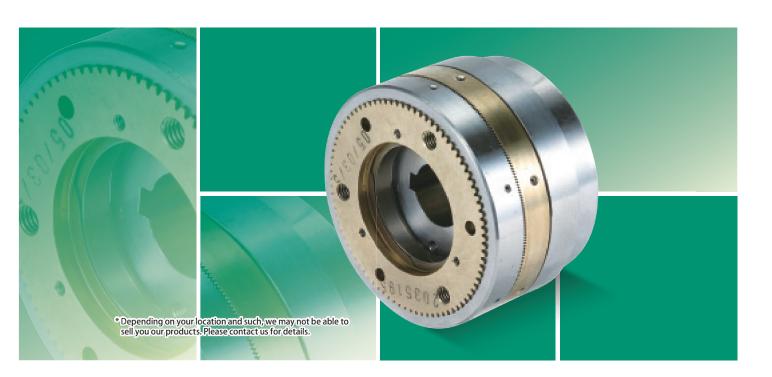
BXW		
BXR	 	
BXL		
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BXL-N		

ELECTROMAGNETIC TOOTH CLUTCHES



Meshing-type Electromagnetic-actuated Clutch Has High Torque and Reliable Transmission

These electromagnetic tooth clutches are electromagnetic-actuated clutches of the type that transmit torque by engaging tooth. Since torque is transmitted by engaging tooth, these clutches can transmit very high torque with a compact size (five to ten times our dry-type single discs). They may be either full position, which engage everywhere around their circumference, or single position, which engage at a set position, engaging in only one location per revolution. The shape of the tooth tip may be either symmetrical or sawtooth. Symmetrical tips can be used in any rotation direction, while sawtooth tips are faster than symmetrical tips and can engage at higher speeds.



Compact, high torque

Since torque is transmitted by the meshing of the tooth, high torque transmission can be achieved with a compact form factor.

No drag torque

Since the tooth do not form a magnetic circuit, engagement and release can be faster, and there is no drag torque.

Easy mounting

Bearings are built in, so there is no centering of stator and rotor.

I Can be used in oily environments

Can be used in oily environments under some usage conditions.

Special position engagement

Special tooth shapes can be made that mesh at multiple locations.

Available Models Lineup 546- -34-NF TOOTH CLUTCHES Full-depth tooth **Full** position 546- -34-NS Single position Sawtooth (right rotation) 546- -34-RF **Full position** 546- -34-RS Single position Sawtooth (left 546- - -34-LF **Full** position rotation) 546- - -34-LS Single position

Tooth Shape/Construction

I Full-depth Tooth

By far the most common tooth shape, it can be used rotating in either direction.

Sawtooth

These have fewer tooth that the full-depth tooth type, and have a smaller angle of mesh insertion. They can thus engage at a relatively higher speed than full-depth tooth.

I Full Position

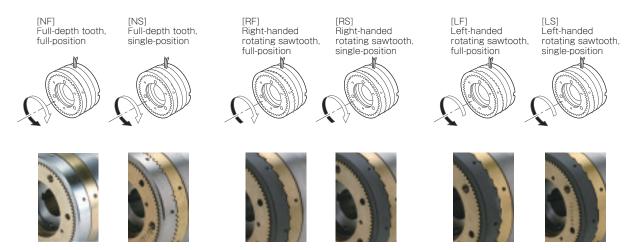
A common tooth shape that can mesh anywhere around the full circumference.

Single Position

This tooth shape is for fixed position engagement, where only one location meshes per revolution.

Name of tooth shape	NF	NS	RF	RS	LF	LS
Type of tooth shape	Full-depth tooth	Full-depth tooth	Sawtooth	Sawtooth	Sawtooth	Sawtooth
Position	Full	Single	Full	Single	Full	Single
Rotational direction	Both	Both	Right	Right	Left	Left

^{*} The reference point for rotation direction (rotor) is the direction as seen from the adapter plate. With armature input, the rotation direction is as stated. Note that with shaft input, the direction is the opposite. Example: To get right rotation at shaft input, use a left-rotating sawtooth (L).



ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** FI FCTROMAGNETIC-ACTUATED **CLUTCHES & BRAKES** ELECTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

546

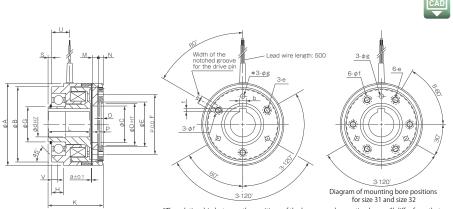
546 Models

Specifications

Model	Size	Torque		Coil (at 2	20℃)		Heat resis class		able ro of enga [min = 1]	gement	Max. rotation	Moment J [kg	of inertia J·m²]		ber of eth	Armature pull-in time	Armature release	Mass
Model	ze	[N·m]	Exciting voltage [V]	Wattage [W]	Current [A]	Resistance [Ω]	: resistance class	NF	NS	Sawtooth	speed [min ⁻¹]	Rotor	Armature	Full-depth tooth, Full	Sawtooth, Full	ta [s]	time t _{ar} [s]	[kg]
546-12-34	12	17.5	DC24	13.3	0.55	44.0	F	50	30	100	1500	6.6×10^{-5}	6.0×10^{-5}	200	25	0.035	0.040	0.5
546-13-34	13	25	DC24	18.7	0.78	31.0	F	50	30	100	1500	1.5×10^{-4}	1.2×10^{-4}	220	30	0.040	0.050	0.9
546-15-34	15	50	DC24	21.3	0.89	27.1	F	50	30	100	1500	3.7×10^{-4}	3.7×10^{-4}	260	36	0.060	0.060	1.5
546-21-34	21	100	DC24	27.0	1.13	21.0	F	50	30	100	1500	8.7×10^{-4}	5.2×10^{-4}	290	36	0.080	0.070	2.4
546-23-34	23	250	DC24	36.2	1.51	15.9	F	50	30	100	1500	2.06×10^{-3}	1.85×10^{-3}	280	38	0.090	0.080	3.9
546-25-34	25	500	DC24	56.6	2.36	10.2	F	50	30	100	1500	4.88×10^{-3}	4.51×10^{-3}	250	40	0.100	0.090	6.8
546-31-34	31	1000	DC24	79.7	3.32	7.2	F	50	30	100	1500	1.12×10^{-2}	1.28×10^{-2}	195	40	0.110	0.110	11.1
546-32-34	32	2200	DC24	114.0	4.75	5.1	F	50	30	100	1500	2.87×10^{-2}	2.92×10^{-2}	186	40	0.120	0.130	15.3

^{*} The armature pull-in and release times are reference values under no load in a stationary state. They are generally longer depending on the size of the load and the operating state when engaged.

Dimensions



^{*}The relationship between the positions of the keyway and mounting bore will differ from that shown in the diagram while the parts are fitted together.

				Un	it [mm]		
	Shaft bore dimensions						
Size	d н7	Models compl the new JIS st	Models compl the old JIS st	iant with andards			
	u 117	b P9	t + 0.5	b E9	t + 0.5		
12	10	$3 \begin{array}{l} -0.006 \\ -0.031 \end{array}$	1.2	$4 \ ^{+ \ 0.05}_{+ \ 0.02}$	1.5		
13	15	5 -0.012 -0.042	2	5 ^{+ 0.05} + 0.02	2		
15	20	$6 {}^{- 0.012}_{- 0.042}$	2.5	5 ^{+ 0.05} + 0.02	2		
13	25	$8 {}^{- 0.015}_{- 0.051}$	3	$7 \ ^{+ 0.061}_{+ 0.025}$	3		
21	25	8 - 0.015 - 0.051	3	7 ^{+ 0.061} + 0.025	3		
21	30	8 - 0.015 - 0.051	3	7 ^{+ 0.061} + 0.025	3		
23	30	$8 {}^{- 0.015}_{- 0.051}$	3	$7 {}^{+ 0.061}_{+ 0.025}$	3		
23	40	$12 {}^{- 0.018}_{- 0.061}$	3	$10 {}^{+ 0.061}_{+ 0.025}$	3.5		
25	40	$12 {}^{- 0.018}_{- 0.061}$	3	$10 {}^{+ 0.061}_{+ 0.025}$	3.5		
25	50	14 - 0.018 14 - 0.061	3.5	$12 {}^{+ 0.075}_{+ 0.032}$	3.5		
31	50	$14 {}^{- 0.018}_{- 0.061}$	3.5	$12 {}^{+ 0.075}_{+ 0.032}$	3.5		
31	60	$18 {}^{- 0.018}_{- 0.061}$	4	$15 {}^{+ 0.075}_{+ 0.032}$	5		
32	60	$18 {}^{- 0.018}_{- 0.061}$	4	$15 {}^{+ 0.075}_{+ 0.032}$	5		
32	70	$20 \ ^{- 0.022}_{- 0.074}$	4.5	$18 {}^{+ 0.075}_{+ 0.032}$	6		

Model	Radial direction dimensions					Axial direction dimensions																
Wodei	Α	В	C	D	E	F	G	е	f	g	Н	K	L	М	N	0	Р	S	U	V	W	a
546-12-34	57	52	22.5	26	27.2	36	20	M4	8.5	-	10	43	34	4.3	3.1	1.3	1.3	2.0	15	4.5	5	0.2
546-13-34	67	58	31	32	33.7	46	25	M5	8.5	4.5	11	49	39	4.9	3.5	1.4	1.3	2.5	16.5	5	6	0.3
546-15-34	82	75	36.5	42	44.5	60	35	M6	10	4.5	12	55	42	6.1	4.8	2.2	1.9	3.5	18	6	8	0.3
546-21-34	95	88	46	52	55	70	45	M8	12	5.5	14	63	45	8.7	6.0	2.8	2.2	3.0	20	6	10	0.4
546-23-34	114	105	55	62	65	80	55	M8	12	7.8	18	69	50	9.0	6.5	3.3	2.2	3.0	24	6	10	0.4
546-25-34	134	127	68	72	75	95	70	M12	15	9.5	20	83	61	11.0	8.4	4.3	2.7	3.0	26	8	10	0.4
546-31-34	166	152	80	90	93.5	120	85	M12	15	9.5	22	93.5	66	13.1	11.4	5.3	3.2	3.5	31	10	12	0.5
546-32-34	195	175	95	100	103.5	150	100	M12	19	11.5	24	110	80	14.0	11.7	6.3	3.2	4.0	38.5	10	12	0.5

How to Place an Order

546-12-34-NF 24V 10DIN



NF: Full-depth tooth, full-position

NS: Full-depth tooth, single-position

RF: Right-handed rotating sawtooth, full-position LF: Left-handed rotating sawtooth, full-position

RS: Right-handed rotating sawtooth, single-position LS: Left-handed rotating sawtooth, single-position

^{*} The allowable rotation speeds of engagement NF and NS indicate, respectively, full-depth tooth/full position and full-depth tooth/single position.

^{*}The dimension φ g marked with [*] does not apply for size 12.

^{*}Depending on your location and such, we may not be able to sell you our products. Please contact us for details.

Selection

I When Found from Motor Output

The clutch-shaft conversion of motor torque (TM) is:

$$T_{M} = \frac{9550 \cdot P}{n_{r}} \cdot \eta \text{ [N-m]} \dots (1)$$

- P: Motor output [kW]
- Clutch-shaft conversion of rotation speed [min-1]
- η : Transmission efficiency from motor to clutch

The required torque (T) when the motor is correctly selected for the load is:

$$T = T_M \cdot K [N \cdot m]$$
(2)

K: Safety factor

When Load Rotation Starts After Engagement

The acceleration torque (TA) for starting up within n rotations is:

$$T_A = \frac{J \cdot n}{9.55 \cdot t_A} [N \cdot m] \cdots (3)$$

J: Total moment of inertia on load side [kg·m²]

ta: Acceleration time [s]

Therefore, the required torque (T) is:

$$T = (T_L + T_A) K [N \cdot m] \cdots (4)$$

TL: Load torque [N•m]

Select the clutch size by searching the specification table for the clutch whose value adequately satisfies the required torque (T).

Safety factor: K

Load state	Factor
Low rotation speed/small torque fluctuation	1.5
Ordinary load/small torque fluctuation	2
High rotation speed/large torque fluctuation	3

Recommended Power Supplies and Accessory Parts

Madel	Danish dada a sanatina	Accessory parts				
Model	Recommended power supplies	Circuit protector (Varistor), qty. 1	Shims (Inner diameter × Outer diameter × Thickness), qty. 5 [mm]			
546-12-34- 🗌 24V 10 🗀	BES-20-51 • BEH-10G	NVD07SCD082 or an equivalent	$10.3 \times 13.7 \times 0.1t$			
546-13-34- 🗌 24V 15 🗀	BES-20-51 • BEH-10G	NVD07SCD082 or an equivalent	$15.3 \times 20.7 \times 0.1t$			
546-15-34- 🗆 24V 20 🗆	BES-20-51 • BEH-10G	NVD07SCD082 or an equivalent	$20.3 \times 27.7 \times 0.1t$			
546-15-34- 🗌 24V 25 🗌	BES-20-51 • BEH-10G	NVD07SCD082 or an equivalent	25.3 × 34.7 × 0.1t			
546-21-34- 🗆 24V 25 🗆	BES-20-52 • BEH-10G	NVD07SCD082 or an equivalent	$25.3 \times 34.7 \times 0.1t$			
546-21-34- 🗆 24V 30 🗆	BES-20-52 • BEH-10G	NVD07SCD082 or an equivalent	$30.3 \times 41.7 \times 0.1t$			
546-23-34- 🗆 24V 30 🗆	BES-20-52 • BEH-10G	NVD07SCD082 or an equivalent	$30.3 \times 41.7 \times 0.1t$			
546-23-34- 🗆 24V 40 🗆	BES-20-52 • BEH-10G	NVD07SCD082 or an equivalent	40.3 × 51.7 × 0.1t			
546-25-34- 🗆 24V 40 🗆	BES-20-52 • BEH-20G	NVD07SCD082 or an equivalent	$40.3 \times 51.7 \times 0.1t$			
546-25-34- 🗆 24V 50 🗆	BES-20-52 • BEH-20G	NVD07SCD082 or an equivalent	50.3 × 61.7 × 0.1t			
546-31-34- 🗆 24V 50 🗆	BES-40-53 • BEH-20G	NVD14SCD082 or an equivalent	50.3 × 61.7 × 0.1t			
546-31-34- 🗆 24V 60 🗆	BES-40-53 • BEH-20G	NVD14SCD082 or an equivalent	60.3 × 71.1 × 0.1t			
546-32-34- 🗆 24V 60 🗆	BES-40-53 • BEH-20G	NVD14SCD082 or an equivalent	60.3 × 71.1 × 0.1t			
546-32-34- 🗆 24V 70 🗆	BES-40-53 • BEH-20G	NVD14SCD082 or an equivalent	70.3 × 79.7 × 0.1t			

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

C023

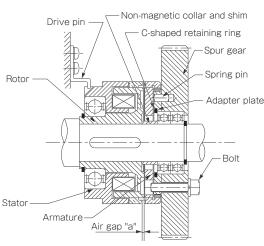
^{*} Varistors need not be used when a BES/BEH model recommended power supply is used. For details, refer to the section on power supplies.

546 Models

Items Checked for Design Purposes

Precautions for Mounting

This clutch is mounted for a through-shaft. The mounting example shown below is for mounting on an ordinary through-shaft.

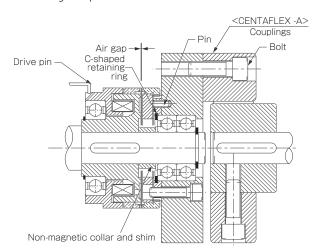


- 1 Set the air gap between the teeth tips on the rotor and armature sides so that it is the value "a" in the dimensions table. Shims may be used to facilitate setting of the air gap.
- 2 Use a collar made of a non-magnetic material (such as stainless steel or brass) to set the air gap. Use the reference values of the table below for the length of the collar when centering bearings relative to the adapter plate.

Collar lengths when using bearings to center

Size	Dimensions [mm]	Size	Dimensions [mm]
12	7.3	23	15.5
13	8.3	25	17.5
15	10.5	31	22.0
21	15.0	32	23.5

- * Process the collar length to the negative tolerance and then make fine adjustments with shims.
- Five shims (0.1 mm in thickness) are provided for each shaft bore diameter.
- * If not using the bearing to center, use a different collar design
- 3 When mounting, lock it securely in the axial direction so that there is no play (rattle) in the axial direction.
- 4 We recommend a tolerance of h6 or j6 for the shaft when mounting.
- **5** This clutch is for through-shafts; when using it on butt shafts, align one of the shafts with a bearing. Using a MIKI PULLEY CENTAFLEX coupling makes it relatively easy to find the centers. See the mounting examples below.



6 The inner diameter of the adapter plate is the same as the outer diameter of the ball bearing, so the center is easy to find when designed to directly press in the ball bearings.

Recommended bearings when inner diameter of adapter plate is used as centering mark

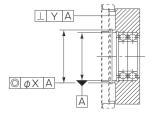
Size	Bore diameter ød [mm]	Centering dimension øD [mm]	Bearing
12	10	26	6000
13	15	32	6002
15	20	42	6004
15	25	42	6905
21	25	52	6205
23	30	62	6206
23	40	62	6908
25	50	72	6910
31	50	90	6210
32	70	100	6914

Ball bearings cannot be used as centering points for combinations of the sizes and shaft diameters at right; in

such cases, install centering positions on the flange (gear, sprocket, or the like) on which the adapter plate is mounted and then find the centers. Use the following as a reference for the precision of the mounting surface of the armature (adapter plate).

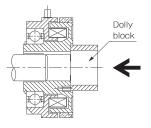
Size	Bore diameter ød [mm]	Centering dimension ØD [mm]
21	30	52
25	40	72
31	60	90
32	60	100

Armature (adapter plate) mounting surface precision



Size	X [mm]	Y [mm]
12	0.04	0.03
13	0.05	0.04
15	0.05	0.04
21	0.06	0.05
23	0.07	0.05
25	0.08	0.06
31	0.08	0.07
32	0.10	0.08

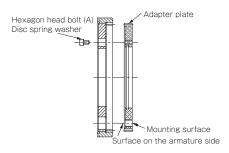
- Use two ball bearings in the flange (gear, sprocket, or the like) on which the armature (adapter plate) is mounted so that no vibration is generated in the armature.
- 3 A pilot bore for mounting the spring pin has been drilled in the adapter plate. (This does not apply to size 12.) Although in some conditions its use can be omitted, we recommend that after the flange (gear, sprocket, or the like) that mounts on the adapter plate is mounted, additional processing gauged against actual objects be performed and spring pins be concurrently used. (Concurrent use of spring pins is not necessary for size 12.) For details, see the section on assembly of the armature part.
- Apply a small amount of adhesive to stop loosening to the bolt that mounts the adapter plate on the gear, sprocket, or the like
- When inserting the stator side onto the shaft, damage can result from strong pounding with a hammer or pushing on the outer circumference part. Press a pipe-



- shaped dolly block near the shaft bore of the boss part and carefully insert it. The material is soft, so do not bend it as you insert.
- 10 Hold the stator only in the direction of rotation, using the cut-out for stopping rotation. Be careful not to apply pressure on the cut-out in the shaft direction at this time.
- **12** We recommend applying lubricant (molybdenum disulfide grease) to the teeth tips to improve the wear resistance of the teeth tips.
- B Hold it so that no force is applied that might pull on or damage leads.

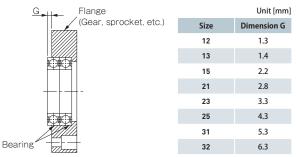
Assembly of Armature Components

• Remove the hexagon head bolt [A] previously fixed in place from the armature side and separate the armature and adapter plate. At this time, make fitting marks with a marker to show where the armature and adapter plate fit together to facilitate re-assembly.

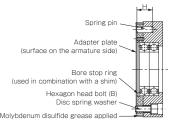


2 Press-fit the bearing onto the flange (gear, sprocket, etc.). If there are bearing centering marks, use a flange design that results in the bearing projection (dimension G) being the value in the table below.

Bearing projection



- * When press-fitting a bearing, apply bearing mount (adhesive) to the outer circumference of the bearing. * Finish the depth of the bearing insertion bore to the positive tolerance (we recommend 0 to +0.1) and adjust with shims so there is no play (rattle) in the thrust direction
- 3 Snap the C-shaped snap ring in the C-shaped snap ring groove of the adapter plate. Use shims to adjust the air gap between the bearing and snap ring (for rattle).
- Mount the adapter plate on the flange and tighten the hexagon head bolt (B) Molybdenum disulfide grease applied to secure it.



- * Pay attention to the orientation of the adapter plate
- Apply a small amount of adhesive to the hexagon head bolt.
- * See the table below for the hexagon head bolt tightening torque.

Adapter plate mounting bolt tightening torque

		Tightening t	Tightening torque [N·m]					
Size	Bolt	When spring pin is used	When no spring pin is used					
		Bolt strength category 8.8 or higher	Bolt strength category 10.9 or higher					
12	3-M4	_	3.4					
13	3-M5	5.2	7.0					
15	3-M6	8.8	11.8					
21	3-M8	22.0	29.5					
23	3-M8	22.0	29.5					
25	3-M12	77.0	104.0					
31	6-M12	77.0	104.0					
32	6-M12	77.0	104.0					

5 Use the adapter plate's pilot bore for pins to simultaneously drill the spring pin bore. (Burr must be removed.) Consult the following table's recommended bore drilling dimensions for spring pin parts when drilling pin bores.

Recommended have drilling dimensions for spring nin parts

iii 16 dii iioi loio	no for opinio pin parto	Unit [mm]
Bore drilling dimension	Recommended depth H	Spring pin
5 + 0.12	13	5 × 10
5 + 0.12	13	5 × 10
6 + 0.12	15	6 × 12
8 + 0.15	19	8 × 16
10 + 0.15	21	10 × 18
10 + 0.15	25	10 × 22
13 + 0.2	25	13 × 22
	Bore drilling dimension 5 + 0.12 5 + 0.12 6 + 0.12 8 + 0.15 10 + 0.15 10 + 0.15	S + 0.12 13 13 13 14 15 15 15 15 15 16 16 16

- * Recommended depth H includes the adapter plate drilling margin.
- **6** Hammer a spring pin into the bore drilling site. Hammer in the spring pin with the indexing direction facing the outer circumference (spline side). When doing so, be careful that the pin does not extend beyond the adapter plate surface. Have spring pins ready that meet the specifications of the table above.
- © Completely remove any dust, powder or the like produced by bore drilling and wipe the spline part with molybdenum disulfide grease.
- 3 Insert the adapter plate back onto the armature using the fitting marks previously drawn, and fasten with the hexagon head bolt [A] that you removed. (Do not use adhesives.) See the table below for the tightening torque.

Hexagon head bolt (A) Disc spring washer	9	Sp	line

Size	Bolt	Tightening torque [N·m]
12	$M3 \times 3$	1.5
13	$M3 \times 4$	1.5
15	$M3 \times 4$	1.5
21	$M4 \times 6$	3.4
23	$M4 \times 6$	3.4
25	$M4 \times 8$	3.4
31	$M5 \times 10$	7.0
32	M6 × 10	11.8

Precautions for Use

- Tooth will not mesh together if the inertia on the driven side is too great. In such cases, we recommend lowering the rotation speed or also using a CENTAFLEX coupling to absorb shock.
- 2 With single position tooth shapes, drag torque will be generated by contact between tooth tips until the tooth reach their engaging position after pull-in. Tooth clutches are structured, however, so the tooth do not form a magnetic circuit, meaning that drag torque is low and hardly ever a problem. When load torque is very small compared to clutch torque, however, drag turning may occur on the driven side. In such cases, a brake must also be used, to prevent drag
- 3 The keyway cannot be aligned with the adapter plate mounting holes in the engaging position. When alignment is necessary, adjust position with the paired side elements of the clutch.
- 4 When used in stationary engagement, teeth may fail to engage and come into contact with other tooth tips when pull-in occurs. Rotation in this condition may result in teeth slipping rather than engaging, so adjust the acceleration speed of the drive side to engage.
- **5** The operating power supply of the clutch is DC 24 V. Keep fluctuations of the applied voltage within -10% to +5%. Since optimal BES model power supplies are available for the tooth clutch, we recommend one of these be used for both.
- 6 Install a switch on the DC side to turn the clutch on and off. Operating times will be slower if it is installed on the AC side. A varistor to protect contacts should also be connected in parallel to the clutch.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNET	ELECTROMAGNETIC- ACTUATED MICRO CLUTCHES & BRAKES
IC-ACTUATED CLUT	ELECTROMAGNETIC- ACTUATED CLUTCHES & BRAKES
CHES AND BRAKE	ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BRAKE MOTORS

Printing machinery, bookbinding machinery, food machinery, wrapping machinery, medical machinery

Induction Motors with Integrated Brakes

Brake motors incorporate an internal electromagnetic-actuated brake or spring-actuated brake without changing the dimensions of the induction motor. A compact power supply for the brake is built into the terminal box, so the brake motor can be simply connected and used. Choose from either base-mounted or flange-mounted types.





Same dimensions as induction motor

Since the brake is incorporated without changing the dimensions of the induction motor, mounting is easy.

Long service life

The large frictional surface area provides a long service life.

Built-in power supply

A small power supply is included in the product and handling is easy.

Quiet running (BMS models)

The rotating part (disc) is completely integrated into the motor shaft, so operation is quiet.

I Manual release (BMS models)

The braking/holding state can be manually released using a release lever.

Stable rapid braking (BMM models)

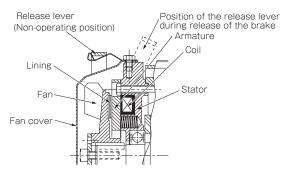
Torque is transmitted by a constant-load spring, enabling stable and rapid braking.

Available Models

	Model	Base-	Flange-				Mot	or output [l	kW]			
	Model	mounted	mounted	0.2	0.4	0.75	1.5	2.2	3.7	5.5	7.5	11
Spring-actuated	BMS	•	•	•	•	•	•	-	-	-	_	_
Electromagnetic- actuated	ВММ	•	•	•	•	•	•	•	•		A	A

Structure

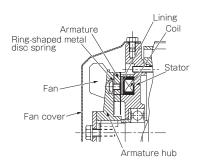
BMS Construction



IBMS Operating Principles

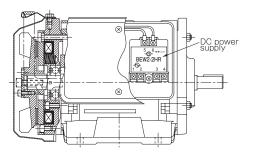
These brakes are spring actuated type brakes. When the power is turned on, the stator is magnetized simultaneous with the motor, and the generated attraction force pulls the armature to the stator, overcoming the pressure of the torque spring. An air gap between the disc and armature is created at that time, the brake is fully released, and the motor shaft rotates. When the current is shut off, the magnetic attraction force of the stator is extinguished, the armature is pushed back by the force of the torque spring, braking force is applied to the disc, and the motor shaft rapidly stops.

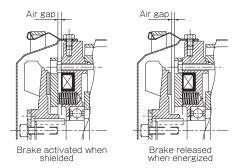
I BMM Construction

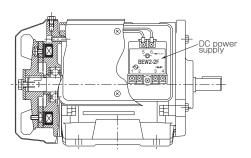


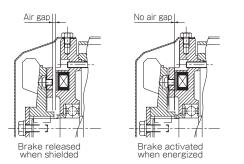
I BMM Operating Principles

These brakes are electromagnetic actuated type brakes. When current flows to the coil, the stator is magnetized and the armature is pulled in. Frictional force working between the lining and armature then generates the braking torque of the brake. When the current is shut off, the armature is pulled back by the ring-shaped metal disc spring located between the armature and hub, and the lining and armature are instantly released.









COLIDILINGS

ETP BUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

SPEED CHANGERS

INVERTER

LINEAR SHAFT DRIVES

TOPOLIE LIMITERS

ROSTA

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
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CLUTCHES & BRAKES
ELECTROMAGNETIC
CLUTCH & BRAKES
UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BMS

вмм

BMS Models Spring-actuated Brake Motors

Specifications

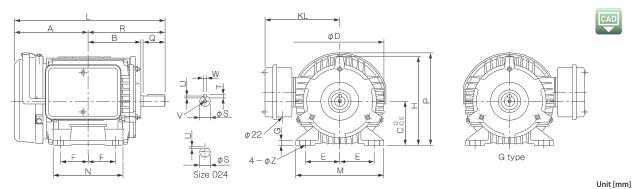
	Мс	otor				E	Brake				Rotating				Operating time	9	
Model	Fra	Out 4	_7		Coil (at	t 20℃)		res	Air	gap	part moment of	Allowable braking	Total braking	Armature	Coastdo	wn time	Mass
Model	Frame No.	Output [kW] 4-poles	Torque T [N·m]	Voltage [V]	Current [A]	Resistance [Ω]	Wattage [W]	Heat istance class	Control value [mm]	Limit value [mm]	inertia J [kg·m²]	energy rate Pba & [W]	energy E _T [J]	pull-in time t _a [s]	Simultaneous off [s]	DC off separately [s]	[kg]
BMS-024-NHBN	63	0.2	2	DC90	0.20	440	18	В	0.15 ~	0.40	0.8 × 10 ⁻³	18	3.5×10^{7}	0.04	0.1	0.08	7.5
BMS-024-NHFN	03	0.2	2	DC90	0.20	440	10	ь	0.25	0.40	0.0 × 10	10	3.5 × 10	0.04	0.1	0.00	8.5
BMS-044-NHB	71	0.4	4	DC90	0.28	324	25	В	0.15 ~	0.40	1.5 × 10 ⁻³	26.2	7.0×10^{7}	0.05	0.1	0.08	10
BMS-044-NHF	/1	0.4	7	DC90	0.20	324	23	ь	0.25	0.40	1.5 × 10	20.2	7.0 × 10	0.03	0.1	0.00	11
BMS-074-HPB	80	0.75	8	DC90	0.33	270	30	В	0.20 ~	0.50	4.3 × 10 ⁻³	29.4	12.5 × 10 ⁷	0.05	0.14	0.09	16.5
BMS-074-HPF	80	0.75	0	DC90	0.55	270	30	ь	0.30	0.50	4.5 × 10	23.4	12.5 × 10	0.05	0.14	0.09	19
BMS-154-HPB	90	1.5	15	DC90	0.34	261	31	В	0.20 ~	0.60	8.1 × 10 ⁻³	45.8	20.0×10^{7}	0.11	0.15	0.09	23
BMS-154-HPF	90	1.3	13	DC90	0.34	201	31	b	0.30	0.00	0.1 \ 10 -	٥.٥٠	20.0 × 10	0.11	0.13	0.09	26

- * The induction motors are fully sealed external fan motors that conform to the JIS C4210 standard (for 0.2 kW and 0.4 kW models) or the JIS C 4213 standard (for 0.75 kW models or higher). (made by Hitachi In-* The power supplies for the motors are 3-phase, 200 V AC at 50 Hz, or 200/220 V AC at 60 Hz.

 * See P.377 for the allowable braking frequency of brake motors. The specific frequency varies with load conditions, so confirm it in your selection calculations.

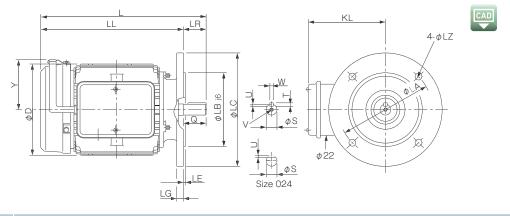
Dimensions

Base-mounted



Model											Dimen	sions o	f part								
wodei	L	R	Α	В	D	KL	Н	Р	C	F	E	N	М	G	Z	S	W	U	T	Q	V
BMS-024-NHBN	215	103	112	79	130	115	128	134	63	40	50	100	130	3.2	7 × 21	11 h6	_	1	_	23	_
BMS-044-NHB	244	120	124	87	145	141	143.5	150	71	45	56	115	140	3.2	7 × 20	14 j6	5	3	5	30	$\text{M5}\times\text{0.8}, \text{length: 18}$
BMS-074-HPB	290.5	140	150.5	97	163	148	161.5	168	80	50	62.5	125	160	3.2	10 × 25	19 j6	6	3.5	6	40	M6 × 1, length: 20
BMS-154-HPB	329	168.5	160.5	114.5	182	144	178	188	90	62.5	70	155	170	10	10	24 j6	8	4	7	50	M6 × 1, length: 20

■ Flange-mounted



١	U	ni	t	1]	n	n	1

Model			Dimensions of part																
Model		L	LR	LL	D	KL	LC	Υ	LB	LA	LE	LG	LZ	S	W	U	T	Q	V
BMS-024-N	HFN	241	23	218	130	115	160	70	110	130	3.5	8	10	11 h6	-	1	_	23	-
BMS-044-N	NHF	265	30	235	145	134.5	160	79	110	130	3.5	10	10	14 j6	5	3	5	30	M5 × 0.8, length: 18
BMS-074-H	HPF	305	40	265	163	142	200	88	130	165	3.5	12	12	19 j6	6	3.5	6	40	M6 \times 1, length: 20
BMS-154-F	HPF	349	50	299	176	144	200	98	130	165	3.5	12	12	24 j6	8	4	7	50	$M6 \times 1$, length: 20

Options and Made to Order

I Products with Motor Terminal Box Mounted in Reverse

Option symbol: G

The location where the brake motor is installed may make it impossible to mount the motor's terminal box in the standard location in some cases. In such cases, the mounting dimensions of the G types can be considered. Use the dimensions drawing to check the positions of the terminal boxes on G type motors.

Products with BEW2-2H Brake Rectifiers

Option symbol: 2H

By using a brake motor with an inverter or the like, the motor can be fitted with a power supply that shuts off DC separately (BEW2-2H) when fast response is needed.

List of Accessories

Brake motors come with the components listed at right.

When mounting a V pulley or the like on a brake motor output shaft, the V pulley or the like can be mounted simply on the motor shaft by concurrently using a motor shaft end face tap and the accessories listed at right.

For size 024, the motor output shaft has a flat face, so the shaft end face cannot be tapped and the accessories listed at right are not provided.

Siz	ze	024	044	074	154
Tightening collars: 1	φ 6.5 × φ 35 × 3.2t	-	0	0	0
Screw stocks: 1	M5 × 70	_	0		
Screw Stocks: 1	M6 × 100	_		0	0
Hexagonal nuts: 1	M5	_	0		
nexagonal nuls: 1	M6	_		0	0

How to Place an Order

Base-mounted

0.2kW : BMS-024-NHBN-Option symbols 0.4kW : BMS-044-NHB Option symbols 0.75kW: BMS-074-HPB Option symbols 1.5kW : BMS-154-HPB

To download CAD data or product catalogs:

I Flange-mounted

0.2kW : BMS-024-NHFN--Option symbols 0.4kW : BMS-044-NHF Option symbols 0.75kW: BMS-074-HPF Option symbols 1.5kW : BMS-154-HPF -Ontion symbols

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

Unit [mm]

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES FI FCTROMAGNETIC ACTUATED **CLUTCHES & BRAKES** FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BMS

вмм

C024

Web code

-Ontion symbols

BMM Models Electromagnetic-actuated Brake Motors

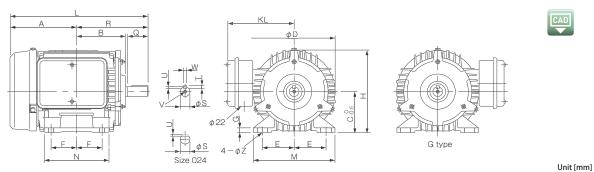
Specifications

	Мо	tor					Brake				Rotating	Allannahla	Tatal	Operati	ng time	
Model		Out 4	_ 7		Coil (at	20°C)		res	Air	gap	part	Allowable braking	Total braking	Armature	Armature	Mass
Model	Frame No.	Output [kW] 4-poles	Torque T [N·m]	Voltage [V]	Current [A]	Resistance [Ω]	Wattage [W]	Heat resistance class	Control value [mm]	Limit value [mm]	moment of inertia J [kg·m²]	energy rate Pba & [W]	energy Eτ[J]	pull-in time ta [s]	release time tar [s]	[kg]
BMM-024-NHBN	63	0.2	2.5	DC180	0.06	2956	11	В	0.10 ~	0.30	0.9 × 10 ⁻³	11	5.0 × 10 ⁷	0.015	0.015	7
BMM-024-NHFN	03	0.2	2.5	DC180	0.00	2930	"	Б	0.20	0.30	0.9 × 10 -	"	3.0 × 10	0.013	0.013	8
BMM-044-NHB	71	0.4	5	DC180	0.07	2458	12.6	В	0.10 ~	0.35	2.4 × 10 ⁻³	26.2	7.0 × 10 ⁷	0.030	0.030	9
BMM-044-NHF	/ 1	0.4	3	DC160	0.07	2430	12.0	D	0.20	0.55	2.4 ^ 10 -	20.2	7.0 × 10	0.030	0.030	10
BMM-074-HPB	80	0.75	10	DC180	0.089	2039	16	В	0.15 ~	0.45	3.8 × 10 ⁻³	32.7	17.0 × 10 ⁷	0.040	0.040	14.5
BMM-074-HPF	80	0.73	10	DC180	0.069	2039	10	Б	0.25	0.43	3.0 ^ 10 -	32.7	17.0 × 10	0.040	0.040	16.5
BMM-154-HPB	90	1.5	20	DC180	0.123	1466	22.1	В	0.15 ~	0.70	9.5 × 10 ⁻³	45.8	25.0 × 10 ⁷	0.060	0.060	22
BMM-154-HPF	90	1.5	20	DC100	0.123	1400	22.1	D	0.25	0.70	9.3 ^ 10 -	43.0	23.0 × 10	0.000	0.000	25
BMM-224-HPB	100	2.2	30	DC180	0.167	1080	30	В	0.20 ~	1.00	15.2 × 10 ⁻³	58.9	50.0 × 10 ⁷	0.070	0.070	32
BMM-224-HPF	100	2.2	30	DC 180	0.107	1080	30	р	0.30	1.00	13.2 × 10 3	36.9	30.0 × 10'	0.070	0.070	37
BMM-374-HPB	112	3.7	50	DC180	0.17	1059	30.6	В	0.20 ~	1.10	22.6 × 10 ⁻³	73.6	75.0 × 10 ⁷	0.070	0.080	42
BMM-374-HPF	112	5./	50	DC180	0.17	1059	50.6	В	0.30	1.10	22.0 × 10 3	/3.5	/5.0 × 10 [/]	0.070	0.080	47

^{*} The induction motors are fully sealed external fan motors that conform to the JIS C4210 standard (for 0.2 kW and 0.4 kW models) or the JIS C 4213 standard (for 0.75 kW models or higher). (made by Hitachi Industrial Equipment Systems)

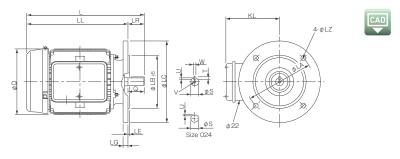
Dimensions

■ Base-mounted



Model										Dir	mensio	ns of pa	art							
Model	L	R	Α	В	D	KL	Н	C	F	E	N	М	G	Z	S	W	U	Т	Q	V
BMM-024-NHBN	215	103	112	80	130	115	128	63	40	50	100	130	3.2	7 × 21	11 h6	-	1	_	23	-
BMM-044-NHB	235.5	120	115.5	87	145	131	143.5	71	45	56	115	140	3.2	7 × 20	14 j6	5	3	5	30	M5 × 0.8, length: 18
BMM-074-HPB	280.5	140	140.5	97	163	138.5	161.5	80	50	62.5	125	160	3.2	10 × 25	19 _{j6}	6	3.5	6	40	M6 × 1, length: 20
BMM-154-HPB	321	168.5	152.5	114.5	182	144	178	90	62.5	70	155	170	10	10	24 j6	8	4	7	50	M6 × 1, length: 20
BMM-224-HPB	368.5	193	175.5	129	198	151	197.5	100	70	80	175	195	12.5	12	28 j6	8	4	7	60	M6 × 1, length: 20
BMM-374-HPB	397	200	197	136	225	164	219.5	112	70	95	175	224	14	12	28j6	8	4	7	60	M6 × 1, length: 20

■ Flange-mounted



Unit [mm]

Model		Dimensions of part															
Model	L	LR	LL	D	KL	LC	LB	LA	LE	LG	LZ	S	W	U	T	Q	V
BMM-024-NHFN	241	23	218	130	115	160	110	130	3.5	8	10	11 h6	-	1	-	23	_
BMM-044-NHF	256.5	30	226.5	145	124.5	160	110	130	3.5	10	10	14 j6	5	3	5	30	$M5 \times 0.8$, length: 18
BMM-074-HPF	295	40	255	163	132	200	130	165	3.5	12	12	19 j6	6	3.5	6	40	$M6 \times 1$, length: 20
BMM-154-HPF	341	50	291	176	144	200	130	165	3.5	12	12	24 j6	8	4	7	50	$M6 \times 1$, length: 20
BMM-224-HPF	388.5	60	328.5	195	151	250	180	215	4.0	16	14.5	28 j6	8	4	7	60	M6 $ imes$ 1, length: 20
BMM-374-HPF	422	60	362	215	164	250	180	215	4.0	16	14.5	28 j6	8	4	7	60	$M6 \times 1$, length: 20

^{*} The power supplies for the motors are 3-phase, 200 V AC at 50 Hz, or 200/220 V AC at 60 Hz.

* See P.377 for the allowable braking frequency of brake motors. The specific frequency varies with load conditions, so confirm it in your selection calculations.

Optional

Made to Order

Products with Motor Terminal Box Mounted in Reverse

Option symbol: G

The location where the brake motor is installed may make it impossible to mount the motor's terminal box in the standard location in some cases. In such cases, the mounting dimensions of the G types can be considered.

Use the dimensions drawing to check the positions of the terminal boxes on G type motors.

Products with High Motor Output, 5.5 kW to 11 kW

We also support motors with high motor output (5.5 kW to 11 kW). Consult Miki Pulley for details.

BMM-

- Motor output/number of poles

s 554: 5.5 kW, 4-pole 754: 7.5 kW, 4-pole 1104: 11 kW, 4-pole

ETP BUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

& REDUCERS

INVEDTEDS

LINEAR SHAFT DRIVES

TOPOLIE I IMITEDO

ROST

List of Accessories

Brake motors come with the components listed at right.

When mounting a V pulley or the like on a brake motor output shaft, the V pulley or the like can be mounted simply on the motor shaft by concurrently using a motor shaft end face tap and the accessories listed at right.

For size 024, the motor output shaft has a flat face, so the shaft end face cannot be tapped and the accessories listed at right are not provided.

						Uni	it [mm]
Size			044	074	154	224	374
Tightening collars: 1	φ 6.5 × φ 35 × 3.2t	_	0	0	0	0	0
Screw stocks: 1	M5 × 70	-	0				
Screw Stocks: 1	M6 × 100	-		0	0	0	0
Havenenel nute. 1	M5	_	0				
Hexagonal nuts: 1	M6	_		0	0	0	0

How to Place an Order

Base-mounted

0.2kW : BMM-024-NHBN
0.4kW : BMM-044-NHB - Option symbols

0.75kW : BMM-074-HPB - Option symbols

1.5kW : BMM-154-HPB - Option symbols

2.2kW : BMM-224-HPB - Option symbols

3.7kW : BMM-374-HPB -

I Flange-mounted

0.2kW : BMM	-024-NHFN	1-
0.4kW : BMM	-044-NHF	Option symbols
0.75kW : BMM	-074-HPF	Option symbols
1.5kW : BMM	-154-HPF	Option symbols
2.2kW :BMM-	-224-HPF	Option symbols
3.7kW : BMM-	-374-HPF	Option symbols
		Option symbols

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
ELECTROMAGNETICACTUATED
CLUTCHES & BRAKES
ELECTROMAGNETIC
CLUTCH & BRAKE
UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BMS

вмм

Option symbols

Web code

C025

BMS/BMM Models

Selection

Study the following items, in order, to determine the final size and type.

• Operating condition settings Set the application, torque, number of operations, etc.

Confirm the torque using Eqs. (1) and (2). • Provisional size and type selection · · · · Provisionally select the size and type based

on calculated torque values. Provisionally select the braking time based

• Consideration of amount of energy

on calculated torque values. Confirm the energy amount using Eqs. (4)

• Consideration of number of braking operations · · ·

Confirm the number of braking operations using Eqs. (6) and (7).

· Determine size and type

Consideration of Torque

$$T_{M} = \frac{9550 \cdot P}{n} \quad [N \cdot m] \quad \dots (1)$$

Тм: Rated torque of motor [N•m]

P: Motor output [kW]

n: Rated rotation speed of motor [min-1]

$$T_B = K \cdot T_M [N \cdot m]$$
 (2)

TB: Braking torque [N•m]

K: Safety factor (1.5 to 2.0)

Consideration of Braking Time

The braking time can be found for brakes using the following equation.

$$t_{ab} = \frac{J \cdot n}{9.55 \cdot (T \pm T \ell)} [s] \dots (3)$$

tab: Braking time [s]

J: Moment of inertia of brake shaft [kg•m²]

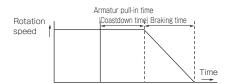
n: Motor rotation speed [min⁻¹]

T: Rated torque of brake [N•m]

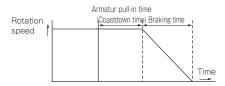
Tℓ: Load torque [N•m]

(The sign of T_ℓ is positive when the load works in the direction that assists braking and negative when it works in the direction that opposes it.)

The time required from excitation of the brake coil to stopping of the load on BMM models is the braking time tab found with the preceding equation plus the armature pull-in time.



The time required from cutting off the power supply of a BMS model brake motor to stopping of the load is the braking time tab found with the above equation plus the armature release time.



When brakes are used for long periods of time, they wear, air gaps grow, and it becomes impossible to pull in the armature even when the coil is excited. If re-adjustment becomes necessary, adjust the air gap as described in the maintenance and inspection section of the operating manual.

Consideration of Amount of Energy

The braking energy rate can be found for brakes using the following equation.

$$P = \frac{J \cdot n^2}{182} \cdot \frac{T}{(T \pm T \ell)} \cdot \frac{S}{60} [W] \cdots (4)$$

P: Braking energy rate [W]

S: Frequency of braking (braking operations/min)

Set a frequency that results in a value P obtained in the above equation that is no greater than the allowable braking energy rate $\mathsf{Pba}\,\ell$.

Consideration of Number of Braking Operations

Use the following equation to find the number of operations before readjustment of the air gap of the brake.

$$E_b = \frac{J \cdot n^2}{182} \cdot \frac{T}{(T \pm T_{\ell})} [J] \qquad (6)$$

Eb: Braking energy of one braking operation [J]

$$L = \frac{E_T}{F_h} [braking operations]$$
 (7)

L: Number of operations before readjustment [braking operations] ET: Total braking energy [J]

Items Checked for Design Purposes

I Precautions for Handling

What is the best way to ensure that the design allows brake motors used in machinery and equipment to perform and function adequately? We describe here approaches to design that we feel are useful in improving machinery reliability. Consult the catalog of the motor manufacturer for information on connecting motors to machinery using V pulleys or the like.

- Design in a reasonable space on the fan cover side to allow for cooling, maintenance and inspections.
- Operating temperature range: -10°C to 40°C. Contact Miki Pulley if you will use the product outside this range.
- If you are using this brake motor in a winch, lift, or the like, also use a brake of a different mechanism to prevent dangerous situations. Also, if you are using a standard shutoff circuit in an elevating winch or the like, there will be a θ load during the braking delay time and an electromotive force will occur in the motor part that will prevent the brake from engaging. For that reason, be sure to use a DC shutoff or separate shutoff circuit.
- If you are mounting a phase-advancing capacitor, consult Miki Pulley.
- Brake motors have consumable components such as linings, and thus have a finite service life. Please keep spares available. Also note that if the start frequency of the brake motor exceeds the allowed value, motor parts may burn or the brake lining may be subject to abnormal wear or damage. Check that the start frequency is staying within the allowed value. Also be aware of the capacitance of contacts for DC shutoff when you are inching at a frequency that exceeds the allowable start frequency.

Allowable start frequency of brake motor

Models	Motor output [kW]	Frequ [star	Moment of inertia of load						
		40%ED	60%ED	J [kg⋅m²]					
	0.2	500	400	0.00125					
BMS	0.4	900	845	0.00128					
вмэ	0.75	460	430	0.0028					
	1.5	370	290	0.0045					
	0.2	450	360	0.00125					
	0.4	900	845	0.00128					
ВММ	0.75	460	430	0.0028					
БММ	1.5	370	290	0.0045					
	2.2	180	145	0.010					
	3.7	180	145	0.015					

- * These values are for 4 poles and a frequency of 50 Hz using the moment of inertia J of the load from the above table as the condition. For 60 Hz, use frequencies of about 70% of the above values.

 * Frequency is a total value for the motor part and brake together. Their values as stand-
- alones aré different.
- * %ED is the percentage duty cycle during repeated operation.

 * The table's example of moment of inertia J of the load is virtually the same as the moment of inertia J of the motor part.
- The approximate temperature of the outer surface of the motor is 80° C to 90° C (for an ambient temperature of 40° C).
- If using an inverter or reduced-voltage starting, connect the brake or brake power supply to the power supply side of the inverter or reduced-voltage starter.
- If the wiring for the brake circuit is in the same conduit as the power lines, be sure to shield it.
- · When inserting a capacitor for improving the power factor into the brake motor circuit, be sure to use a separate shutoff circuit.
- Grounding terminals are provided in or on the side of the terminal box or at the bottom of the frame. Be sure to do the grounding work. Mobile or movable machinery is covered by labor safety regulations as well. Be sure to ground it with large-gauge grounding wires to prevent accidents from shocks.
- Keep the voltage imbalance rate to 1% or less. Also keep the maximum current value for each phase to 105% or less of the nameplate current value when a voltage imbalance occurs.
- · Always mount the cover on the terminal box after connections are made.
- Brake torque may vary somewhat. Break-in operation (40 to 60 brakings) is particularly advisable at initial use.
- If power goes out, be sure to turn the power switch off. Accidents can occur if the electricity comes back on unexpectedly.
- Before starting a BMS model, always check that the release lever is in the non-operating position before starting machinery operation.

Wiring

BMS

A power supply with built-in relays (BEW2-2HR) is incorporated into BMS models, so BMS models generally have a responsiveness close to that of separate DC shutoff, and are adequate for use. By concurrently using an inverter or the like, the motor can be fitted with a power supply that shuts off DC separately (BEW2-2H) when even faster response is needed. This is supported as an option. Please specify it in advance.

BEW2-2HR: Brake power supply for building into relays for BMS (built

into terminal box)

MgSw: Electromagnetic switch

M: Motor Brake

The power supply, motor terminal block, and brake are connected in advance, so the unit can be used by wiring only the U, V, and W leads

BEW2-2H: Separate shutoff power supply for BMS (Specify in advance when ordering a brake motor.)

Cutting by DC Simultaneous cutting BEW2-2HR BEW2-2I MgSw MgSw

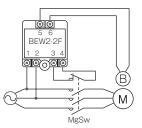
BMM

BEW2-2F: Brake power supply for BMM (built into terminal box)

MgSw: Electromagnetic switch

M: Motor Brake

(BEW2-2F is connected in advance.)



I Precautions for Use

Inspect the following items periodically.

- Is the device operating properly?
- Has water or oil penetrated the brake part?
- · Has tightening of the mounting screws of all parts been completed?
- During periodic inspections, remove the motor fan cover and use compressed air to blow out wear debris created by friction to eliminate it or pull-in it up with a dust collector.
- · Check whether the air gap is within its service life limit. If it is at the limit value, adjust it to the prescribed air gap stated in the operating
- If the limit air gap has been exceeded, BMS models are particularly prone to the brake becoming unable to release due to malfunctioning armature pull-in, which can lead to problems such as motors burning

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES FI FCTROMAGNETIC ACTUATED **CLUTCHES & BRAKES** FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

> SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

вмм

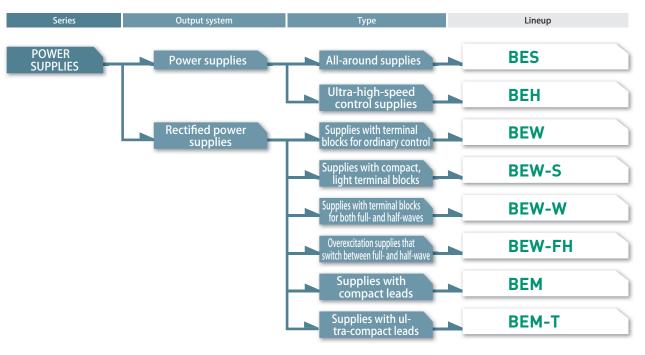
POWER SUPPLIES

Power Supplies to Get the Best Performance from Electromagnetic Clutches and Brakes

Compatible with AC 100, 200, and 400 V input power supplies. Outputs DC 24, 45, 90, and 180 V specifications for electromagnetic clutches and brakes. Broadly divided into power supplies for electromagnetic-actuated devices, which primarily require high-speed and ultra-high-speed control, and rectified power supplies, which are used by spring-actuated brakes and the like. A broad selection of power supplies are available.



Available Models



Model Selection

Madal/Tura	Applicable clutches and brakes			Input voltage		Output voltage				Function			
Model/Type	Electromagnetic- actuated	Tooth	Spring-actuated	100V	200V	400V	24V	45V	90V	180V	Overexcitation	Reverse excitation	Weak excitation
BES	0	0	0	0	0		0	0	0		0		
ВЕН	0	0		0	0		0				0	0	

Madal/Ton	Applicable	Applicable clutches and brakes			nput voltag	e		Output	voltage			Function	
Model/Type	Electromagnetic- actuated	Tooth	Spring-actuated	100V	200V	400V	24V	45V	90V	180V	Overexcitation	Reverse excitation	Weak excitation
BEW			0	0	0	0		0	0	0			
BEW-S			0	©	0	0		0	0	0			
BEW-W			0	©	0	0		0	0	0			
BEW-FH			0	©	0	0		0	0		0		0
ВЕМ			0	0	0	0		0	0	0			
ВЕМ-Т			0	0	0	0		0	0	0			

COUPLINGS

FTP RUSHINGS

ELECTROMAGNETIC CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

I INEAD CHAET DDIVE

TODOLIE LIMITEDS

POSTA

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
ELECTROMAGNETICACTUATED
ACTUATED
CLUTCHES & BRAKES
ELECTROMAGNETIC
CLUTCHES & BRAKES
ELECTROMAGNETIC
CLUTCH & BRAKE
UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BES
BEH
BEW
BEW-S
BEW-W
BEW-FH
BEM
BEM-T

Product Lineup

BES

For ordinary high-speed control



RoHS-compliant

All-around types suitable for the full range of electromagnetic clutches and brakes

Built-in overexcitation function

Can operate at high frequency and high precision.

Zero standby power

When used with one of our spring-actuated brakes, power consumption can be reduced by over 70%.

Light and compact

All terminals are contactless.

Compatible with international standards

UL listed. Products compatible with EC directives (CE markings) are available as options.

Applicable clutches and brakes

Electromagnetic-actuated clutches and brakes Tooth clutches Spring-actuated brake

Input voltage

AC100V/200V

Output voltage

DC24V/45V/90V

BEH

For ultra-high-speed control



RoHS-compliant

Top-of-the-line ultra-high-speed control, high-precision types with built-in overexcitation/reverse excitation functions

Quiet design

There is no excitation noise while operating.

Combination control is easy

Operations that frequently switch clutches and brakes, such as inching, can be performed using only a single input signal.

An array of operating modes

Compatible with a diverse range of applications.

Auto-tuning function

Easy to set for the optimum operating conditions. Causes of problems can also be easily identified using the alarm displays.

Applicable clutches and brakes

Electromagnetic-actuated clutches and brakes Tooth clutches

Input voltage

AC100V/200V

Output voltage

DC24V

BEW For ordinary control



RoHS-compliant

Basic power supply device model for electromagnetic clutch and brake control

Diverse array of specifications

Power supplies are available with a variety of specifications, including half-wave rectified and full-wave rectified.

I Terminal block type

These are of the terminal block type, which allows easy connection, with a DC switching terminal.

I Applicable clutches and brakes

Spring-actuated brake Electromagnetic-actuated clutches and brakes

Input voltage

AC100V/200V/400V

Output voltage

DC45V/90V/180V

BEW-S Compact, light



RoHS-compliant

Power supplies for ordinary control of spring-actuated brakes

Half-wave rectified

Compact, light models with selected functions.

I Terminal block type

These are types with terminal blocks that make connection easy. They are simple power supplies that are set on only the input side and output side.

Applicable clutches and brakes

Spring-actuated brake

Input voltage

AC100V/200V/400V

Output voltage

DC45V/90V/180V

ETP BUSHINGS

ELECTROMAGNETIC

CLUTCHES & BRAKES

BEW-W

For both full- and half-wave rectification



RoHS-compliant

Spring-actuated brakes with different specifications can be handled by a single unit

For both full- and half-wave rectification

Half-wave and full-wave rectified output can be handled by changing the connection method.

Compact, high wattage

Take a wide range of electrical inputs, from low voltage to high.

Terminal block type

These are types with terminal blocks that make connection easy. They are simple power supplies that are set on only the input side and output side.

Applicable clutches and brakes

Spring-actuated brake

Input voltage

AC100V/200V/400V

Output voltage

DC45V/90V/180V

Applicable clutches

Spring-actuated brake

AC100V/200V/400V

Output voltage

DC45V/90V/180V

and brakes

Input voltage

SERIES

ELECTROMAGNETIC-ACTUATED MICRO

ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES

ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BEW-FH

Compact overexcitation power supplies



RoHS-compliant

BEM

Compact, light

Can be set for the outcome you desire: higher operating speed, longer service life, and more

Used as overexcitation supplies

These provide benefits such as super-long (roughly double) service lives and shorter (roughly halved) armature pull-in times for electromagnetic clutches and brakes.

Used as weak excitation supplies

These provide benefits such as lower power consumption (roughly one quarter), suppressed heat generation (roughly one quarter) in the stator (electromagnetic coil), and shorter armature release times.

I Terminal block type

These are of the terminal block type, which allows easy connection, with a DC switching terminal.

Power supplies for ordinary control of spring-actuated brakes

Lead type

These are lead input/output types that are suited to relay connections.

Usable in adverse environments

Since the entire case is molded of resin, they can be used in atmospheres such as dusty locations.

Applicable clutches and brakes

Spring-actuated brake

Input voltage

AC100V/200V/400V

Output voltage

DC45V/90V/180V

BEM-TUltra-compact, light

RoHS-compliant



RoHS-compliant

Power supplies for ordinary control of spring-actuated brakes

L Easy connection

Uses tab terminals on the output side to achieve reductions in connection space and man-hours.

I Mounting freedom

These are compact, slim, and can be installed anywhere. The mountings are also movable, so the input/output direction can be set freely.

Usable in adverse environments

Since the entire case is molded of resin, they can be used in atmospheres such as dusty locations.

Applicable clutches and brakes

Spring-actuated brake

Input voltage

AC100V/200V/400V

Output voltage

DC45V/90V/180V

BES
BEH
BEW
BEW-S
BEW-W
BEW-FH
BEM
BEM-T

BES Models For Ordinary High-speed Control

Specifications

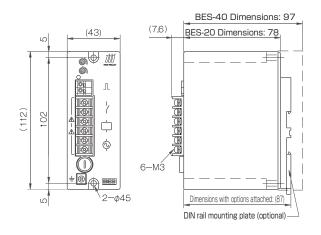
Model	BES-20- □ -1	BES-40- □ -1	BES-20- □	BES-40- □
Input voltage	$AC100V \pm 10$	9% 50/60Hz	AC200V ± 10	0% 50/60Hz
Output current	2.0A	4.0A	2.0A	4.0A
Voltage control system		PWM o	ontrol	
Constant excitation voltage	Adjusted fo	or each model and	size at the time o	of shipment
Overexcitation voltage	DC 90 V (with AC 10	Full-wave 00 V input)		
Overexcitation time	Adjusted fo	or each model and	size at the time of	of shipment
Protective functions		Input side Quicl	k-acting fuse (5A)	
Insulating resistance	DC 500 V With I	Megger 100 M Ω	(between termina	al and main body)
Dielectric strength voltage	AC 1000 V 5	0 Hz 1 min. (bet	ween terminal an	nd main body)
Usage environment	-10 to +	50℃ /10 to 90%R	H (with no conde	nsation)
Mass	0.3kg	0.7kg	0.3kg	0.7kg

 $^{^{}st}$ The voltage that is output is not insulated from the power supply, so shocks can result if touched.

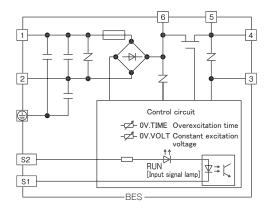
Terminals and Functions

Terminal symbol	Terminal name	Function description
1-2	Power supply input terminal	Connector for a commercial power supply
3-4	Output terminal	Connector for an electromagnetic clutch or brake
5-6	Control terminal 1	Output is controlled by opening and closing between terminals using a relay or the like.
	Ground terminal	External ground terminal (third class ground or more)
S1-S2	Control terminal 2	Output is controlled by turning the DC 24 V on and off (30 mA, smoothing power supply)

Dimensions



Structure



How to Place an Order

BES-20-10-1 DIN

Output current 20:2 A 40: 4 A Refer to the power supply size

Input voltage 1: 100 V AC Blank: 200 V AC

Mounting method DIN: Mounting by DIN mounting rail Blank: Direct mounting *The DIN mounting rail mounting option can only be set for BES-20.

Options (Sets that meet EMC directives)

Equipment can conform to EC directives (for the CE marking) if you also order, using the following model number, a noise filter (one) and ferrite cores (two) as a set to meet EMC directives.

BES-20-EMC

Table of Power Supply/Size Correspondence MIKI PULLEY electromagnetic-actuated clutch/brake size 20 40 Nominal power supply output current Power supply size Excitation voltage For 24 V 25 MIKI PULLEY electromagnetic tooth clutch sizes 23 Nominal power supply output current 20 40 Power supply size Excitation voltage For 24 V 53 MIKI PULLEY spring-actuated brake size 20 Nominal power supply output current Excitation voltage 45/90 V 61 62 63 Power supply size Excitation voltage For 24 V 71 72 73

^{*} The constant excitation voltage for the 45/90 V excitation voltages of spring-actuated brakes is the DC 45 V specification for an input of AC 100 V and the DC 90 V specification for an input of AC 200 V.

Characteristics

Operating Response

All circuits have been made contactless, and response from signal input to output to the electromagnetic-actuated clutch or brake is fast and stable.

Energy Saving

Standby power is "zero." Absolutely no electricity is wastefully consumed.

By combining this power supply with a MIKI PULLEY spring-actuated brake, the electricity consumption and heat generation of the spring-actuated brake is reduced by more than 70%, saving energy.

Noise During Operation

BES models use a quiet design, but electromagnetic clutches and brakes may produce excitation noise when operating under some mounting conditions. This noise is not abnormal and is not cause for concern.

Two Types of Control Systems

You can operate under either PLC control (which uses voltage control via programmable controllers or the like) or contactor control (which controls using relays and the like).

In the case of contactor control, however, a power controller for controlling the power supply line must be used.

■ Supply Voltage Fluctuations and Output Voltage

BES model power supplies are designed to operate reliably even when supply voltage fluctuates. Characteristically, however, their output voltage will rise or fall along with rises and falls of supply voltage. To fulfill electromagnetic clutch/brake performance, supply voltage fluctuations should be kept within a range of $\pm\,10\%$.

Precautions for Use

Circuit Protector

BES models incorporate circuit protectors, so there is no need to connect circuit protectors to the output side (between 3 and 4). Also, since voltage is controlled using PWM, the actual voltage output is the same level as the input voltage. This means that connecting the varistor that comes with 24 V-specification clutches and brakes or the like may result in explosion of the varistor or damage to the power supply. Never connect such devices.

I Protective Functions

BES models contain fuses on the input side. When a fuse engages, the likely cause is a malfunction on the output side.

- Short on output side
- Ground fault on output side
- Malfunction on output side (electromagnetic-actuated clutch/brake) Thoroughly verify that there are no malfunctions on the output side before resuming operation.

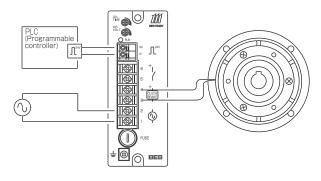
I How to Check Output Voltage Values

If you are checking the output voltage with a voltage meter, tester or the like, check the value with a load such as an electromagnetic clutch or brake connected to the output side.

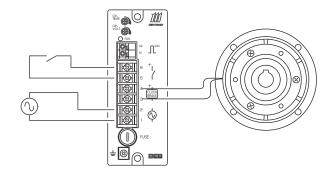
If nothing is connected, it shows a value close to the supply voltage.

Wiring Methods and Timing Charts

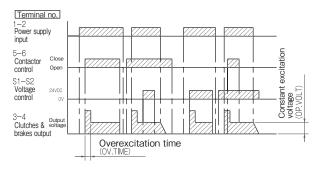
Wiring 1 (PLC Control)



Wiring 2 (Contactor Control)



Time Chart



COUPLINGS

ETP BUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

LINEAR SHAFT DRIVES

TOPOLIE I IMITEDO

ROSTA

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
ELECTROMAGNETICACTUATED
CLUTCHES & BRAKES
CLUTCHES & BRAKES
ELECTROMAGNETICCLUTCHES & BRAKES
CLUTCH & BRAKE
UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS

BES

BEH

.....

BEW-S

BEW-W

BEW-FH BEM

.....

BEM-T

C026

BEH Models For Ultra-high-speed Control

Specifications

Mo	del	BEH-10G	BEH-20G	BEH-20G-1				
	Input voltage		$\text{AC200V} \pm 10\%$	AC100V ± 10%				
Input			Single phase, 50/60 Hz					
	Overexcitation voltage	Initial valu	e 100 V, 0 to 250	V variable				
0	Constant excitation voltage	Initial val	Initial value 24 V, 0 to 250 V variable					
Output voltage	Reverse excitation voltage	Initial value 100 V, 0 to 250 V variable						
	Voltage control system		PWM control					
Output	current	2A	4A	4A				
Applicab	le clutch/	02 ~ 16						
brak	e size	MIKI PULLEY electromagnetic-actuated clutches and brakes Rated voltage DC 24 V						
Protective	functions	Undervoltage protection, overvoltage protection, overcurrent protection/detection, break detection, element overheating protection, input-side fuse (20 A)						
Usage en	vironment	-10 - +50°C / 10 - 90%RH						
Ma	ass	0.85kg	0.9kg	0.9kg				

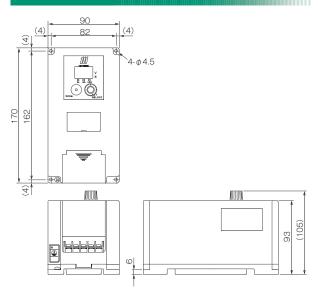
Operating Settings

	g settings SW (SW3) Switch No.	ON (up)	OFF (down)	Settings when shipped	
1	Setup/operating mode	Setup mode	Operation mode	OFF	
2	Stand-alone/ interlocked mode	Stand-alone mode	Interlocked mode	OFF	
3	Break/overcurrent detection	Enabled	Disabled	OFF	
4	Current/voltage control	Current control	Voltage control	OFF	
5	Control AUX	Enabled	Disabled	OFF	
6	Jog operation	Enabled	Disabled	OFF	
7	Slope operation	Enabled	Disabled	OFF	
8	One-shot operation	Enabled	Disabled	OFF	

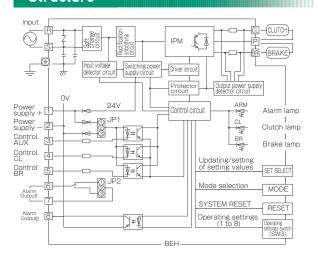
Terminals and Functions

Terminal symbol	Terminal name	Function description
R-S	Power supply input terminal	Connector for a commercial power supply
CL-P	Clutch output terminal	Connector for a clutch
BR-P	Brake output terminal	Connector for a brake
±	Ground	External ground terminal (third class ground or more)
1	Power supply terminal +	Positive terminal of control power supply (shared with the internal supply's +24 V)
2	Power supply terminal -	Negative terminal of control power supply (shared with the internal supply's 0 V)
3	Control AUX	When operating switch 5 (AUX operation) is on, executes the operation of the conditions set in the table.
4	Control clutch	Turns output between P and CL on and off.
5	Control brake	Turns output between P and BR on and off.
6 • 7	Alarm output 1	A relay that operates during an alarm stop (relay output)
8	Alarm output 2	Output operates during an alarm stop (transistor output)

Dimensions



Structure



Characteristics

Operating Response

The circuit construction is completely contactless, and response from signal input to output to the electromagnetic-actuated clutch or brake is fast and stable. The operating speed of the electromagnetic clutch or brake is also increased to the limit speed by the overexcitation and reverse excitation functions.

This is the top-of-the-line model for electromagnetic clutch/brake power supplies. It achieves ultra-high-speed control and high precision.

Noise During Operation

The BEH models are quiet power supplies.

Electromagnetic clutches and brakes normally produce howling sounds during operation. The quiet design of BEH models eliminates such sounds.

Output Control System

You can select either Stand-alone Mode, which controls stand-alone electromagnetic clutches and brakes independently, or Interlocked Mode, which is suited to combination control of electromagnetic clutches and brakes.

There is also a diverse array of other operating modes, such as current control mode and jog mode. These are compatible with a diversity of applications.

Supply Voltage Fluctuations and Output Voltage

BEH models control output voltage to be constant even with a certain amount of supply voltage fluctuation. This ensures stable output even in locations with a bad power supply environment. Variations in electromagnetic clutch/brake response disappear.

However, overly large voltage fluctuations will be sensed as abnormal voltages and set off an alarm. To ensure proper operation, keep supply voltage fluctuation to within a range of \pm 10%.

Precautions for Use

Circuit Protector

BEH models incorporate circuit protectors, so there is no need to connect circuit protectors to the output side (between CL, P and BR). When a circuit protector is included, the alarm goes off and operation stops. Also, since voltage is controlled using PWM, the actual voltage output is the same level as the input voltage. This means that connecting the varistor that comes with 24 V-specification clutches and brakes or the like may result in explosion of the varistor or damage to the power supply. Never connect such devices.

Power Supply Protective Functions

These power supplies are equipped with a variety of protective

These functions also alert the user to the cause of the alarm when the various alarms engage. Thoroughly verify that the cause of the alarm has been cleared and that there are no abnormalities before resuming operation.

I How to Check Output Voltage Values

If you are checking the output voltage with a voltage meter, tester or the like, check the value with a load such as an electromagnetic clutch or brake connected to the output side.

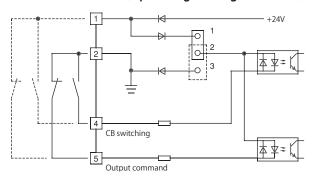
If nothing is connected, the protective functions of break detection engage, and a value around the DC 280 V charged in the capacitor is shown, due to the characteristics of this power supply.

Applicable Ranges and Special Adjustments

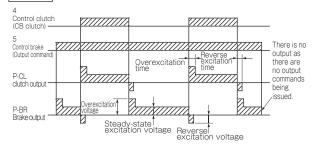
These power supplies can be used as supplies for all electromagnetic coils, not just electromagnetic clutches and brakes. The conducting conditions can be altered freely by changing internal settings. Feel free to consult Miki Pulley regarding settings, operating methods, and the like

Wiring Methods and Timing Charts

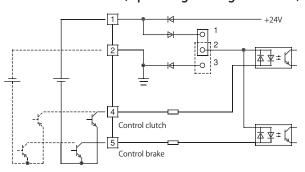
Interlocked Mode (Operating Settings SW-2 Off)



Terminal no. Toggles between the clutch and brake using a single input signal

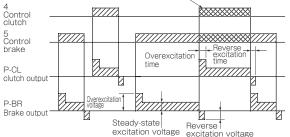


Stand-alone Mode (Operating Settings SW-2 On)



The corresponding clutch/brake operates using the signals Terminal no. received by the input terminals. (Clutches and brakes cannot release output at the same time.)

The priority to determine the order of importance for signals received simultaneously can be set as desired. *The factory default setting is clutch priority.



How to Place an Order



Web code

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES



SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

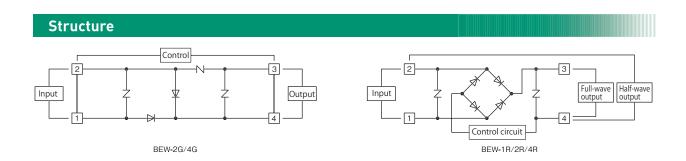
BRAKE MOTORS

POWER SUPPLIES

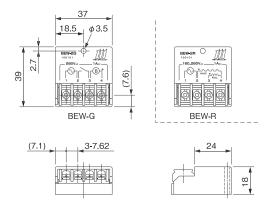
MODELS BES BEH BEW BEW-S BEW-W BEW-FH ВЕМ

BEW Models Supplies with Terminal Blocks for Ordinary Control

Specifications BEW-2R BEW-4R Model BEW-2G BEW-4G BEW-1R AC100V . AC200V 50/60Hz Input voltage AC400V Input voltage range AC 280 V max. AC 480 V max. AC90 ~ 140V $AC180 \sim 280V$ AC360 ~ 480V For both half- and full-wave rectification Rectification method Half-wave rectification Half-wave Full-wave Full-wave Full-wave Output voltage DC45V DC90V DC45V DC90V DC180V DC45V DC90V DC90V DC180V DC180V DC360V When the ambient temperature is 20°C Values in () are for an ambient temperature of 60°C DC1.0A DC1.0A DC2.0A DC1.0A DC0.7A Output current When the ambient temperature is 20°C les in () are for an ambion temperature of 60°C 45W Output 90W 45W 90W 180W 90W 180W 90W 180W 126W 252W Wattage (50W) (100W) (100W) Voltage specification DC45V (AC100V) DC180V (AC400V) DC180V (AC200V) DC180V (AC400V) DC90V DC45V DC90V DC45V DC90V DC90V DC360V Numbers in parentheses are (AC200V) (AC100V) (AC200V) (AC100V) (AC100V) (AC200V) (AC400V) input voltages 02 03 04 05 Applicable 06 Size setting 08 △: Applicable depending 10 on clutch/brake 12 model 14 • 16 Λ 18 20 Λ Λ Λ Λ MIKI PULLEY electromagnetic-Applied actuated clutches and brakes clutches/ Spring-actuated brake All Rated voltage DC 45/90/180 V brakes DC45/90/180V Insulating resistance DC 500 V, 100 M Ω with Megger Between terminal and body Dielectric strength voltage 2000 V AC, 50 Hz, 1 min. 1500 V AC, 50 Hz, 1 min. 2000 V AC, 50 Hz, 1 min. 1500 V AC, 50 Hz, 1 min. Usage environment With no condensation -20 - +60°C Mass Per product 0.04kg



Dimensions



Terminals and Functions

I	Model	Terminal symbol	Terminal name	Function description		
		1-2	Power supply input terminal	Connector for a commercial power supply		
	BEW-G	2-3	Control terminal	Output is controlled by opening and closin between terminals with a relay or other contact		
		3-4	Output terminal	Connector for an electromagnetic clutch or brake		
		1-2	Power supply input terminal	Connector for a commercial power supply		
	BEW-R	2-4	Output terminal (half-wave)	Connector for an electromagnetic clutch or brake (when half-wave rectified)		
		3-4	Output terminal (full-wave)	Connector for an electromagnetic clutch or brake (when full-wave rectified)		

Characteristics

Output System

Two systems are available, half-wave rectified and full-wave rectified. Half-wave rectified takes a commercial power supply as the input and generates a halfwave rectified DC voltage on the output side. These power supply devices are known for their very simple construction and low cost, but their voltage pulse is large. They are therefore prone to generating variations in operating response in electromagnetic clutches and brakes, they produce a howling noise when conducting, and they tend to generate more heat from their electromagnetic coils than full-wave rectified supplies or smoothing supplies.

When the above are to be avoided, consider changing to a full-wave rectified supply, smoothing supply, or a DC 24 V specification.
Full-wave rectified power supply devices are known for having smaller voltage

pulses than half-wave rectified supplies and tending to have little variation in electromagnetic clutch and brake operating response. They can thus be used not just for spring-actuated brakes but also for electromagnetic-actuated clutches and brakes.

Note that when the rated voltage of the electromagnetic coil does not match the voltage output from the power supply device, you will not be able to obtain the electromagnetic clutch/brake characteristics given in the specifications.

Precautions for Use

Circuit Protector

These power supply devices have built-in circuit protectors (varistors) on the input and output sides. There basically is no need, therefore, to install external circuit protectors.

I Primary and Secondary Control Methods

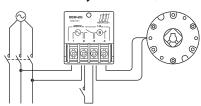
Primary control, which uses on/off of the input voltage to control electromagnetic clutches/brakes (shorting terminals 3-4), saves wiring, but makes the armature release time extremely long, so the braking time of the brake becomes long. (No surge voltage is generated.)

With secondary control (which controls terminals 3-4 with a relay or other contact), armature release time is shorter, as is the braking time of the brake, but there is more wiring and some surge voltages occur. Select primary or secondary control based on the characteristics you desire.

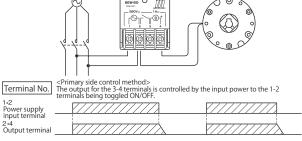
To download CAD data or product catalogs:

Wiring Methods and Timing Charts

BEW-G Secondary Control (Basic Wiring)

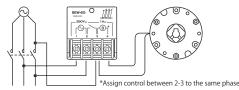


Primary Control (Wire Saving)



Check the above before use as even though the back voltage from the coil will no longer generate when the power supply is toggled ON/OFF, the armature release time will increse.

BEW-G Secondary Control (Wire Saving)

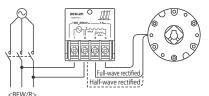


Terminal No.

<Secondary side control method>
The output for the 3-4 terminals is controlled by the input power to the 1-2 terminals being left on and the 2-3 terminals being toggled ON/OFF.

1-2 Power supply input terminal		
2-3		
Output terminal -		
3-4 Control terminal	7//////	

BEW-R **Primary Control**



Terminal no.

The output for the 2-4 terminals(half-wave) or 3-4 terminals(full-wave) is controlled by the input power to the 1-2 terminals being toggled ON/OFF.

Output terminal (half-wave) Output terminal

*The same level of brake responsiveness can be obtained with primary side control as with secondary side control.

How to Place an Order

BEW-2G

Specifications G: Standard R: Relay included Input voltage specifications Rated input 1: 100 V AC

Web code

Rated input 2: 200 V AC Rated input 4: 400 V AC

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES FI FCTROMAGNETIC ACTUATED **CLUTCHES & BRAKES** FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

> SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BES BEH BEW BEW-S BEW-W BEW-FH ВЕМ вем-т

MODELS

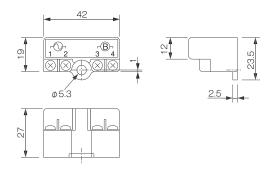
BEW-S Types Compact, Light Supplies with Terminal Blocks

Specificat	tions						
	Model		BEV	V-2S		BEW-4S	
	AC100V		•		•		
	AC200V	± 10% 50/60Hz		•		•	
Input voltage	AC400V						•
	Maximum input vo	ltage	AC2	50V		AC510V	
Rec	tification method				Half-wave rectification		
(Output voltage		DC45V	DC90V	DC45V	DC90V	DC180V
Output current	hen the ambient temper/ Values in () are for an temperature of 6	ambient 60°C			DC1.0A (DC0.6A)		
Output Wattage	hen the ambient temper/ Values in () are for an temperature of 6	ambient	45W (25W)	90W (50W)	45W (25W)	90W (50W)	180W (100W)
	Voltage specifica Numbers in parenthese voltages		DC45V (AC100V)	DC90V (AC200V)	DC45V (AC100V)	DC90V (AC200V)	DC180V (AC400V)
		01	•	•	•	•	•
		02	•	•	•	•	•
		03	•	•	•	•	•
		04	•	•	•	•	•
		05	•	•	•	•	•
Size setting	: Applicable	06	•	•	•	•	•
	: Applicable	08	•	•	•	•	•
	depending on clutch/ brake model	10	•	•	•	•	•
	21410 1110401	12		•		•	•
		14		•		•	•
		16		•		•	•
		18		Δ		Δ	•
		20		Δ		Δ	Δ
		25		Δ		Δ	Δ
Applied lutches/brakes	MIKI PULLEY electror actuated clutches an Rated voltage DC 45/	d brakes	Spring-actuated brake				
sulating resistance	Dahwaan tarmin-1-	nd hady		DC	500 V, 100 M Ω with Megger		
electric strength voltage	Between terminal a	nu boay	1000 V AC,	50 Hz, 1 min.		2000 V AC, 50 Hz, 1 min.	

Dimensions

Usage environment

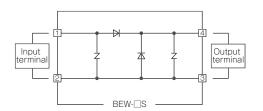
Mass



With no condensation

Per product

Structure



Terminals and functions

-20 ∼ +60°C

0.021kg

Terminal symbol	Terminal name	Function description		
1-2	Power supply input terminal	Connector for a commercial power supply		
3-4	Output terminal	Connector for an electromagnetic clutch or brake		

Characteristics

Output System

BEW-2S/4S types take a commercial power supply as the input and generate a half-wave rectified DC voltage on the output side. These power supply devices are known for their very simple construction and low cost, but their voltage pulse is large. They are therefore prone to generating variations in operating response in electromagnetic clutches and brakes, they produce a howling noise when conducting, and they tend to generate more heat from their electromagnetic coils than full-wave rectified supplies or smoothing supplies.

When the above are to be avoided, consider changing to a full-wave rectified supply (BEW-R types), smoothing supply, or a DC 24 V specification.

How to Calculate Output Voltage Output voltage = Input voltage × a (a set coefficient) * a (set coefficient) = 0.45: half-wave rectification

BEW-2S: AC100V \times 0.45 = DC45V BEW-4S: AC400V \times 0.45 = DC180V

Note that when the rated voltage of the electromagnetic coil does not match the output voltage calculated above, you will not be able to obtain the electromagnetic clutch/brake characteristics given in the specifications.

Precautions for Use

Circuit Protector

(Ex.)

These power supply devices have built-in circuit protectors (varistors) on the input and output sides. There basically is no need, therefore, to install external circuit protectors.

Primary and Secondary Control Methods

These power supply devices use primary control, in which electromagnetic clutches and brakes are controlled by turning input voltage on and off, as their basic control.

This control system saves wiring, but has a longer armature release time than secondary control, extending the braking time of spring-actuated brakes.

This phenomenon becomes more marked the larger the electromagnetic clutch or brake is. Primary control is thus used predominantly on small spring-actuated brakes.

Also, primary control does not generate the surge voltage (counterelectromotive voltage) when the electromagnetic clutch or brake goes off that secondary control does, so it is very effective in machinery when noise must be avoided.

When secondary control is used to improve response, install relay contacts between the output terminals and electromagnetic clutches/ brakes as shown in the wiring diagram at right.

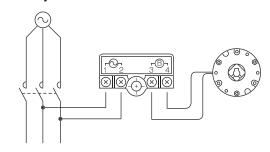
At this time, you must install discharge elements such as varistors between relay contacts or in parallel to the electromagnetic clutch/ brake.

How to Place an Order

BEW-2S Input voltage specifications

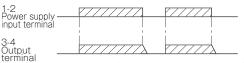
Wiring Methods and Timing Charts

Primary Control



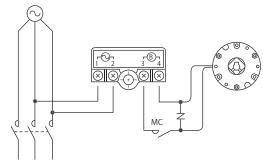
Terminal no.

<< Primary side control method>>
The output for the 3-4 terminals is controlled by the input power to the 1-2 terminals being toggled ON/OFF.

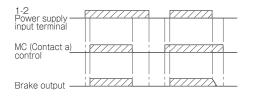


*Check the above before use as even though the surge voltage from the electromagnetic coil will no longer generate when the power supply is toggled ON/OFF, the armature release time will increse.

Secondary Control



Terminal no. | << Secondary side control method>> The brake output is controlled by the input power being input to the 1-2 terminals and the relay being toggled ON/OFF.



COUPLINGS

ETP BUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

TOPOLIE I IMITEDO

ROSTA

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
ELECTROMAGNETICACTUATED
CLUTCHES & BRAKES

ELECTROMAGNETIC
CLUTCH & BRAKE
UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BES
BEH
BEW
BEW-S
BEW-W
BEW-FH
BEM
BEM-T

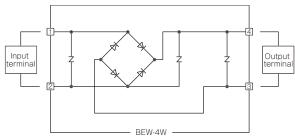
2: Rated input voltage of 200 V AC 4: Rated input voltage of 400 V AC

BEW-W Types Supplies with Terminal Blocks for Both Full- and Half-waves

Specifications BEW-4W Model • AC100V AC200V 50/60Hz Input voltage AC400V AC510V Maximum input voltage For both half- and full-wave rectification Rectification method Full-wave Half-wave Full-wave Half-wave Half-wave Full-wave Output voltage DC45V DC90V DC90V DC180V DC180V DC360V When the ambient temperature is 20°C DC3.0A Values in () are for an ambient temperature of 60°C Output current When the ambient temperature is 20°C 135W 270W 270W 540W 540W 1080W Values in () are for an ambient temperature of 60°C Output Wattage (112W) (225W) (225W) (540W) (540W) (900W) DC45V DC90V DC90V DC180V DC180V DC360V Voltage specification Numbers in parentheses are input voltages (AC 100 V (AC 100 V (AC 100 V (AC 400 V (AC 400 V full-wave half-wave) full-wave) full-wave) half-wave) full-wave) • • 02 • • 03 • • 04 • 05 • 06 • Size : Applicable Settings 08 • • △ : Applicable depending on model of clutch or brake 10 \triangle 12 \triangle • • 14 Δ 16 \triangle • Δ 18 • 20 Λ 25 MIKI PULLEY electromagnetic-actuated Applied clutches and brakes Rated voltage DC 45/90/180 V Spring-actuated brake Insulating resistance DC 500 V, 100 M Ω with Megger Between terminal and body Dielectric strength voltage 2200 V AC, 50 Hz, 1 min. -20 ~ +60°C / 10 ~ 90%RH Usage environment With no condensation

Structure

Per product

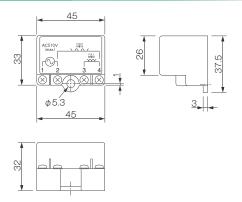


Terminals and Functions

0.045kg

Terminal symbol	Terminal name	Function description
1 - 2	Power supply input terminal	Connector for a commercial power supply
3 - 4	Output terminal	Connector for an electromagnetic clutch or brake

Dimensions



Characteristics

For Both Half-wave Rectified and Full-wave Rectified

For BEW-4W types, you can select between half-wave rectified and fullwave rectified by changing the connections of the wiring as shown in the figure at right.

These power supply devices are high Wattage and allow a wide range of voltage inputs, from low voltage to high. As a result, a wide variety of electromagnetic clutches and brakes can be handled by a single BEW-4W power supply alone.

You can either focus on the type of brake, assuming you will rewire, or conversely, handle a variety of types of brakes with a BEW-4W power supply alone.

How to Calculate Output Voltage

Output voltage = Input voltage \times a (a set coefficient) * a (set coefficient) = 0.45: half-wave rectified/0.9: full-wave rectified

(Ex.)

Half-wave: $AC200V \times 0.45 = DC90V$ Full-wave: $AC100V \times 0.9 = DC90V$

Note that when the rated voltage of the electromagnetic coil does not match the output voltage calculated above, you will not be able to obtain the electromagnetic clutch/brake characteristics given in the specifications.

Precautions for Use

Primary and Secondary Control Methods

These power supply devices use primary control, in which electromagnetic clutches and brakes are controlled by turning input voltage on and off, as their basic control.

This control system saves wiring, but has a longer armature release time than secondary control, extending the braking time of springactuated brakes.

This phenomenon becomes more marked the larger the electromagnetic clutch or brake is. Primary control is thus used predominantly on small spring-actuated brakes.

Also, primary control does not generate the surge voltage (counterelectromotive voltage) when the electromagnetic clutch or brake goes off that secondary control does, so it is very effective in machinery when noise must be avoided.

When secondary control is used to improve response, install relay contacts between the output terminals and electromagnetic clutches/ brakes as shown in the wiring diagram at right.

At this time, you must install discharge elements such as varistors between relay contacts or in parallel to the electromagnetic clutch/

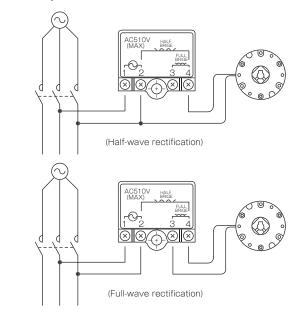
How to Place an Order

To download CAD data or product catalogs:

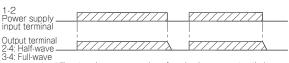
BEW-4W

Wiring Methods and Timing Charts

Primary Control

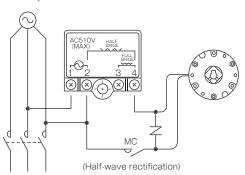


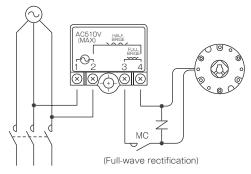
<< Primary side control method>> Terminal no. The output for the 3-4 terminals is controlled by the input power to the 1-2 terminals being toggled ON/OFF.



* There is no longer a surge voltage from the electromagnetic coil when power goes on or off, but armature release time is longer, so confirm this prior to use

Secondary Control





<<Secondary side control method>>
The brake output is controlled by the input power being input to the 1-2 terminals and the relay being toggled ON/OFF. Terminal no.

C030



ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO CLUTCHES & BRAKES FI FCTROMAGNETIC ACTUATED **CLUTCHES & BRAKES** FLECTROMAGNETIC **CLUTCH & BRAKE**

SPRING-ACTUATED BRAKE

UNITS

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS BEH BEW BEW-S BEW-W BEW-FH ВЕМ

BEW-FH Types Overexcitation Supplies that Switch Between Full- and Half-wave

Specifications BEW-1FH BEW-4FH Model BFW-2FH AC100V ± 10% AC200V 50/60Hz Input voltage AC400V Input voltage range AC80 ∼ 130V AC170 ∼ 300V $AC80 \sim 480V$ Overexcitation (full-wave rectified) for 0.5 sec followed by constant excitation (half-wave rectified) Control method Overexcitation Constant excitation Overexcitation Constant excitation Constant excitation Output voltage DC90V DC45V DC180V DC90V DC360V DC180V When the ambient temperature is 20°C Values in () are for an ambient temperature of 60°C DC1.6A (DC1.3A) Constant excitation DC1.6A (DC1.3A) DC1.2A (DC1.0A) Output current Constant excitation Constant excitation When the ambient temperature is 20°C 72W (58W) 144W (117W) 216W (180W) Output Wattage Values in () are for an ambient temperature Constant excitation Constant excitation Constant excitation of 60°C Purpose of use Using overexcitation Using weak excitation Using overexcitation Using weak excitation Using overexcitation Using weak excitation Clutch/brake rated voltage DC45V DC90V DC90V DC180V DC180V • 02 03 • • 04 05 • • • 06 Size Settings • • • 08 Applicable 10 12 • 14 16 18 20 25 MIKI PULLEY electromagnetic-actuated Applied clutches and brakes Spring-actuated brake Rated voltage DC 45/90/180 V DC 500 V, 100 M Ω with Megger Insulating resistance

Structure

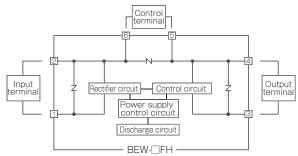
Between terminal and body

With no condensation

Per product

Dielectric strength voltage

Usage environment



Terminals and Functions

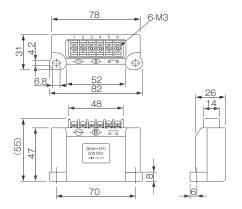
2000 V AC, 50 Hz, 1 min

-20 ∼ +60°C

0.065kg

Terminal symbol	Terminal name	Function description
1-2	Power supply input terminal	Connector for a commercial power supply
3-4	Output terminal	Connector for an electromagnetic clutch or brake
5-6	Control terminal	Output is controlled by opening and closing between terminals with a relay or other contact

Dimensions



Characteristics

Used as Overexcitation Supplies

BEW-FH models go through about 0.5 sec of full-wave rectified output and then transition to half-wave rectified output. BEW-FH power supply devices create an overexcitation state by matching their constant excitation voltage to the rated voltage of the electromagnetic clutch/brake to obtain the following effects.

- Longer electromagnetic clutch/brake service life (about double)
- Shorter armature pull-in time (about half) to achieve high frequency operation
- Longer service life (about double)
- Reduced startup interference by combined use of a spring-actuated brake and a motor

Also, the following effects can also be obtained by determining the specifications of the spring-actuated brake under the assumption that a BEW-FH power supply will be used.

- Higher torque
- Slimmer and more compact

Used as Weak Excitation Supplies

Conversely, BEW-FH power supply devices create a weak excitation state after armature pull-in by matching their overexcitation voltage to the rated voltage of the electromagnetic clutch/brake to obtain the following effects.

- Lower electricity consumption (about 1/4)
- Lower stator (electromagnetic coil) heat production (about 1/4)
- Shorter armature release time

Precautions for Use

Circuit Protector

These power supply devices have built-in circuit protectors (varistors) on the input and output sides. There basically is no need, therefore, to install external circuit protectors.

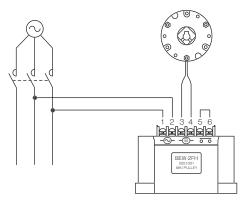
I Primary and Secondary Control Methods

Primary control, which uses on/off of the input voltage to control electromagnetic clutches/brakes (shorting terminals 5-6), saves wiring, but makes the armature release time extremely long, so the braking time of the brake becomes long. (No surge voltage is generated.) With secondary control (which controls terminals 5-6 with a relay or other contact), armature release time is shorter, as is the braking time of the brake, but there is more wiring and some surge voltages occur. Select primary or secondary control based on the characteristics you

Terminals 5-6 are part of the circuit that flows into the brake, so add voltage and current to the considerations when you select relay contacts and the like.

Wiring Methods and Timing Charts

Primary Control

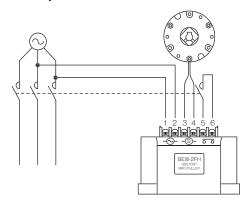


Terminal no. <<Pri>F. 6. to:

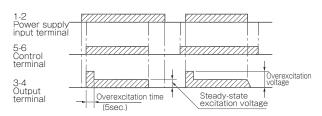
goes on or off, but armature release time is longer, so confirm this prior to use

1-2
Power supply input terminal
5-6
Control terminal
3-4
Output terminal
* There is no longer a surge voltage from the electromagnetic coil when power

Secondary Control



Terminal no. Secondary side control methods The output from the 3-4 terminal is controlled by the input power to the 1-2 terminal being left on and the 5-6 terminal being toggled ON/OFF.



How to Place an Order

BEW-1FH

C031

Input voltage specifications Rated input 1: 100 V AC Rated input 2: 200 V AC Rated input 4: 400 V AC COUPLINGS

ETP BUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

SPEED CHANGERS

INVERTERS

LINEAR SHAFT DRIVES

TOPOLIE I IMITEDO

ROST

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
ELECTROMAGNETICACTUATED
CLUTCHES & BRAKES
ELECTROMAGNETIC
CLUTCHES & BRAKES
CLUTCHES & BRAKES
CLUTCHES & BRAKES

SPRING-ACTUATED BRAKE

UNITS

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

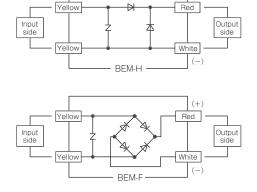
POWER SUPPLIES

BES
BEH
BEW
BEW-S
BEW-W
BEW-FH
BEM
BEM-T

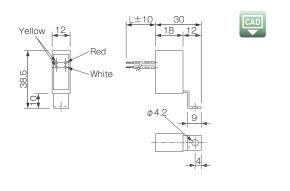
BEM Models Supplies with Compact Leads

	Model	Model BEM-2H BEM-4H			BEM-2F				
	AC100V		•		•			•	
	AC200V	± 10% 50/60Hz		•		•			•
Input voltage	AC400V						•		
	Maximum input voltage		AC2	250V		AC510V	1	AC2	50V
	Rectification method			На	lf-wave rectificat	ion		Full-wave r	ectification
	Output voltage		DC45V	DC90V	DC45V	DC90V	DC180V	DC90V	DC180
Output current	When the ambient tempe Values in () are for a temperature of	n ambient		1.0A 0.6A)		DC1.0A (DC0.6A)			1.0A 0.6A)
Output Wattage	When the ambient tempe Values in () are for a temperature of	n ambient	45W (25W)	90W (50W)	45W (25W)	90W (50W)	180W (100W)	90W (50W)	180W (100W
	Voltage specific Numbers in parenthes voltages		DC45V (AC100V)	DC90V (AC200V)	DC45V (AC100V)	DC90V (AC200V)	DC180V (AC400V)	DC90V (AC100V)	DC180\ (AC200\
		01	•	•	•	•	•	•	•
		02	•	•	•	•	•	•	•
		03	•	•	•	•	•	•	•
		04	•	•	•	•	•	•	•
		05	•	•	•	•	•	•	•
Size setting	• : Applicable	06	•	•	•	•	•	•	•
0.20 0019	\triangle : Applicable depending	08	•	•	•	•	•	•	•
	on clutch/brake model	10	•	•	•	•	•	•	•
		12		•		•	•	•	•
		14		•		•	•	•	•
		16		•		•	•	•	•
		18		Δ		Δ	•	Δ	•
		20		Δ		Δ	Δ	Δ	•
	MIKE BUILT EV. 1.	25		Δ		Δ	Δ	Δ	•
Applied lutches/brakes	MIKI PULLEY electromag clutches and br Rated voltage DC 45	akes	Spring-actuated brake			ake			
ulating resistance	Between terminal a	and hody			DC 500	V, 100 M Ω with	Megger		
ectric strength voltage	Detricen terminat o	300,	1500 V AC,	50 Hz, 1 min.	220	0 V AC, 50 Hz, 1 r	min.	1500 V AC, 5	50 Hz, 1 min

Structure



Dimensions



Terminals and Functions

Lead color	Function name	Function description
Yellow (two)	Input side	Connector for a commercial power supply
Red/white	Output side	Connector for an electromagnetic clutch or brake

Characteristics

■ For Both Half-wave Rectified and Full-wave Rectified

BEM-2H/4H types take a commercial power supply as the input and generate a half-wave rectified DC voltage on the output side. These power supply devices are known for their very simple construction and low cost, but their voltage pulse is large. They are therefore prone to generating variations in operating response in electromagnetic clutches and brakes, they produce a howling noise when conducting, and they tend to generate more heat from their electromagnetic coils than full-wave rectified supplies or smoothing supplies.

When the above are to be avoided, consider changing to a full-wave rectified supply (BEM-2F types), smoothing supply, or a DC 24 V specification.

BEM-2F types generate a full-wave rectified DC voltage. These power supply devices are known for having smaller voltage pulses than half-wave rectified supplies and tending to have little variation in electromagnetic clutch and brake operating response.

How to Calculate Output Voltage

Output voltage = Input voltage × a (a set coefficient)
* a (set coefficient) = 0.45: half-wave rectified/0.9: full-wave rectified

(Ex.)

BEM-2H, -4H: 200 V AC \times 0.45 = 90 V DC BEM-2F: AC100V \times 0.9 = DC90V

Note that when the rated voltage of the electromagnetic coil does not match the output voltage calculated above, you will not be able to obtain the electromagnetic clutch/brake characteristics given in the specifications.

Precautions for Use

Primary and Secondary Control Methods

These power supply devices use primary control, in which electromagnetic clutches and brakes are controlled by turning input voltage on and off, as their basic control.

This control system saves wiring, but has a longer armature release time than secondary control, extending the braking time of springactuated brakes.

This phenomenon becomes more marked the larger the electromagnetic clutch or brake is. Primary control is thus used predominantly on smaller spring-actuated brakes.

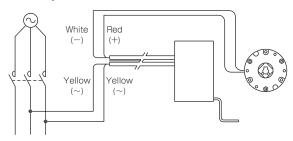
Also, primary control does not generate the surge voltage (counterelectromotive voltage) when the electromagnetic clutch or brake goes off that secondary control does, so it is very effective in machinery when noise must be avoided.

When secondary control is used to improve response, install relay contacts between the output terminals and electromagnetic clutches/ brakes as shown in the wiring diagram at right.

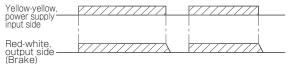
At this time, you must install discharge elements such as varistors between relay contacts or in parallel to the electromagnetic clutch/ brake.

Wiring Methods and Timing Charts

Primary Control

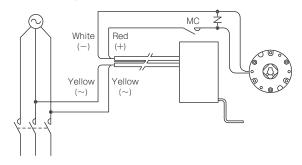


Lead wires << Primary side control method>>
The output for the (red/white) output lead wire is controlled by the input power to the (yellow) input lead wire being toggled ON/OFF.

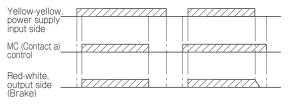


* There is no longer a counterelectromotive voltage from the electromagnetic coil when power goes on or off, but armature release time is longer, so confirm this prior to use.

Secondary Control



Lead wires
Secondary side control method>>
The brake output is controlled by the input power being input to the (yellow) input lead wire and the relay being toggled ON/OFF



COUPLINGS

ETP BUSHINGS

ELECTROMAGNETIC
CLUTCHES & BRAKES

& REDUCERS

INVERTERS

LINEAR SHAFT DRIVE

TOROLIE LIMITERS

ROST

SERIES

ELECTROMAGNETICACTUATED MICRO
CLUTCHES & BRAKES
FLECTROMAGNETIC-

ACTUATED
CLUTCHES & BRAKES
ELECTROMAGNETIC

CLUTCH & BRAKE UNITS

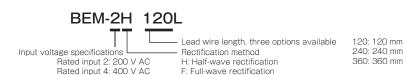
SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

How to Place an Order

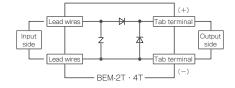


MODELS

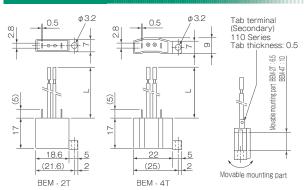
BEM -T Types Supplies with Ultra-compact Leads

	Model		BEN	1-2T		BEM-4T			
	AC100V		•		•				
	AC200V	± 10%		•		•			
Input voltage	AC400V	50/60Hz					•		
	Maximum input voltage		AC2	80V		AC480V			
	Rectification method				Half-wave rectification	ı			
	Output voltage		DC45V	DC90V	DC45V	DC90V	DC180V		
Output current	When the ambient ten Values in parentheses a temperature	are for an ambient	DC1.0A	(DC0.6A)		DC0.7A (DC0.5A)			
Output Wattage	When the ambient ten Values in parentheses a temperature	are for an ambient	45W (25W)	90W (50W)	30W (20W)	60W (40W)	125W (90W)		
	Voltage speci Figures in parentheses		DC45V (AC100V)	DC90V (AC200V)	DC45V (AC100V)	DC90V (AC200V)	DC180V (AC400V)		
		01	•	•	•	•	•		
		02	•	•	•	•	•		
		03	•	•	•	•	•		
		04	•	•	•	•	•		
		05	•	•	•	•	•		
Size setting	: Applicable	06	•	•	•	•	•		
	∴ : Applicable depending on clutch or brake model	08	•	•	•	•	•		
	ctuter of brake model	10	•	•	•	•	•		
		12		•		•	•		
		14		•		Δ	•		
		16		•		Δ	•		
		18		Δ.		Δ.			
		20		Δ		Δ	Δ		
Applied utches/brakes	MIKI PULLEY electrom clutches and Rated voltage DC	brakes		Δ	Spring-actuated brake	Δ	Δ		
ılating resistance				DC 5	500 V, 100 M Ω with Me	egger			
ctric strength voltage	Between termin	al and body	1500 V AC, 50 Hz, 1 min.		2	2000 V AC, 50 Hz, 1 min			

Structure



Dimensions



Terminals and Functions

Terminal Function name		Function description
Leads (two)	Input side	Connector for a commercial power supply
Tab terminals (two locations)	Output side	Connector for an electromagnetic clutch or brake

Recommended Products for the Tab Terminal Partner Side

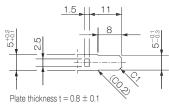
 Receptacle 	170043-1	(made by AMP)
 Insulation sleeve 	170823-1	(made by AMP)
• ICT insulation-covere	d terminal, FA	type, 110 series
• ICTDEN	280509-FA	(made by Nichifu)
• Flat insertion terminal	CSS 62853-F	(made by Nichifu)
 Insulation cap 	62826-F	(made by Nichifu)

Design of Mounting Part

The standard mounting feet can not only be moved, they can be removed and a dedicated mount used. Design using the following figure as a guide or consult Miki Pulley.



Recommended mounting dimensions



Characteristics

Output System

BEM-2T/4T types take a commercial power supply as the input and generate a half-wave rectified DC voltage on the output side. These power supply devices are known for their very simple construction, compact size, and low cost, but their voltage pulse is large. They are therefore prone to generating variations in operating response in electromagnetic clutches and brakes, they produce a howling noise when conducting, and they tend to generate more heat from their electromagnetic coils than full-wave rectified supplies or smoothing supplies.

When the above are to be avoided, consider changing to a full-wave rectified supply (BEM-2F types), smoothing supply, or a DC 24 V specification.

How to Calculate Output Voltage Output voltage = Input voltage × a (a set coefficient) * a (set coefficient) = 0.45: half-wave rectification (Ex.)

BEM-2T: $AC200V \times 0.45 = DC90V$

Note that when the rated voltage of the electromagnetic coil does not match the output voltage calculated above, you will not be able to obtain the electromagnetic clutch/brake characteristics given in the specifications.

Precautions for Use

Primary and Secondary Control Methods

These power supply devices use primary control, in which electromagnetic clutches and brakes are controlled by turning input voltage on and off, as their basic control.

This control system saves wiring, but has a longer armature release time than secondary control, extending the braking time of spring-actuated brakes.

This phenomenon becomes more marked the larger the electromagnetic clutch or brake is. Primary control is thus used predominantly on smaller spring-actuated brakes.

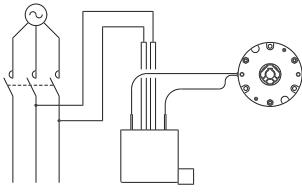
Also, primary control does not generate the surge voltage (counterelectromotive voltage) when the electromagnetic clutch or brake goes off that secondary control does, so it is very effective in machinery when noise must be avoided.

When secondary control is used to improve response, install relay contacts between the output terminals and electromagnetic clutches/brakes as shown in the wiring diagram at right.

At this time, you must install discharge elements such as varistors between relay contacts or in parallel to the electromagnetic clutch/ brake.

Wiring Methods and Timing Charts

Primary Control



<< Primary side control method>>
The output for the tab terminal on the output side is controlled by the input power to the input lead wire being toggled ON/OFF.

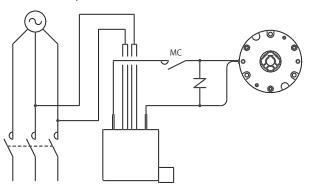
Lead wire, power supply input side

Tab terminal, output side

(Brake) **Check the above before use as even though the back voltage from the content of the

*Check the above before use as even though the back voltage from the electromagnetic coil will no longer generate when the power supply is toggled ON/OFF, the armature release time will increse.

Secondary Control



<<Secondary side control method>>
The brake output is controlled by the input power being input

to the input lead wire and the relay being toggled ON/OFF

Lead wire, power supply input side

MC (Contact a) control

Brakes

How to Place an Order

BEM-2T 120L

Lead wire length, three options available
Input voltage specifications 2T: 200 V AC 240: 240 mm
4T: 400 V AC 360: 360 mm

COLIPLINGS

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CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS
BES
BEH
BEW
BEW-S
BEW-W
BEW-FH
BEM
BEM-T

C033

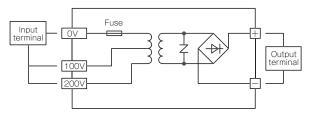
Types of Power Supply Devices

Power supply devices are necessary for electromagnetic clutches and brakes to operate. MIKI PULLEY's electromagnetic clutches and brakes all use DC power supply coils, so commercial power supplies must be converted to DC voltages by any one of a variety of methods and that voltage then supplied to the clutch or brake.

There are many ways to create a DC power supply voltage. The operating characteristics of the electromagnetic clutch and brake are greatly affected by the type and specifications of that power supply device.

Transformer Stepdown/Single-phase Fullwave Rectified System

This is the most commonly used system for power supplies for electromagnetic clutches/ brakes. This system is used with DC 24 V electromagnetic clutches/brakes, has a simple, sturdy construction, and has major resistance to surge voltages (counterelectromotive voltage) that are produced when electromagnetic clutches/brakes are turned on or off, making this a rectification system that is very easy to work with.

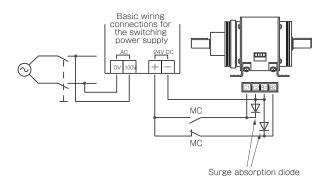


Switching Power Supplies (Off-the-shelf)

These are widely used as power supplies (usually DC 24 V) for relays, timers, programmable controllers, and a variety of other electrical equipment. They are light, compact power supply devices that generate smoothed, stable

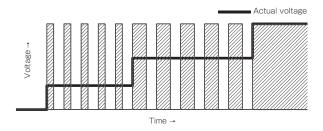
However, these power supplies are characteristically vulnerable to surge voltages generated when electromagnetic coils like those found in electromagnetic clutches and brakes turn on and off. Manufacturers of switching power supplies do not guarantee them for use in such applications. If you are using a switching power supply as the power supply device for an electromagnetic clutch or brake, you must connect a diode to serve as a surge absorber in parallel to the electromagnetic coil.

Surge absorbing diodes dramatically lengthen the armature release time, so care is advised in their use.



The PWM Control System

Repeatedly turning energization on and off is a system that creates a simulation of a given voltage as the effective value. Compared to the wasting of surplus electrical energy as heat in resistance control or the like, PWM control saves energy by turning energization on and off at high speed with control elements to get only the power needed, meaning that energy is not wasted as heat.



Half-wave Rectified Supplies (BEW and **BEM Models**)

Half-wave rectified power supply devices are circuits that contain two diodes, take commercial power supplies as direct input, and generate half-wave rectified DC voltage on the output side.

These power supply devices have very simple circuit structures compared to other power supply devices, and they are compact and

However, they produce variations of around 10 ms in electromagnetic clutch/brake operation due to the energizing system, which repeatedly starts and stops in a cycle of half of 50/60 Hz, the frequency of commercial power supplies. They are also prone to producing a howling noise when they are energized, and tend to generate more heat from their electromagnetic coils than full-wave rectified supplies or smoothing supplies.

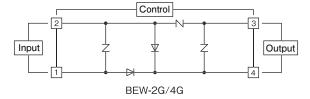
This means they can be used when these trends will not have a major impact, in the event they occur. Miki Pulley recommends the use of half-wave rectified supplies in combination with spring-actuated

When variations in operation, howling noise when energized, and the like are to be avoided, consider changing to a full-wave rectified supply (BEW-1R/2R/4R types) or a DC 24 V specification.

Calculating the Output Voltage from a Half-wave **Rectified Power Supply**

Output voltage = Input voltage \times a (a set coefficient) * a (set coefficient) = 0.45: half-wave rectification (Ex.)

AC100V DC45V 0.45 = AC200V × 0.45 = DC90V **AC400V** × 0.45 = **DC180V**



Full-wave Rectified Supplies (BEW and **BEM Models**)

Full-wave rectified power supply devices are circuits that contain four diodes, take commercial power supplies as direct input, and generate full-wave rectified DC voltages on the output side.

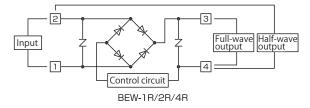
These power supplies are somewhat more expensive than half-wave rectified supplies, since they use more diodes to construct circuits, but they keep voltage pulses low, so they can suppress variation in electromagnetic clutch/brake operating times.

They can therefore be used as power supply devices for all electromagnetic clutches and brakes.

Calculating the Output Voltage from a Full-wave **Rectified Power Supply**

Output voltage = Input voltage \times a (a set coefficient) * a (set coefficient) = 0.9: full-wave rectification (Ex.)

AC100V DC90V × 0.9 =**AC200V DC180V** × 0.9 =



Overexcitation Supplies (BES, BEH, and **BEW-FH Models**)

Overexcitation power supplies are power supply devices that apply and control voltage above the rated voltage for a certain set period of time with the goal of speeding up the armature pull-in time of electromagnetic clutches and brakes, boosting the torque generated, and lengthening service life (electromagnetic-actuated clutches/ brakes).

By using these power supplies, the above described electromagnetic clutch and brake characteristics are notably improved.

Caution is advised, however, because if the conducting frequency and time of the electromagnetic clutch/brake are not set appropriately, the coil of the electromagnetic clutch/brake will generate abnormal heat, potentially leading to damage.

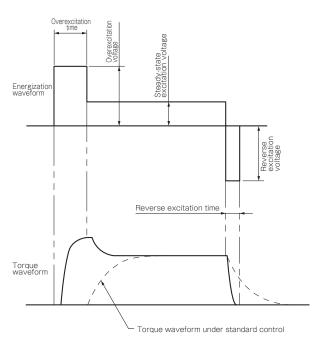
Reverse Excitation Function (BEH Models)

The reverse excitation function is a conductance system that, when energization to the electromagnetic clutch/brake is turned off, applies and controls, for a certain set period of time, a voltage of opposite polarity to the voltage just prior to energization going off, with the goal of shortening the armature release time of electromagnetic clutch/brake.

These power supply devices are more effective the larger the electromagnetic clutch or brake is. With our clutch/brake size 25, it achieves five times the responsiveness of an ordinary transformer stepdown/single-phase full-wave rectified system.

This is a big help in improving high-frequency operation and fighting phenomena.

- * MIKI PULLEY overexcitation power supply devices are pre-set to optimal values. They are pre-set to the optimal value for the given size of MIKI PULLEY electromagnetic clutch or brake, so no special adjustments are needed when installing. If you are not combining the power supply with a MIKI PULLEY electromagnetic clutch/brake, these are not optimal value conditions. Please consultMiki Pulley.
- * BEH models are smoothing overexcitation power supply devices. BEH models, which are smoothing power supplies, have very stable electromagnetic clutch/brake operating response characteristics compared to non-smoothed supplies.



Weak Excitation Supplies (BES and BEW-FH Models)

In recent years, the dimensions of electromagnetic coils and structural components have become more complex and capacities larger to meet demands for spring-actuated brakes that are more compact, slimmer, and provide higher torque.

Directly opposing societal demands for greater energy savings, greater recyclability, and avoidance of toxic materials have meanwhile created a challenging environment for electromagnetic clutches and brakes.

Spring-actuated brakes by their nature require a strong attraction force when the armature is being pulled in, but once they are pulled in, can be held in place with only a tiny amount of power.

Power beyond that required to maintain the spring-actuated brake in a released state can be considered wasted power; spring-actuated brakes waste very large amounts of such power.

Weak excitation power supplies remedy this problem of springactuated brakes and achieve the following sorts of effects.

Miki Pulley can design many types of both spring-actuated brakes and power supply devices to resolve such problems. Do not hesitate to consult us.

Compact, slim, high torque, high responsiveness, and long service life

A compact, slim, high-torque, and highly responsive spring-actuated brake with a long service life is achieved by designing the brake assuming that it will use a weak excitation power supply.

Energy saving

By creating a weak excitation state, they cut ordinary power by more than 90% while similarly reducing heat generated by electromagnetic coils by more than 90%.

Reducing the fault rate

They dramatically reduce burning of spring-actuated brakes caused by abnormal heat generation in electromagnetic coils or rises in ambient temperature, as well as burning in the periphery of spring-actuated brakes.

Increasing recyclability

They can be broken down into their constituent raw materials, increasing the recyclability of structural components.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

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FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS BES BEH BEW BFW-S BEW-W BEW-FH ВЕМ

Control of Electromagnetic Clutches and Brakes

Power supply devices are what is required to make electromagnetic clutches and brakes work, but control devices are necessary for freely controlling electromagnetic clutches and brakes consistent with machinery operation, so this portion must be installed separately.

Miki Pulley's BEH models, which are high-performance power supplies, get minute control input from programmable controllers or the like and perform high-Wattage energization control.

However, other power supply devices are constructed so that the power applied to the electromagnetic clutches and brakes is applied unaltered to control contacts or the like, meaning that power relays and other power control equipment is needed for control.

Each piece of control equipment has its own features, so those features must be adequately studied and control equipment selected that is matched to the machinery specifications.

Power Relays (Off-the-shelf)

There are relays that can control relatively large currents up to 10 A, which are generally called power relays.

These relays guarantee power control of high voltage and current values for AC power supplies, but in DC power supply control, they must be used within extremely low specification value ranges when the load is a DC inductive load.

This is because relay contacts are heavily worn by surge voltage (counterelectromotive voltage) generated during electromagnetic coil control. Since electromagnetic clutches and brakes have electromagnetic coils, check the catalog specification values at the conditions of the DC inductive load of the power relay you will use. General guideline values are given below.

For LY series, made by Omron

Primary Control of Electromagnetic Clutches and

AC voltage: AC 110 V (no more than the maximum AC 250 V)

AC current: AC 4 A max. Wattage: 100W max.

Secondary Control of Electromagnetic Clutches and

DC voltage: DC 24 V (no more than the maximum DC 125 V)

DC current: DC 1 A max. 25W max. Wattage:

- * Secondary control values are for when a MIKI PULLEY varistor is used
- The above values must be within the specification value ranges for all three items
- * For primary and secondary control, see the control wiring of the individual model of power supply.
- * When diodes are used as discharge elements, the specification values of primary control are al lowed even with secondary control

Electromagnetic Contactors (Off-the-shelf)

Electromagnetic contactors and electromagnetic switches, which are widely used in control of induction motors and the like, are very effective as control equipment for controlling large electromagnetic clutches and brakes.

These electromagnetic contactors can control several times as much voltage and current as power relays, and are particularly effective in high-voltage control.

Electromagnetic contactors are suited to high-power control, but a discharge element such as a varistor must be added for surge voltages (counterelectromotive voltages) generated when controlling electromagnetic clutches and brakes.

Were one to control a large electromagnetic clutch or brake without using a discharge element, the surge voltage generated might exceed 2000 V. This voltage easily exceeds the rated voltage of the electromagnetic contactor, ultimately greatly wearing the contacts, which is likely to prevent the equipment from having its expected

General guideline values are given below.

For SC series, made by Fuji Electric

Primary Control of Electromagnetic Clutches and Brakes

AC voltage: AC 220 V (no more than the maximum AC 440 V)

AC current: AC 3 A max. Wattage: 450 W max.

Secondary Control of Electromagnetic Clutches and Brakes

DC voltage: DC 220 V max. DC current: DC 2 A max. Wattage: 150W max.

- Secondary control values are for when a MIKI PULLEY varistor is used.
- * The above values must be within the specification value ranges for all three items.
 * For primary and secondary control, see the control wiring of the individual model of power supply.
- * When diodes are used as discharge elements, the specification values of primary control a lowed even with secondary control.

Solid State Relays/SSR (Off-the-shelf)

SSRs used in control of the various load devices are highly suited to control by programmable controller. In recent years, their use has continued to grow. Most SSRs are intended for control of AC supplies; 80% of SSRs on the market are for AC power supply control.

When using an AC control SSR for an electromagnetic clutch/brake, the input voltage (which is the primary side of the power supply device) is controlled.

The "zero cross control" used in SSR control slows response when used with primary control, so be careful when using it with electromagnetic clutches and brakes.

Maximum rated voltage is a very important specification with DC supply control SSRs.

When controlling an electromagnetic clutch or brake with a DC SSR, the surge voltage generated must be kept within the SSR rating. In other words, a discharge element such as a varistor or diode must be

If no discharge element is added, the SSR will be damaged in a short time. For details, contact the SSR manufacturer or Miki Pulley.

Contactless Control (Power MOS-FET/Power Transistor)

The major goals of contactless control of electromagnetic clutches and brakes are high-frequency operation and high-precision operation.

Such control is suited to cases in which delay of output vis-a-vis input signals, as happens with control using contacts, is undesirable. It offers major advantages such as the doing away with the need for wearrelated maintenance and the ability to make devices smaller by making a control board.

Although contactless control has these many advantages, caution is advisable when selecting elements. Should a selection be made badly, not only will the electromagnetic clutch or brake not deliver the desired characteristics, the elements will be damaged in a short period of time, and peripherals could even be affected.

The following serves as a general guide for selecting elements.

Control of selection example 101-12-13 and an ordinary switching supply

Conditions

Clutch used: 101-12-13 Rated voltage: DC 24 V Rated current: DC 1.09 A

Varistor used: 82 V varistor (TNR7V820K)

Elements selected

• Rated voltage: 200 V min. • Rated current: 5 A min.

■ Key selection issues

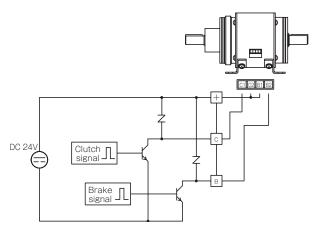
The rated voltage of the element must be at least the highest voltage applied to the element.

In the above example, the surge voltage generated when the electromagnetic clutch or brake is controlled by on/off is the highest value.

Varistors have variation in clamping voltages due to their operating characteristics, and a maximum clamping voltage is defined. Under these element conditions (82 V elements), that value is 135 V.

A safety factor for this voltage is required for the element. With a minimum safety factor of 1.3, 135 V \times 1.3 = 175.5 V. Thus, the rated voltage of the element must be at least 200 V.

The rated current of the element must be at least three times the current value actually flowing. Also, the amount of heat generated by the element varies considerably with the type of element selected, energizing conditions, and ambient environment. In the end, evaluate the heat generation of the element under usage conditions, and check whether the amount of heat generated is within the specified value range of the element.



Other Control

■ Current control (electromagnetic-actuated clutches and brakes)

This control system is intended for torque control of electromagnetic clutches and brakes.

Electromagnetic clutches and brakes generate attraction force using the current flowing into the electromagnetic coil and transmit torque using that attraction force. The value of the current flowing into the electromagnetic coil must therefore be controlled in order to control

Miki Pulley offers power supply devices for performing this current control. Feel free to consult Miki Pulley.

■ Voltage control

There are many different purposes to voltage control, and many different ways to implement that control. All of the following are voltage controls.

• Weak excitation control

Simple torque control (using voltage regulation)

Softens shocks upon engagement

Speeds up armature release

Suppresses heat generation in electromagnetic coils

Overexcitation control

Shortens armature pull-in time

Boosts torque

• Rapid excitation control Shortens armature pull-in time

· Rapid overexcitation control

Shortens armature pull-in time Boosts torque

To implement the control described above, the power supply voltage must be set to a prescribed state and some kind of control performed.

- Switching control, preparing several types of supply voltage
- · Control of voltage using knob
- Switching control without using contacts
- Voltage control that inserts resistors in series to divide voltage

■ Rapid excitation control

This is a circuit that makes the time constant smaller to speed up the armature pull-in time of the electromagnetic clutch or brake.

The circuit places resistors in series with the electromagnetic clutch/ brake and pre-sets the power supply voltage high. The supply voltage and the resistance values are set according to various conditions so that DC 24 V, which is the rated voltage, is applied to the electromagnetic coil.

This control method requires that a current similar to the current value flowing to the electromagnetic clutch/brake also flow to the resistors and that the resistance Wattage be set high. The heat generated by the resistors must also be considered.

The time constant exhibits the characteristic that the value of the current flowing inward gradually rises as DC voltage is applied, since the electromagnetic clutch or brake is an inductive load This characteristic has a value determined by the type and size of the electromagnetic clutch or brake, such that the larger the object, the slower the current movement becomes.

Rapid overexcitation control

The armature pull-in time can be made even shorter than with rapid excitation control by adding a large capacitor to the rapid excitation circuit.

An overexcitation voltage is generated by the capacitor, so the on/off times must be set factoring in the heat generated by the electromagnetic coil and the time to charge the capacitor.

ETP BUSHINGS

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

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FI FCTROMAGNETIC **CLUTCH & BRAKE** UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

BES BEH BEW

BFW-S

MODELS

BEW-W

BEW-FH ВЕМ

вем-т

Surge Voltages and Discharge Elements

What is Surge Voltage?

When current flows to the electromagnetic coil of an electromagnetic clutch or brake, the coil is excited, the pull-in force required by the clutch or brake is generated, and work is performed.

Energy is accumulated within the coil, which has reached the prescribed current value; the larger the clutch or brake size, the larger is the amount of that energy. At this time, if current is shut off, a surge voltage of only part of the accumulated energy is generated. This is generated by working to keep current flowing, since the electromagnetic clutches and brakes are inductive loads. Surge voltages are larger with larger sizes, as noted above, and voltages easily exceeding 1000 V are generated in control contacts and within electromagnetic coils. This phenomenon can cause contact burning or electromagnetic coil insulation breakdown. It is thus very important to use discharge elements to limit this surge voltage to an appropriate value.

In general, a high surge-limit voltage means a short armature release time; conversely, a low limit voltage tends to mean a longer time. When selecting a circuit protector, it is very important to factor in machinery specifications, power supply device/control circuit conditions, and the like.

The Role of Varistors

We recommend using a varistor for the discharge element.

The reason is that it is easy to set the limit voltage needed for the varistor to appropriately control the electromagnetic clutch/brake; the element is also very small and can adequately handle different amounts of surge energy.

By selecting an appropriate varistor, the electromagnetic clutch/brake can be used without impairing innate characteristics.

When the selection has an inappropriately high limit voltage, control contact may be burned or the power supply device damaged.

Conversely, when the limit voltage is too low, the varistor may be burned by the power supply device or the power supply device may be damaged. Also, even when such phenomena do not occur, the armature release time is prone to becoming long.

Types of Discharge Elements

	Clutch/brake		Clutch/brake				
Element type	Circuit diagram	Current decay	Characteristics	Size	Rated voltage (input voltage specification)	Recommended product	
				Electromag- netic-actuated #02 to #25	DC24V	NVD07SCD082 or an equivalent (NVD14SCD082 or an equivalent)	
				Electromag- netic-actuated #31 or over	DC24V	NVD14SCD082 or an equivalent	
					DC24V	NVD07SCD082 or an equivalent	
			Very effective in	Spring-	DC 45 V (AC 100 V - half- wave rectified) DC 90 V (AC 100 V - full- wave rectified)	NVD07SCD220 or an equivalent	
	+ O MC	1111111	keeping surge voltage small	actuated #01 to #18	DC 90 V (AC 200 V - half- wave rectified)		
Varistor			without adding delay to the		DC 180 V (AC 200 V - full- wave rectified)	NVD07SCD470 or an equivalent	
	VR Z (C/B)		armature release time.		DC 180 V (AC 400 V - half- wave rectified)	NVD14SCD820 or an equivalent	
	-0	1111111			DC24V	NVD14SCD082 or an equivalent	
				Spring- actuated #20 or over	DC 45 V (AC 100 V - half- wave rectified) DC 90 V (AC 100 V - full-	NVD14SCD220 or an equivalent	
					wave rectified) DC 90 V (AC 200 V - half- wave rectified)		
					DC 180 V (AC 200 V - full- wave rectified)	NVD14SCD470 or an equivalent	
					DC 180 V (AC 400 V - half- wave rectified)	NVD14SCD820 or an equivalent	
	+ O MC R D (C/B)		Can keep power consumption of the power supply part low and resistor Wattage low. The armature release time becomes somewhat longer, so care is required in high frequency use.	ow e #01 to #25 es to	DC24V	☐ Rated voltage of diode • DC 24 V: 100 V min.	
Resistor					DC 45 V (AC 100 V - half-wave)	 AC 100 V: 400 V min. AC 200 V: 800 V min. 	
+					DC 90 V (AC 100 V - full-wave)	☐ Rated current of diode • Specification of excitation	
Diode					DC 90 V (AC 200 V - half-wave)	current or more	
					DC 180 V (AC 200 V - full-wave)	 About 10 times coil resistance 	
	MC	II I I I I I I I	While the effect in suppressing surge voltage		DC24V	☐ Rated voltage of diode	
	+ 0 100		is very high, the armature release time becomes		DC 45 V (AC 100 V - half-wave)	DC 24 V: 100 V min. AC 100 V: 400 V min.	
Diode	D A C(B)		extremely long. Pay attention to high-frequen-	#01 to #25	DC 90 V (AC 100 V - full-wave)	• AC 200 V: 800 V min.	
	T Y		cy specifications and fighting between clutches		DC 90 V (AC 200 V - half-wave)	Specification of excitation current or more	
	-0	t	and brakes.		DC 180 V (AC 200 V - full-wave)	. Current or more	
	MC		Although armature		DC24V	Capacitor C [μ F]: Ratio to contact	
Resistor	+0		release time becomes very		DC 45 V (AC 100 V - half-wave)	current is: $\frac{C \left[\mu F \right]}{L \left[\mu F \right]} = \frac{0.5 \sim 1}{1}$	
+	R [] L		short, a high-break- down-voltage	je #01 to #25	DC 90 V (AC 100 V - full-wave)	I [A] $\stackrel{-}{}$ 1 Breakdown voltage: 600 [V] Resistance R [Ω]: Ratio to contact	
Capacitor	† °		capacitor must be used and the		DC 90 V (AC 200 V - half-wave)	Resistance $R[\Omega]$: Ratio to contact current is: $R[\Omega]$	
	-0	$ \Psi _{t}$	device becomes large.		DC 180 V (AC 200 V - full-wave)	$\frac{ V }{ E V } = 1$ Wattage = 1 [W]	

^{*} Recommended varistors with NVD
model names are made by KOA. Items in parentheses are the products that can be used.

Symbols Used in Electrical Circuits

I Figure Notations

With rapid advances in science and technology, many new codes and symbols have been adopted in drawings. The drawing symbols below have been created based on JIS handbooks and code and on drawing symbol handbooks primarily for machinery and elements that have long been widely used. The IEC standard or commonly used symbol is labeled Symbol 1; previously used symbols are labeled Symbol 2,

	Sym	bol		Symbol		
Name	Symbol 1 (IEC or equivalent)	Symbol 2 (old symbol)	Name	Symbol 1 (IEC or equivalent)	Symbol 2 (old symbol)	
DC power supply	-		Motor	M		
AC power supply			Induction motor	M 3~		
Fuse			Generator	G		
Relay a-contact	\		Electromagnetic clutch	<u>—©</u> —		
Relay b-contact	<u> </u>	ļ - <u></u>	Electromagnetic brake	B		
Pushbutton switch a-contact	E		Clutch or Brake	_ @_		
Pushbutton switch b-contact			Transformer			
Limit switch a-contact	~_		Resistor			
Limit switch b-contact			Variable resistor		— > ***	
Timer (ON delay) a-contact			Capacitor	+++	\(\psi\) \(\psi\)	
Timer (ON delay) b-contact	_¥_		Varistor	# /	‡ <i>1</i>	
Knife switch	H-77 H-7-7-1	11 111	Diode			
Magnetic contactor	~_	~~~	Rectifier (bridge type)			
Lamp	\bigotimes		Transistor (NPN type)			
Buzzer		BZ	Transistor (PNP type)	_<		
Ground	<u>_</u>		Photocoupler	¥=		
Connect to outer case	7//		Coil	$\sim\sim$		

 $[\]mbox{\ensuremath{^{\ast}}}$ This catalog uses the symbols that are currently the most common in its figures.

ELECTROMAGNETIC **CLUTCHES & BRAKES**

SERIES

ELECTROMAGNETIC-ACTUATED MICRO **CLUTCHES & BRAKES** ELECTROMAGNETIC-ACTUATED CLUTCHES & BRAKES ELECTROMAGNETIC CLUTCH & BRAKE UNITS

SPRING-ACTUATED BRAKE

ELECTROMAGNETIC TOOTH CLUTCHES

BRAKE MOTORS

POWER SUPPLIES

MODELS BES BEH BEW BEW-S BEW-W BEW-FH BEM